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# RESEARCH MEMORANDUM

A SPECIAL METHOD FOR FINDING BODY DISTORTIONS THAT  
REDUCE THE WAVE DRAG OF WING AND BODY  
COMBINATIONS AT SUPERSONIC SPEEDS

By Harvard Lomax and Max. A. Heaslet

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NATIONAL ADVISORY COMMITTEE  
FOR AERONAUTICS

WASHINGTON

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## NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

## A SPECIAL METHOD FOR FINDING BODY DISTORTIONS THAT

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## SUMMARY

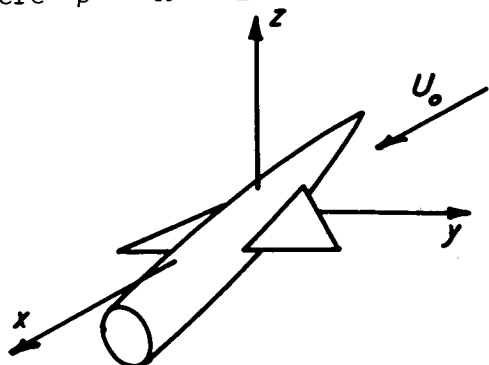
For a given wing and supersonic Mach number, the problem of shaping an adjoining fuselage so that the combination will have a low wave drag is considered. Only fuselages that can be simulated by singularities (multipoles) distributed along the body axis are studied. However, the optimum variations of such singularities are completely specified in terms of the given wing geometry. An application is made to an elliptic wing having a biconvex section, a thickness-chord ratio equal to 0.05 at the root, and an aspect ratio equal to 3. A comparison of the theoretical results with a wind-tunnel experiment is also presented.

## INTRODUCTION

The most simplifying assumptions that still permit the construction of a mathematical model general enough to contain quantitative information about steady three-dimensional supersonic flow are those basic to the development of linearized theory. Of these, the two principal assumptions are that the viscosity effects are negligible and the perturbation velocities are almost everywhere small enough to be neglected relative to the flight or free-stream velocity. Under such restrictions the flow field can be described in terms of a perturbation velocity potential  $\phi$  obeying the equation

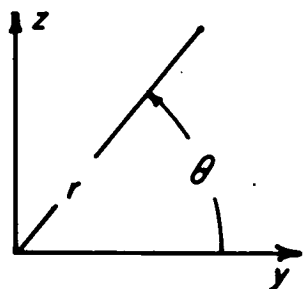
$$\beta^2 \phi_{xx} - \phi_{yy} - \phi_{zz} = 0 \quad (1)$$

where  $\beta^2 = M^2 - 1$  and the reference coordinate system<sup>1</sup> is shown in sketch (a). Further, the wave drag of any object in a flow field governed by equation (1) can be evaluated (see, e.g., ref. 1) by means of the equation



$$D = -\rho_0 \int_{-\infty}^{\infty} dx \int_0^{2\pi} d\theta \left[ \lim_{r \rightarrow \infty} (r \varphi_r \varphi_x) \right] \quad (2)$$

where  $x, r$ , and  $\theta$  are cylindrical coordinates also defined in sketch (a).



Sketch (a)

General solutions to equation (1) are numerous and classical. In applying these solutions to the interpretation of physical phenomena the usual approach is to fit them to the given boundary conditions, that is, to make the flow field simulated by them conform to the shape of the disturbing object as well as to a uniform free

stream at infinity. Hence, from this point of view, the choice of a type of general solution to be used in analyzing a particular problem with the least mathematical effort depends on the geometric form of the object under consideration. For example, general solutions based on Green's theorem are well adapted to the study of forces on single planar wings in a steady supersonic flow. On the other hand, the general solution given by Lamb (ref. 2) - which is composed of an infinite set of multipole distributions disposed along a line - is well adapted to the study of the flow around fuselage-like objects.

In this report use is made of certain general solutions to equation (1) but with a deviation from the usual approach mentioned above. One considers, in fact, two different kinds of solutions which represent separately, in a given vicinity, different classes of real objects and, by means of equation (2), finds optimum combinations of these solutions from the viewpoint of low wave drag. The analysis involved in solving this problem has, in general, a distinct mathematical advantage over the problem of calculating the drag of a given object; namely, that the immediate problem of finding a shape with a relatively low wave drag is divorced from any detailed reference to the shape itself. It is true, of course, that the stream surface representing this shape must eventually be found and, in fact, a limitation on the applicability of the method is given by the requirement that this shape be real. However, the problem

<sup>1</sup>It should be stressed that the  $x$  axis is parallel to the free-stream direction (wind axes) so a body of revolution can be symmetrical about this axis only at zero angle of attack.

of finding the shape of the object when  $\Phi$  is known is a matter of direct calculation.<sup>2</sup> One should also be careful to notice that the optimum solutions obtained by this procedure are not necessarily true optimums but purely relative to the choice of solutions used in the analysis.

## LIST OF IMPORTANT SYMBOLS

A	wing aspect ratio
$A_n(x)$	$(-\beta)^n$ times the $n$ th derivative of the $n$ th multipole distribution $a_n(x)$ (See eq. 16.)
a	semiroot chord of elliptic wing
$a_n(x)$	strength of $n$ th-order multipole distribution multiplying $\cos n\theta$
$B_n(x)$	$(-\beta)^n$ times the $n$ th derivative of the $n$ th multipole distribution $b_n(x)$
b	semispan of elliptic wing
$b_n(x)$	strength of $n$ th-order multipole distribution multiplying $\sin n\theta$
$C_D$	drag coefficient, $\frac{D}{qS}$
$C_p$	pressure coefficient, local pressure minus static pressure divided by $q$
D	wave drag
$\bar{D}_n$	wave drag associated with $n$ th-order multipole distribution (See eq. 59.)
$L_0', L_0$	maximum fore-and-aft extent of wing equivalent multipole distribution
$L'(\theta), L(\theta)$	maximum fore-and-aft extent of wing equivalent multipole distribution for angle $\theta$
M	free-stream Mach number

---

<sup>2</sup>From a mathematical point of view the essence of the method outlined above is that the analysis involves the solution to direct problems, that is, problems of integration. Calculating the drag of a given body, on the other hand, involves the solution to inverse problems, that is, problems involving the inversion of integral equations.

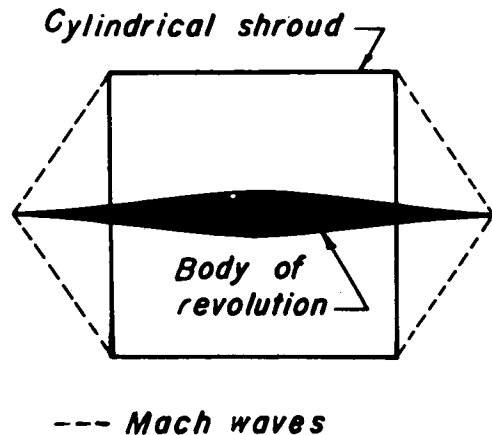
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$q$	free-stream dynamic pressure, $\frac{\rho_0 U_0^2}{2}$
$\bar{r}$	$\frac{\beta R}{L_0}$
$\bar{r}_e$	see equation (46)
$R$	radius of body
$S$	area of wing plan form
$S_w(x, \theta)$	normal projection of wing cross-sectional area measured in oblique planes
$t$	maximum thickness of wing root chord
$U_0$	speed of free stream
$V$	volume
$x, y, z$	Cartesian coordinate system, $x$ parallel to free-stream direction
$x, r, \theta$	cylindrical coordinate system, $x$ parallel to free-stream direction
$\alpha(x)$	strength of $n$ th-order optimum cancellation multipoles (See eq. (36).)
$\beta$	$\sqrt{M^2 - 1}$
$\lambda_u$	slope of wing upper surface measured parallel to free-stream direction
$\mu$	$\tan^{-1} (\beta \cos \theta)$
$\rho_0$	free-stream density
$\phi$	perturbation velocity potential

#### DEFINITION OF THE PROBLEM

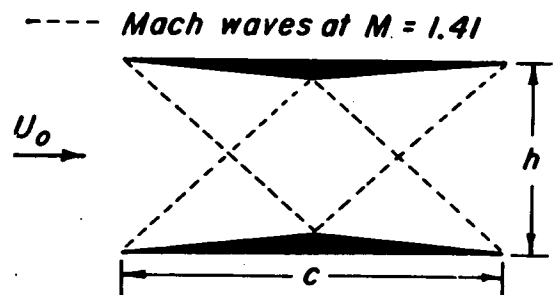
The problem of designing an airplane to have a minimum wave drag must be stated quite precisely. If the aerodynamicist is approached with the question, "Given an aerodynamic shape, can its wave drag be lowered?" he can always reply that any volume of material having a wave drag can always be reshaped within a space of finite dimensions so that it will have less wave drag at a given Mach number. Such an answer is interesting but,

at present, not very useful to the airplane designer. There is first, of course, the basic criterion that the total drag should be minimized at a given lift and minimizing a component part of this total without holding the other parts fixed does not necessarily yield the lowest possible drag for a given set of restraints. For example, the configuration illustrated in sketch (b) has no wave drag when traveling at zero angle of attack; but it has a relatively high friction drag, because of the large amount of wetted area, and its drag due to lift could also be relatively high. Completely aside from all such performance considerations, however, are many other important considerations that are unfortunately more or less vaguely defined from an aerodynamic point of view. For example, an airplane must contain a certain amount of usable volume, the shaping of individual parts is limited by structural requirements, and the arrangement of these parts must not seriously harm the airplane stability and control. The interrelation of all such separate demands presents an extremely complex design problem making it difficult to deviate too far from the reliable shapes set by experience.

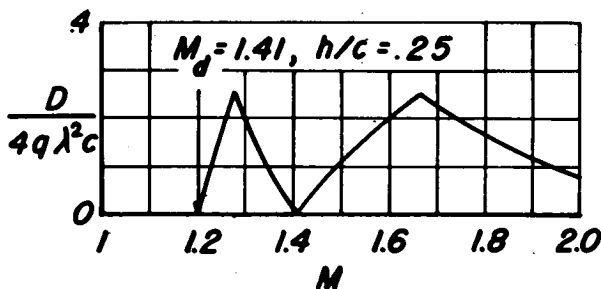
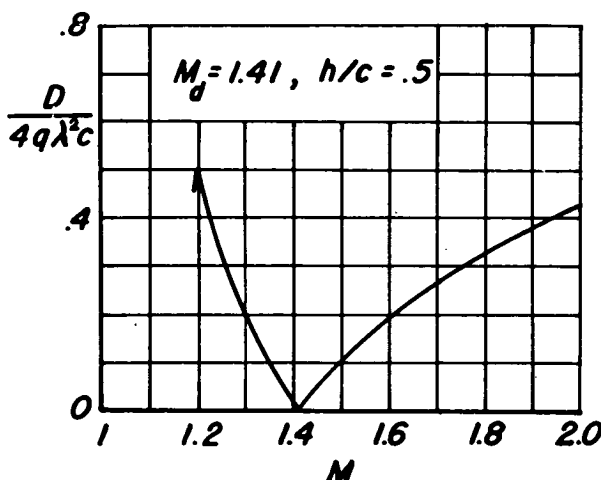


Sketch (b)

As a result of the above-mentioned difficulties, the aerodynamicist who is concerned with discovering a practical airplane shape having low wave drag finds the real definition of his problem somewhat obscure. In a sense his first problem is, literally, to pose a problem; that is, to impose a minimum number of arbitrary but pertinent restraints within the framework of which the wave drag is to be minimized. Even when this has been done, he still is concerned with the question of uniqueness, since optimum shapes are not necessarily unique even when several restraints are imposed. Consider, for example, the problem of finding the Busemann biplane which will have minimum wave drag at a given Mach number for a fixed section strength, volume, and wetted area. If the design Mach number is 1.41, one such design (on the basis of linearized theory) is shown in sketch (c) where the chord-gap ratio,  $h/c$ , is equal to  $1/2$ . The resulting variation of the wave drag is shown in the upper part of sketch (d). However, when the gap is closed to the point where  $h/c$  equals  $1/4$ , the variation of wave drag, shown in



Sketch (c)



Sketch (d)

the lower part of sketch (d), is the same within the interval  $1.28 \leq M \leq 1.66$  and everywhere else is lower. It is likely that one would have first discovered the former solution, yet to the accuracy of the theory used, the latter is obviously preferable.

With the above observations always in mind, attention will be directed in this report to the analysis of simplified configurations composed of two distinct types of volume: planar types, that is, wing-like volumes, thin in one dimension and bounded by surfaces that never deviate far from a reference plane; and rectilinear types, that is, fuselage-like volumes longer in one dimension than in the other two and disposed more or less symmetrically about a straight line

In particular the following problem is posed:

Given a thin nonlifting wing, what is the shape of an adjoining fuselage, the stream surface of which is simulated by a line of multipoles in the same plane as the wing, that will minimize the wave drag of the combination at a given Mach number?

## BASIC CONCEPTS

### A Line of Sources

The velocity potential induced at the point  $x, r, \theta$  by a group of sources distributed along the  $x$  axis, starting at  $-L_0$ , is well known to be given by

$$\phi(x, r, \theta) = -\frac{1}{2\pi} \int_{-L_0}^{x-\beta r} \frac{a_0(\xi) d\xi}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} \quad (3)$$



where  $a_0(\xi)$  is the source strength per unit of length. In order to calculate wave drag one needs only the value of  $\phi$  as  $r$  approaches infinity. This asymptotic value is simple enough to find provided it is observed that, as  $r$  is increased,  $x$  should also be increased so the potential can be studied in the vicinity of the Mach waves radiating from the disturbing object. Hence, set

$$x = x_0 + \beta r \quad (4)$$

so for a given  $r$ ,  $x_0$  measures the streamwise distance of the point  $x, r, \theta$  from the Mach wave emanating from the origin and, in particular, the foremost wave is located at  $x_0 = -L_0$ . (See sketch (e).)

If equation (4) is placed into equation (3) and  $r$  is assumed to be large, the potential induced by a source is

$$\phi)_{r \rightarrow \infty} = - \frac{1}{2\pi\sqrt{2\beta r}} \int_{-L_0}^{x_0} \frac{a_0(\xi) d\xi}{\sqrt{x_0 - \xi}} \quad (5)$$

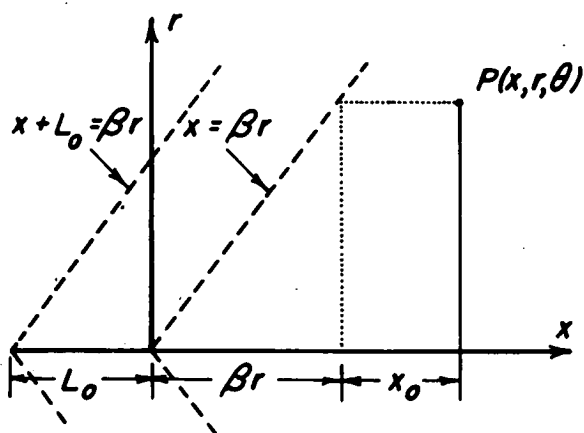
and the induced velocities are

$$\phi_x)_{r \rightarrow \infty} = - \frac{1}{2\pi\sqrt{2\beta r}} \int_{-L_0}^{x_0} \frac{a_0'(\xi) d\xi}{\sqrt{x_0 - \xi}} \quad (6a)$$

$$\phi_r)_{r \rightarrow \infty} = -\beta\phi_x \quad (6b)$$

Multipoles

Lamb, in reference 2, page 527, has presented a general solution to equation (1) consisting of an infinite set of basic singular solutions. These basic singularities, referred to as multipoles, can be distributed along a line and weighted so as to reproduce certain body shapes enclosing the line. The expression for the perturbation velocity potential for a distribution of  $n$ th-order ( $n = 0, 1, 2, \dots$ ) multipoles starting at  $-L_0$  and continuing along the  $x$  axis can be written in terms of a cylindrical coordinate system (sketch (a)) as



Sketch (e)

$$\Phi_n(x, r, \theta) = -\frac{r^n}{2\pi} \left( \frac{1}{r} \frac{\partial}{\partial r} \right)^n \int_{-L_0}^{x-\beta r} \frac{[a_n(\xi) \cos n\theta + b_n(\xi) \sin n\theta] d\xi}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} \quad (7)$$

The operator  $\left( \frac{1}{r} \frac{\partial}{\partial r} \right)^2$  is defined as

$$\left( \frac{1}{r} \frac{\partial}{\partial r} \right)^2 = \frac{1}{r} \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial}{\partial r} \right) = -\frac{1}{r^3} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial r^2}$$

and the definition of  $\left( \frac{1}{r} \frac{\partial}{\partial r} \right)^n$  follows by induction. If the notation<sup>3</sup>

$$\left( \frac{\partial}{\partial x} \right)^n \int_a^x \frac{A(y) dy}{\sqrt{x-y}} = (-1)^n \frac{(1)(3) \cdots (2n-1)}{2^n} \int_a^x \frac{A(y) dy}{(x-y)^{(2n+1)/2}}$$

is introduced, where the symbol  $\int$  is read "finite part of the integral," equation (7) becomes

$$\Phi_n(x, r, \theta) = -\frac{r^n \beta^{2n} (2n)!}{2^{n+1} \pi(n)!} \int_{-L_0}^{x-\beta r} \frac{[a_n(\xi) \cos n\theta + b_n(\xi) \sin n\theta] d\xi}{[(x-\xi)^2 - \beta^2 r^2]^{(2n+1)/2}} \quad (8)$$

and the general expressions for the induced velocities become - writing only the term involving the cosine, since the result for the sine is identical -

$$\Phi_x(x, r, \theta) = \sum_{n=0}^{\infty} \frac{r^n \beta^{2n} (2n+2)!}{2^{2n+2} \pi(n+1)!} \int_{-L_0}^{x+\beta r} \frac{(x-\xi) a_n(\xi) \cos n\theta d\theta}{[(x-\xi)^2 - \beta^2 r^2]^{(2n+3)/2}} \quad (9a)$$

$$\Phi_r(x, r, \theta) = -\sum_{n=0}^{\infty} \frac{\beta^{2n} r^{n-1} (2n)!}{2^{n+1} \pi(n)!} \int_{-L_0}^{x-\beta r} \frac{[n(x-\xi)^2 + (n+1)\beta^2 r^2] a_n(\xi) \cos n\theta d\xi}{[(x-\xi)^2 - \beta^2 r^2]^{(2n+3)/2}} \quad (9b)$$

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<sup>3</sup>For a detailed discussion of the finite-part concept as used in this report see reference 3.

$$\frac{1}{r} \phi_{\theta}(x, r, \theta) = \sum_{n=0}^{\infty} \frac{n r^{n-1} \beta^{2n} (2n)!}{2^{n+1} \pi(n)!} \int_{-L_0}^{x-\beta r} \frac{a_n(\xi) \sin n\theta d\xi}{[(x-\xi)^2 - \beta^2 r^2]^{(2n+1)/2}} \quad (9c)$$

Another very useful way of developing these multipole solutions evolves from an application of operational techniques. To begin with, rewrite equation (1) in terms of a polar coordinate system, thus

$$\beta^2 \frac{\partial^2 \phi}{\partial x^2} - \frac{\partial^2 \phi}{\partial r^2} - \frac{1}{r} \frac{\partial \phi}{\partial r} - \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2} = 0 \quad (10)$$

Next, define the Laplace transform of  $\phi(x, r, \theta)$  by

$$\bar{\phi}(s, r, \theta) = \int_0^{\infty} \phi(x, r, \theta) e^{-xs} dx \quad (11)$$

and apply this transform to equation (10). There results (for a proof see Appendix A)

$$\beta^2 s^2 \bar{\phi} - \frac{\partial^2 \bar{\phi}}{\partial r^2} - \frac{1}{r} \frac{\partial \bar{\phi}}{\partial r} - \frac{1}{r^2} \frac{\partial^2 \bar{\phi}}{\partial \theta^2} = 0 \quad (12)$$

Now, if a general solution to equation (12) is expressed in the form

$$\bar{\phi}(s, r, \theta) = f(r) \cos n\theta$$

then  $f(r)$  must satisfy the equation

$$\frac{d^2 f}{dr^2} + \frac{1}{r} \frac{df}{dr} - \left( \frac{n^2}{r^2} + \beta^2 s^2 \right) f = 0$$

Solutions to this are given by

$$f(r) = \bar{C}_n(s) I_n(\beta r s) + \bar{A}_n(s) K_n(\beta r s)$$

where  $I_n$  and  $K_n$  are modified Bessel functions as defined in reference 4, page 77. Hence, if  $\bar{\phi}$  is to vanish as  $r$  goes to infinity, a general

solution to equation (10) can be written in the form

$$\bar{\varphi}(s, r, \theta) = \frac{-1}{2\pi} \sum_0^{\infty} [\bar{A}_n(s) \cos n\theta + \bar{B}_n(s) \sin n\theta] K_n(\beta rs) \quad (13)$$

The above result will be transformed back to the physical plane in two ways. First, apply the identity (ref. 4, p. 79)

$$K_n(z) = (-1)^n \left( \frac{1}{z} \frac{d}{dz} \right)^n K_0(z)$$

and re-express equation (13) as (only the coefficient of the  $\cos n\theta$  term is written since the treatment of the sine term is identical)

$$\bar{\varphi}(s, r, \theta) = -\frac{1}{2\pi} \sum_0^{\infty} (-1)^n \cos n\theta \frac{\bar{A}_n(s)}{\beta^n s^n} r^n \left( \frac{1}{r} \frac{d}{dr} \right)^n K_0(\beta rs)$$

The inverse Laplace transform of  $K_0(\beta rs)$  - see reference 5 - is

$$L^{-1}[K_0(\beta rs)] = \begin{cases} 0 & , \quad x < \beta r \\ \frac{1}{\sqrt{x^2 - \beta^2 r^2}} & , \quad x > \beta r \end{cases}$$

So, since

$$\int_{-L_0}^x dx_1 \int_{-L_0}^{x_1} dx_2 \cdots \int_{-L_0}^{x_{n-1}} dx_n A_n(x_n) = \frac{1}{(n-1)!} \int_{-L_0}^x (x - x_1)^{n-1} A_n(x_1) dx_1 \quad (14)$$

an application of the convolution integral and other standard operational techniques yield

$$\varphi(x, r, \theta) = -\frac{1}{2\pi} \left\{ \int_{-L_0}^{x-\beta r} \frac{A_0(\xi) d\xi}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} + \sum_1^{\infty} r^n \left( \frac{1}{r} \frac{d}{dr} \right)^n \int_{-L_0}^{x-\beta r} \frac{\left[ \frac{(-1)^n}{\beta^n (n-1)!} \int_{-L_0}^{\xi} (\xi - x_1)^{n-1} A_n(x_1) dx_1 \right]}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} d\xi \right\} \quad (15)$$

From comparison of equations (8) and (15), the relation between the strengths  $a_n(x)$  and  $A_n(x)$  for the two different forms of the solution is found to be

$$\left. \begin{aligned} a_0(x) &= A_0(x) \\ (-\beta)^n a_n(x) &= \frac{1}{(n-1)!} \int_{-L_0}^x (x-x_1)^{n-1} A_n(x_1) dx_1, \quad n > 0 \end{aligned} \right\} \quad (16a)$$

or

$$(-\beta)^n a_n^{(n)}(x) = A_n(x) \quad (16b)$$

where  $a_n^{(n)}(x)$  symbolizes the operation  $\frac{d^n}{dx^n} a_n(x)$  and where use is made of the conditions

$$a_n^{(n)}(-L_0) = a_n^{(n-1)}(-L_0) = \dots = a_n(-L_0) = 0 \quad (17)$$

Another way to transform equation (13) back to the physical plane is to do so directly. In this way one finds (from ref. 5)

$$L^{-1}[K_n(\beta r s)] = \begin{cases} 0, & x < \beta r \\ \frac{\cosh\left[n \cosh^{-1}\left(\frac{x}{\beta r}\right)\right]}{\sqrt{x^2 - \beta^2 r^2}}, & x > \beta r \end{cases}$$

from which equation (13) reduces immediately to

$$\varphi(x, r, \theta) = -\frac{1}{2\pi} \sum_{n=0}^{\infty} \cos n\theta \int_{-L_0}^{x-\beta r} \frac{A_n(\xi) \cosh\left[n \cosh^{-1}\left(\frac{x-\xi}{\beta r}\right)\right]}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} d\xi \quad (18)$$

The perturbation velocities in the field represented by this potential are readily calculated. Thus

$$\varphi_x(x, r, \theta) = -\frac{1}{2\pi} \sum_0^{\infty} \cos n\theta \int_{-L_0}^{x-\beta r} \frac{A_n'(\xi) \cosh \left[ n \cosh^{-1} \left( \frac{x-\xi}{\beta r} \right) \right]}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} d\xi \quad (19a)$$

$$\frac{1}{r} \varphi_\theta(x, r, \theta) = \frac{1}{2\pi r} \sum_0^{\infty} n \sin n\theta \int_{-L_0}^{x-\beta r} \frac{A_n(\xi) \cosh \left[ n \cosh^{-1} \left( \frac{x-\xi}{\beta r} \right) \right]}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} d\xi \quad (19b)$$

and by taking the derivative of equation (13) with respect to  $r$ , one finds

$$\bar{\varphi}_r = \frac{1}{2\pi} \left\{ \beta s \bar{A}_0(s) K_1(\beta r s) + \frac{1}{2} \sum_1^{\infty} \beta s \bar{A}_n(s) [K_{n-1}(\beta r s) + K_{n+1}(\beta r s)] \right\}$$

which transforms to

$$\varphi_r(x, r, \theta) = \frac{1}{2\pi} \left( \int_{-L_0}^{x-\beta r} \frac{(x-\xi) A_0'(\xi) d\xi}{r \sqrt{(x-\xi)^2 - \beta^2 r^2}} + \frac{\beta}{2} \sum_1^{\infty} \cos n\theta \int_{-L_0}^{x-\beta r} \frac{A_n'(\xi) \left\{ \cosh \left[ (n-1) \cosh^{-1} \left( \frac{x-\xi}{\beta r} \right) \right] + \cosh \left[ (n+1) \cosh^{-1} \left( \frac{x-\xi}{\beta r} \right) \right] \right\} d\xi}{\sqrt{(x-\xi)^2 - \beta^2 r^2}} \right) \quad (19c)$$

If the relation between the functions  $a_n(x)$  and  $A_n(x)$  is given by equation (16), the velocities represented by equations (9) and (19) are, of course, identical.

In order to obtain limiting values induced by multipoles distributed along the  $x$  axis starting at  $-L_0$ , one returns to either equation (8) or (18) and calculates the leading term in a  $1/r$  expansion. As in the derivation of equation (5), it is necessary to observe that as  $r$  is increased,  $x$  should also be increased so  $\varphi$  is given in the vicinity of the foremost Mach cone created by the multipole distributions. Hence, using equation (4), one finds for equation (18)

$$\varphi = -\frac{1}{2\pi} \sum_0^{\infty} \cos n\theta \int_{-L_0}^{x_0} \frac{A_n(\xi) \cosh \left[ n \cosh^{-1} \left( 1 + \frac{x_0 - \xi}{\beta r} \right) \right] d\xi}{\sqrt{2\beta r(x_0 - \xi) \left( 1 + \frac{x_0 - \xi}{2\beta r} \right)}}$$

which has the leading term as  $r$  goes to infinity

$$\varphi)_{r \rightarrow \infty} = -\frac{1}{2\pi\sqrt{2\beta r}} \sum_0^{\infty} \cos n\theta \int_{-L_0}^{x_0} \frac{A_n(\xi) d\xi}{\sqrt{x_0 - \xi}} \quad (20)$$

Similarly, the perturbation velocities reduce to

$$\varphi_x)_{r \rightarrow \infty} = -\frac{1}{2\pi\sqrt{2\beta r}} \sum_0^{\infty} \cos n\theta \int_{-L_0}^{x_0} \frac{A_n'(\xi) d\xi}{\sqrt{x_0 - \xi}} \quad (21a)$$

$$\varphi_r)_{r \rightarrow \infty} = -\beta \varphi_x \quad (21b)$$

$$\left( \frac{1}{r} \varphi_{\theta} \right)_{r \rightarrow \infty} = \frac{1}{2\pi\sqrt{2\beta r}} \sum_0^{\infty} n \sin n\theta \int_{-L_0}^{x_0} \frac{A_n(\xi) d\xi}{\sqrt{x_0 - \xi}} \quad (21c)$$

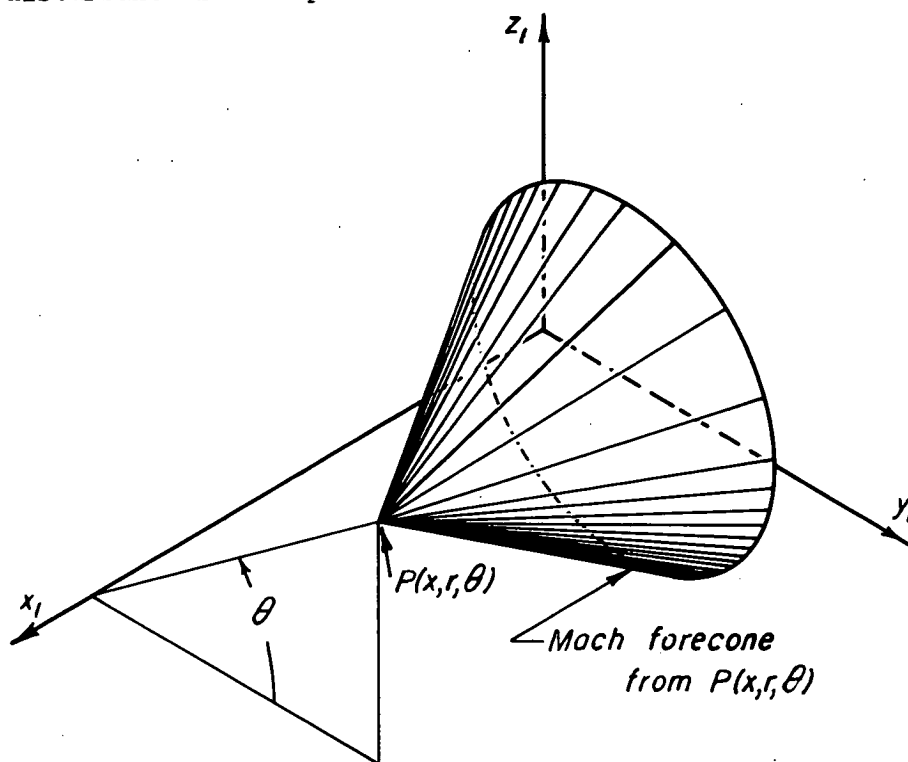
In calculating the wave drag using equation (2) only the velocity components  $\varphi_x)_{r \rightarrow \infty}$  and  $\varphi_r)_{r \rightarrow \infty}$  are necessary. Hence, from comparison of equations (21a) and (21b) with (6a) and (6b), it follows that at a given  $\theta$  a series of multipoles induce the same momentum flux on an infinite cylindrical control surface as a line of sources having a strength variation  $a_0(x)$  equal to  $\sum_0^{\infty} \cos n\theta A_n'(\xi)$ . If one identifies a line of sources with a body of revolution, then it is apparent that, at a given  $\theta$ , a dragwise equivalence has been established between a line of multipoles and a body of revolution.

# Hayes' Theorem and Its Application

In the previous section a relation was found between multipole and source strengths which produce, at a fixed  $\theta$ , equivalent momentum transport across a cylinder of infinite radius. By using a theorem due to Hayes (ref. 6) one can derive the strength relationship between any distribution of singularities throughout space and a line of sources which gives the same equivalence.

The essence of Hayes' theorem is that, for a fixed  $\theta$ , the velocities induced on a cylinder of infinite radius by singular solutions to equation (1) (e.g., sources and doublets) are invariant to displacements of the singularities along certain oblique planes. In order to be specific, the equation of these oblique planes is next derived.

Consider the point  $x, r, \theta$  in a flow field having a supersonic free stream moving parallel to the  $x$  axis. Sketch (f) shows the Mach forecone (by definition the Mach forecone is the boundary of the region within which a disturbance in a supersonic stream can affect the flow at the



Sketch (f)

cone apex) from  $x, r, \theta$  in  $x_1, y_1, z_1$  space. The equation of the forecone is

$$x_1 = x - \beta \sqrt{(r \cos \theta - y_1)^2 + (r \sin \theta - z_1)^2} \quad (22)$$



One wishes to let  $r$  become very large and find the shape of the forecone as it passes through regions close to the origin of the  $x_1, y_1, z_1$  coordinate system, regions in which the objects creating the wave drag are located. From equation (4), and the expansion of equation (22) for large  $r$ , it follows that

$$\begin{aligned} x_1 &= x_0 + \beta r - \beta r \left[ 1 - \frac{2}{r} (y_1 \cos \theta + z_1 \sin \theta) + \frac{y_1^2 + z_1^2}{r^2} \right]^{1/2} \\ &= x_0 + \beta (y_1 \cos \theta + z_1 \sin \theta) - \frac{\beta}{2r} (y_1 \sin \theta - z_1 \cos \theta)^2 + \dots \end{aligned}$$

and when  $r$  goes to infinity

$$x_1 = x_0 + \beta y_1 \cos \theta + \beta z_1 \sin \theta \quad (23)$$

which is the equation of the oblique plane mentioned above. It should be noted that the envelope formed from these planes by fixing  $x_0$  and varying  $\theta$  between 0 and  $2\pi$  coincides with the Mach forecone and aftercone from the point  $x_0, 0, 0$ .

Hayes' result can now be stated<sup>4</sup>

To the lowest order in  $1/r$ , as  $r$  tends to infinity, the magnitude of the perturbation velocity potential and its gradients at a fixed azimuth angle is invariant to a finite translation of sources (or any other singular solution to the wave equation) on planes parallel to that given by equation (23).

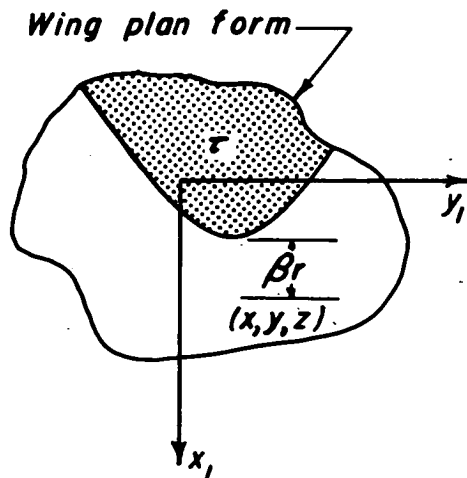
Consider the application of Hayes' theorem to planar distributions of sources lying in the  $z_1 = 0$  plane. As is well known, such a distribution simulates a wing symmetrically disposed about the horizontal ( $z_1 = 0$ ) plane. In fact, if  $\lambda_u(x_1, y_1)$  is the local slope of the wing upper surface, the local source strength per unit area (according to thin airfoil theory) required to simulate the wing is  $-U_0 \lambda_u / \pi$  and the velocity potential of the disturbed flow field is given by

$$\phi(x, y, z) = -\frac{U_0}{\pi} \iint_{\tau} \frac{\lambda_u(x_1, y_1) dx_1 dy_1}{\sqrt{(x - x_1)^2 - \beta^2(y - y_1)^2 - \beta^2 z^2}} \quad (24)$$

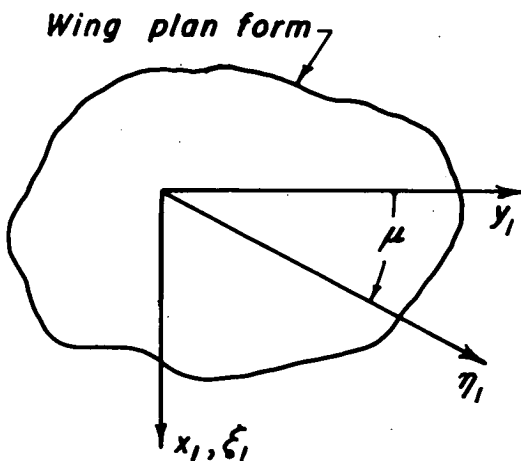
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<sup>4</sup>For proofs, see Hayes' original derivation (ref. 6) or, if more convenient, reference 1.

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Sketch (g)



Sketch (h)

where  $\tau$  is the area of integration (see sketch (g)) bounded by the wing edge and the trace in the  $z_1 = 0$  plane of the Mach forecone from the point  $x, y, z$ . Next introduce the new coordinates  $\xi_1$  and  $\eta_1$  such that  $\xi_1$  lies along the  $x_1$  axis and  $\eta_1$  lies along the intersection of the  $z_1 = 0$  plane and the plane given by equation (23) (see sketch (h)). Set

$$\tan \mu = \beta \cos \theta \quad (25)$$

and

$$\left. \begin{aligned} \xi_1 &= x_1 - y_1 \tan \mu \\ \eta_1 &= y_1 \sec \mu \\ x_1 &= \xi_1 + \eta_1 \sin \mu \\ y_1 &= \eta_1 \cos \mu \end{aligned} \right\} \quad (26)$$

Then, in terms of the  $\xi_1, \eta_1$  system, equation (24) becomes

$$\phi(x, y, z) = -\frac{U_0}{\pi} \iint_{\tau} \frac{\lambda_u(\xi_1 + \eta_1 \sin \mu, \eta_1 \cos \mu) \cos \mu \, d\xi_1 d\eta_1}{\sqrt{(x - \xi_1 - \eta_1 \sin \mu)^2 - \beta^2 (y - \eta_1 \cos \mu)^2 - \beta^2 z^2}} \quad (27)$$

As before, the asymptotic value of  $\phi$  as  $r = \sqrt{y^2 + z^2} \rightarrow \infty$  is to be calculated. Accordingly, one can apply Hayes' theorem and sum up all the

sources along a line  $\xi_1 = \text{constant}$  (e.g., between a and b in sketch (i)) and place them as a single source on the axis. The strength of this large equivalent source is given by

$$U_0 S_w'(\xi_1, \theta) = 2U_0 \cos \mu \int_{\text{wing}} \lambda_u(\xi_1 + \eta_1 \sin \mu, \eta_1 \cos \mu) d\eta_1 \quad (28)$$

where the integration is taken across the complete wing along the line  $\xi_1 = \text{constant}$  and

$$S_w'(\xi_1, \theta) = \frac{\partial}{\partial \xi_1} S_w(\xi_1, \theta).$$

The term  $S_w(x, \theta)$  has a clear geometrical interpretation (see sketch (j)), being simply the normal projection of the wing area intercepted by the oblique plane<sup>5</sup>

$$x_1 = x + \beta y_1 \cos \theta.$$

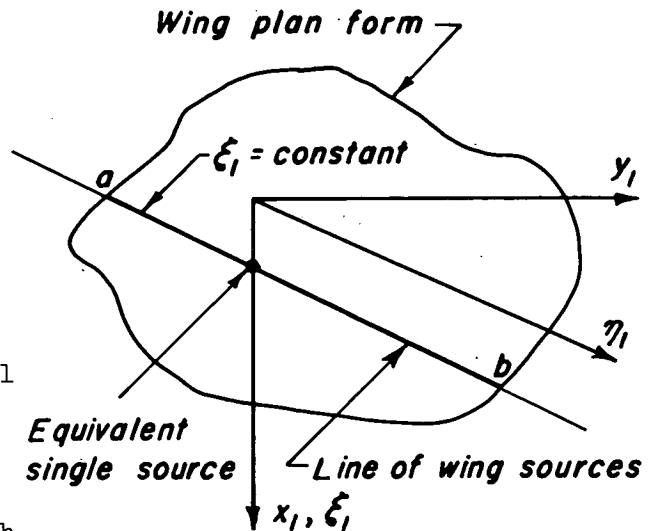
The above defines the strength variation of a line of sources (and, therefore, a body of revolution) which induces, for large  $r$  and a fixed  $\theta$ , a potential field identical to that induced by a given wing. Hence, the results given in equation (6) yield

$$\Phi(x)_{r \rightarrow \infty} = - \frac{U_0}{2\pi\sqrt{2\beta}r} \int_{-L(\theta)}^{x_0} \frac{S_w''(\xi_1, \theta) d\xi_1}{\sqrt{x_0 - \xi_1}} \quad (29a)$$

$$\Phi(r)_{r \rightarrow \infty} = -\beta \Phi_x \quad (29b)$$

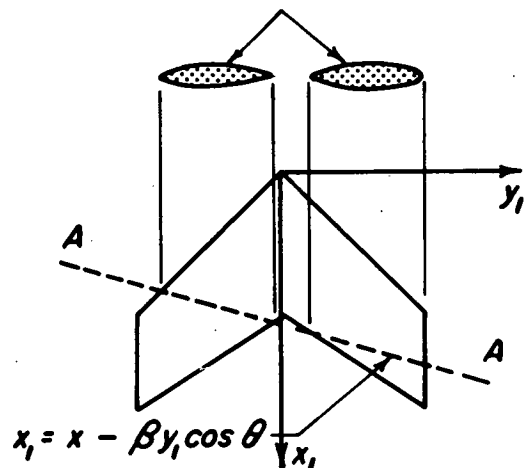
A similar result exists for a planar doublet distribution (see ref. 1 or 6) but, in this report, only problems in which the wings have

<sup>5</sup>The true oblique plane is given by equation (23) but the wing is so close to the  $z_1 = 0$  plane that the variation with  $z_1$  can be neglected.



Sketch (i)

$S(x, \mu) = \text{Normal projection of wing area along AA}$



Sketch (j)

no loading (local lift) will be considered. Lifting effects can be treated in a similar fashion, of course, if the wing doublet strengths are known.

### Cancellation Multipoles and Drag Minimization

Since the flow field is governed by a linear partial differential equation the velocities induced by different solutions to it are additive. Therefore, the drag of an object simulated by various multipoles distributed along the  $x_1$  axis and a sheet of sources in the  $z_1 = 0$  plane is given by

$$D = -\rho_0 \int_0^{2\pi} d\theta \int_{-\infty}^{\infty} dx \left\{ \lim_{r \rightarrow \infty} \left[ (\phi_r)_m + (\phi_r)_w \right] \left[ (\phi_x)_m + (\phi_x)_w \right] \right\}$$

where the subscripts  $m$  and  $w$  refer to the multipoles and wing sources, respectively. But equations (21) and (29) identify, for a fixed  $\theta$ , these velocities with those induced by equivalent line sources. Hence, for any given  $\theta$ , one can immediately apply Kármán's drag formula (ref. 7) and then for the total drag, integrate  $\theta$  from 0 to  $2\pi$ . This leads to

$$D = -\frac{\rho_0}{8\pi^2} \int_0^{2\pi} d\theta \int_{-L'(\theta)}^{L(\theta)} dx_1 \int_{-L'(\theta)}^{L(\theta)} dx_2 \left\{ U_0 S_w''(x_1, \theta) + \sum_{n=0}^{\infty} (-\beta)^n \left[ a_n^{(n+1)}(x_1) \cos n\theta + b_n^{(n+1)}(x_1) \sin n\theta \right] \right\} \\ \left\{ U_0 S_w''(x_2, \theta) + \sum_{n=0}^{\infty} (-\beta)^n \left[ a_n^{(n+1)}(x_2) \cos n\theta + b_n^{(n+1)}(x_2) \sin n\theta \right] \right\} \ln |x_1 - x_2|$$

However, since both the wing and multipoles are in the same plane (interpreted physically, the wing is centrally mounted on the fuselage) and the wing is simulated by sources only (has no twist or camber), one can show the optimum value of each  $b_n^{(n+1)}(x_1)$  is identically zero.<sup>6</sup>

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<sup>6</sup>By symmetry

$$S_w''(x, \theta) = S_w''(x, 2\pi - \theta)$$

Hence

$$\int_0^{2\pi} \sin n\theta S_w''(x, \theta) d\theta = 0$$

and any positive or negative variation of  $b_n^{(n+1)}(x_1)$  can only increase the drag.

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Hence, one can write

$$D = - \frac{\rho_0}{8\pi^2} \int_0^{2\pi} d\theta \int_{-L'(\theta)}^{L(\theta)} dx_1 \int_{-L'(\theta)}^{L(\theta)} dx_2 \left[ U_0 S_w''(x_1, \theta) + \sum_0^{\infty} (-\beta)^n a_n^{(n+1)}(x_1) \cos n\theta \right] \\ \left[ U_0 S_w''(x_2, \theta) + \sum_0^{\infty} (-\beta)^n a_n^{(n+1)}(x_2) \cos n\theta \right] \ln |x_1 - x_2| \quad (30)$$

Next expand the term  $S_w''(x, \theta)$  in a Fourier series. One finds

$$U_0 S_w''(x, \theta) = \sum_0^{\infty} (-\beta)^n \alpha_n^{(n+1)}(x) \cos n\theta \quad (31)$$

where

$$\alpha_0(x) = \frac{U_0}{2\pi} \int_0^{2\pi} S_w'(x, \theta) d\theta \quad (32)$$

$$\alpha_n^{(n)}(x) = \frac{U_0}{\pi(-\beta)^n} \int_0^{2\pi} S_w'(x, \theta) \cos n\theta d\theta \quad (33)$$

Place these expressions in equation (30), integrate with respect to  $\theta$  - using the orthogonal property of the trigonometric series - and one finds

$$D = 2D_0 + \sum_1^{\infty} D_n \quad (34)$$

where

$$\frac{D_n}{q} = - \frac{\beta^{2n}}{4\pi U_0^2} \int_{-L_0}^{L_0} dx_1 \int_{-L_0}^{L_0} dx_2 \left[ \alpha_n^{(n+1)}(x_1) + a_n^{(n+1)}(x_1) \right] \\ \left[ \alpha_n^{(n+1)}(x_2) + a_n^{(n+1)}(x_2) \right] \ln |x_1 - x_2| \quad (35)$$

Since one can show<sup>7</sup>

$$I = - \int_{-L_0}^{L_0} dx_1 \int_{-L_0}^{L_0} dx_2 f'(x_1) f'(x_2) \ln |x_1 - x_2| \geq 0$$

the minimum value of  $D$  as expressed by equation (34) is given when each  $D_n$  is itself a minimum. In other words, each  $D_n$  can be minimized separately. Further, it follows that the value of the minimum itself is zero and occurs when

$$a_n^{(n+1)}(x) = -\alpha_n^{(n+1)}(x) = \begin{cases} -\frac{U_0}{2\pi} \int_0^{2\pi} S_w''(x, \theta) d\theta, & n = 0 \\ -\frac{U_0}{\pi(-\beta)^n} \int_0^{2\pi} S_w''(x, \theta) \cos n\theta d\theta, & n > 0 \end{cases} \quad (36)$$

Equation (36) is the mathematical definition of the optimum cancellation multipoles; namely, those multipoles which are just equal in magnitude and opposite in sign to the wing equivalent multipoles - equivalent in the sense that they induce an identical momentum flux across a cylinder of infinite radius.

Obviously, if all the optimum cancellation multipoles were used, the wave drag of the combination would be zero. This result must, however, be properly interpreted with regard to the simulated shape. In order that the multipole lines can represent the distortion of a real fuselage, one must assume a cylindrical body exists upstream from the Mach cone  $x + L_0 = \beta r$  (the effects of the nose are being neglected). This body forms the initial boundary of the stream tube which represents the physical fuselage in the vicinity of the wing and multipole lines. Clearly, the area enclosed by this initial boundary can be small enough for the subsequent stream surface to cross itself and represent, therefore, a physically unreal body. Hence, the fact that the wave drag of the wing and multipole combination can be reduced to zero is quite valid, but in the

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<sup>7</sup>Set  $f(x) = \sum_1^{\infty} A_n \sin n\psi$ ,  $x = -L_0 \cos \psi$ . Integration gives

$$I = \frac{\pi^2}{2} \sum_1^{\infty} n A_n^2$$

which can never be negative.

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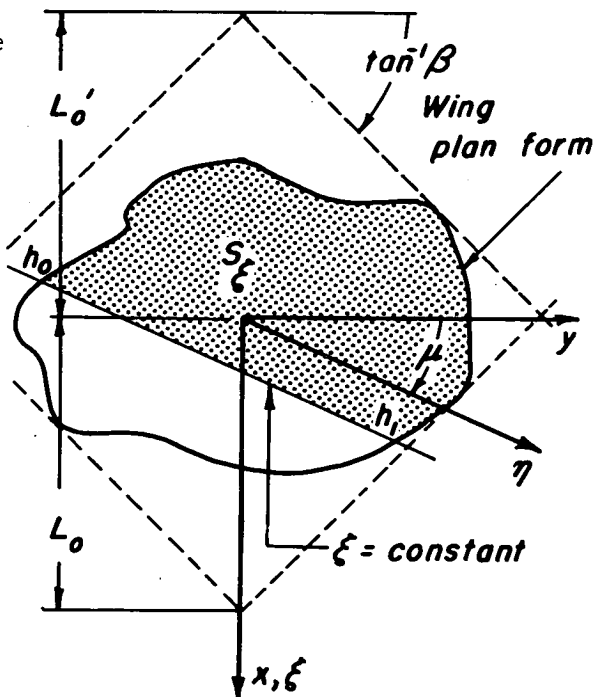
over-all picture not only have the inevitable nose and tail drags been neglected but also the shape simulated by the combination can be unrealistic.

## Some Properties of the Cancellation Multipoles

Let us consider next some of the restrictions necessarily imposed on cancellation-multipole distributions and some of the particular properties of those given by equation (36). In the first place, if  $a_n(x)$  is any multipole distribution that generates a potential field given by equation (8) or (15), it follows from equation (17) that the value of  $a_n(x)$  and its first  $n$  derivatives should be everywhere continuous. Further, if  $a_n(x)$  is a constant behind some point, say  $L_0$  (i.e., for  $\infty > x > L_0$ ), the induced flow field would simulate expanding streamlines in the case  $n = 0$  or some form of vorticity in the case  $n > 0$ ; the former case is to be avoided since any simulated body is assumed to have a finite area at  $x = \infty$ , and the latter case is to be avoided if there are no resultant forces normal to the free stream.

One can show that all the above properties are satisfied by  $\alpha_n(\xi)$ , the optimum cancellation-multipole distribution as defined by equation (36). First, notice that  $\alpha_n^{(n+1)}(\xi)$  must be zero everywhere outside the wing-enclosing Mach forecone and aftercone, that is for  $-\infty < \xi < -L_0$  and  $L_0 < \xi < \infty$  (see sketch (k)). (Any multipoles in these regions cannot combine with the wing equivalent multipoles and must, therefore, increase the drag.) Hence, one can set

$$\begin{aligned}\alpha_n^{(n)}(-L_O') &= \alpha_n^{(n-1)}(-L_O') \\ &= \dots \alpha_n(-L_O') \\ &= 0\end{aligned}$$



Sketch (k)

Then the condition of continuity is automatically satisfied for  $\alpha_n^{(n)}(\xi)$  in the entire interval  $-\infty < x < \infty$  if  $S_w'(\xi, \theta)$  is derived from a wing having finite wave drag (in particular, from a wing having no blunt edges along which the normal component of the free-stream Mach number is unity or greater). It follows immediately that  $\alpha_n^{(m)}(\xi)$ ,  $m < n$ , is continuous since the latter is found by integrating (further smoothing)  $\alpha_n^{(n)}(\xi)$ .

The proof that  $\alpha_n(L_0)$  as given by equation (36) is zero requires more consideration. One can show, however, that  $\alpha_n^{(m)}(L_0) = 0$  where  $0 \leq m \leq n$ . First, the equality  $\alpha_n^{(n)}(L_0) = 0$  follows from the fact that the wing closes and  $S_w'(L_0, \theta)$  itself is zero. Next consider the definition of  $\alpha_n^{(m)}(\xi)$ . Thus

$$\begin{aligned}\alpha_n^{(m)}(\xi) &= \frac{-U_0}{(-\beta)^n \pi} \int_0^{2\pi} S_w'(\xi, \theta) \cos n\theta \, d\theta \\ &= \frac{-2U_0}{(-\beta)^n \pi} \int_0^{2\pi} \cos \mu \cos n\theta \, d\theta \int_{h_0(\theta, \xi)}^{h_1(\theta, \xi)} \lambda_u(\xi + \eta \sin \mu, \eta \cos \mu) d\eta\end{aligned}$$

where use has been made of equation (28) for the definition of  $S_w'(\xi, \theta)$  and  $h_0$  and  $h_1$  are defined in sketch (k). Since

$$\alpha_n^{(m)}(\xi) = \frac{1}{\Gamma(n-m)} \int_{-L_0}^{\xi} (\xi - \xi_1)^{n-m-1} \alpha_n^{(n)}(\xi_1) d\xi_1 \quad (37)$$

one has

$$\begin{aligned}\alpha_n^{(m)}(\xi) &= \frac{-2U_0}{(-\beta)^n \pi \Gamma(n-m)} \int_0^{2\pi} \cos n\theta \, d\theta \\ &\quad \int_{-L_0}^{\xi} d\xi_1 \int_{h_0(\theta, \xi_1)}^{h_1(\theta, \xi_1)} d\eta (\xi - \xi_1)^{n-m-1} \lambda_u(\xi_1 + \eta \sin \mu, \eta \cos \mu) \cos \mu\end{aligned}$$

Change the  $\xi_1, \eta$  coordinates back to the  $x, y$  system by means of equation (26) and this becomes

$$\alpha_n^{(m)}(\xi) = \frac{-2U_0}{(-\beta)^n \pi \Gamma(n-m)} \int_0^{2\pi} \cos n\theta \, d\theta \int \int_{S_\xi} (\xi - x + \beta y \cos \theta)^{n-m-1} \lambda_u(x, y) dx dy$$



The area  $S_\xi$ , shown in sketch (k), becomes independent of  $\theta$  when  $\xi = L_0$  (being then just the area of the wing itself), therefore

$$\alpha_n^{(m)}(L_0) = \frac{-2U_0}{(-\beta)^n \pi \Gamma(m-n)} \iint_S \lambda_u(x,y) dx dy$$

$$\int_0^{2\pi} (L_0 - x + \beta y \cos \theta)^{n-m-1} \cos n\theta d\theta = 0$$

since, for  $m < n$

$$\int_0^{2\pi} \cos^m \theta \cos n\theta d\theta = 0$$

Hence, for the  $\alpha_n(\xi)$  defined by equation (36)

$$\alpha_n^{(n)}(L_0) = \alpha_n^{(n-1)}(L_0) = \alpha_n^{(n-2)}(L_0) = \dots = \alpha_n(L_0) = 0 \quad (38)$$

#### AIRPLANE SHAPE

In the previous section a connection was established between multipole distributions and their resulting wave drag. Further, this connection was direct and relatively simple if the strengths and positions of the distributions were given. Unfortunately the connection between the multipoles and the shape of the simulated surface is generally not so simple. Such a relation does certainly exist, however, and if the strengths of the multipoles are known, the relationship is again direct. That is, a given distribution of multipoles yields directly, by the formulas given in the previous section, the induced velocities everywhere in the flow field; these, in turn, fix the stream surfaces along any one of which (since, of course, the theory neglects viscosity) a physical surface can be imagined.

In general, if

$$\left. \begin{aligned} F_c(x,y,z) &= 0 \\ F_p(x,r,\theta) &= 0 \end{aligned} \right\} \quad (39)$$

are the equations of a stream surface in Cartesian and polar coordinates, respectively, then the equations

$$\left. \begin{aligned} (U_0 + \varphi_x) \frac{\partial F_c}{\partial x} + \varphi_y \frac{\partial F_c}{\partial y} + \varphi_z \frac{\partial F_c}{\partial z} &= 0 \\ (U_0 + \varphi_x) \frac{\partial F_p}{\partial x} + \varphi_r \frac{\partial F_p}{\partial r} + \frac{1}{r^2} \varphi_\theta \frac{\partial F_p}{\partial \theta} &= 0 \end{aligned} \right\} \quad (40)$$

must hold.

For example, in studies of thin wings lying in a plane, the particular form of equation (39)

$$z - h(x, y) = 0$$

is assumed and equation (40) becomes

$$-(U_0 + \varphi_x) \frac{\partial h}{\partial x} - \varphi_y \frac{\partial h}{\partial y} + \varphi_z = 0$$

or, neglecting second-order effects,

$$\frac{\partial h}{\partial x} = \frac{1}{U_0} \varphi_z$$

which is the familiar boundary condition used in thin-airfoil theory. On the other hand, if the equation of the body shape is written in the form

$$r - R(x, \theta) = 0$$

then equation (40) becomes, for linearized theory,

$$U_0 \frac{\partial R}{\partial x} = \varphi_r - \frac{\varphi_\theta}{R^2} \frac{\partial R}{\partial \theta} \quad (41)$$

If the flow field is radially symmetrical or if the body surface is

quasi-cylindrical, equation (41) reduces to

$$\frac{\partial R}{\partial x} = \frac{1}{U_0} \varphi_r \quad (42)$$

which is the familiar boundary condition used in the study of quasi-cylindrical bodies or bodies of revolution.

In general, a nonlinear partial differential equation of the first order such as equation (41) can be reduced to two simultaneous, ordinary, nonlinear differential equations of the first degree (see, e.g., ref. 8). Thus equation (41) becomes

$$\left. \begin{aligned} \frac{d\theta}{dx} &= \frac{1}{U_0 R^2} \varphi_\theta(x, R, \theta) \\ \frac{dR}{dx} &= \frac{1}{U_0} \varphi_r(x, R, \theta) \end{aligned} \right\} \quad (43)$$

and if  $\varphi_\theta$  and  $\varphi_r$  are known functions of  $x$ ,  $R$ , and  $\theta$ , these can be solved numerically.

If the strengths of all rectilinear multipoles and source sheets are given, equation (19) or (24) can be used to find  $\varphi_r$  and  $\varphi_\theta$  at arbitrary field points. Hence, the first step in finding the body shapes reduces to that of integrating such equations. However, these integrations are difficult and tedious even when entirely numerical procedures are employed and the results still have to be interpreted in terms of the body shape according to equations (43). Therefore, from a practical viewpoint, it is necessary to study certain approximate methods for obtaining the velocity field.

Let attention be concentrated on the disturbances created by a line of multipoles. In particular, consider the fields induced by simple polynomial distributions satisfying, in each case, the end conditions given by equation (17). For particular variations set

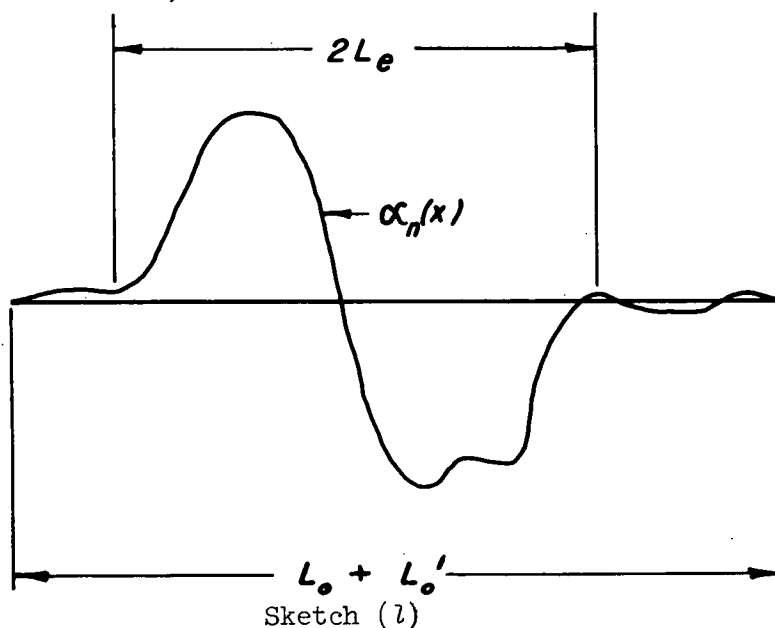
$$\left. \begin{aligned} a_0(\bar{x}) &= c_0(1 - \bar{x}^2)\bar{x} \\ a_2(\bar{x}) &= c_2(1 - \bar{x}^2)^3\bar{x} \\ a_4(\bar{x}) &= c_4(1 - \bar{x}^2)^5\bar{x} \end{aligned} \right\} \quad (44)$$

where  $c_0$ ,  $c_2$ , and  $c_4$  are constants determining the amplitudes and  $\bar{x} = x/L_0$ . Figure 1(a) shows the variations of these coefficients with  $\bar{x}$ , and figures 1(b) through 1(f) show how velocities induced by these distributions vary with  $\bar{x}_0 (x_0 = x - \beta r)$  and  $\bar{r} (\bar{r} = \beta r/L_0)$ . The results have been compared with those for large  $\bar{r}$  given by equation (21) and with those for small  $\bar{r}$  given by slender-body theory. Values for the latter theory are determined from equations (9) or (19) by expanding the expressions in powers of  $r$  and neglecting all but the first terms. Thus it can be shown

$$\varphi_{nr})_{r \rightarrow 0} = \begin{cases} \frac{a_0(x)}{2\pi r}, & n = 0 \\ \frac{(-2)^n n! a_n(x) \cos n\theta}{4\pi r^{n+1}}, & n > 0 \end{cases} \quad (45a)$$

$$\left(\frac{1}{r} \varphi_{n\theta}\right)_{r \rightarrow 0} = \frac{(-2)^n n! a_n(x) \sin n\theta}{4\pi r^{n+1}}, \quad n \geq 0 \quad (45b)$$

The significance of figure 1 with regard to practical applications is more or less obvious. The first step in its use is to find the effective length of the cancellation-multipole distributions. Since the wing is given, the streamwise variation of the cancellation multipoles can be



calculated. Actually this variation will extend between the apexes of the enclosing Mach forecone and aftercone, a distance of  $L_0 + L_0'$  (see sketch (k)). However, depending on the wing plan form and section, the effective lengths of the distributions (the interval of principal variation) can be considerably less as illustrated in sketch (l)). Designate this effective length as  $2L_e$  and the distance to the vicinity of the body surface as  $r_e$ , and one can define

the parameter  $\bar{r}_e$  thus

$$\bar{r}_e = \frac{\beta r_e}{L_e} \quad (46)$$

Using figure 1 and the parameter  $\bar{r}_e$ , one can now estimate the error incurred by the use of various approximate methods for calculating the body shape. A convenient way to carry out these estimations is to study the magnitude of the first crest of the waves shown in figures 1(b) through 1(f), and the distance this crest lies from the foremost Mach cone. Graphs showing the variations of these quantities with  $\bar{r}$  are given in figures 2, 3, and 4.

By means of the above concepts, let us study briefly four different approximate methods that can be used to calculate a body shape.

### Slender-Body Theory

Slender-body theory is represented in figure 3 by the straight lines having the slopes, on the log-log scale, equal to  $-(n+1)$  where  $n$  is the order of the multipole. Since this theory amounts to an expansion of the equations for the velocities in powers of  $\bar{r}$ , it obviously represents a good approximation when  $\bar{r}_e$  is sufficiently small. Notice that for a given percentage error the limiting value of  $\bar{r}_e$  for which the method applies increases as the order of the multipoles increases. For example, when  $\bar{r}_e = 0.2$ ,  $\phi_{0r}$  as given by slender-body theory is 19 percent less than that given by exact linearized theory for the case shown, whereas  $\phi_{2r}$  is only 3 percent less. Correspondingly, the positions of the wave crests follow the path predicted by slender-body theory to larger values of  $\bar{r}$  as the order of the multipoles increases. The latter trend is illustrated by figure 4.

If for a particular problem  $\bar{r}_e$  is small enough for slender-body theory to be considered a good approximation, the equation for the body shape,  $r = R(x, \theta)$ , corresponding to the combined wing and optimum cancellation multipoles defined in equation (36) is determined by the expression (using equations (45), (36), and (14) together with equation (42))

$$\frac{d\theta}{dx} = \left[ \frac{\phi_\theta(x, R, \theta)}{U_\infty R^2} \right]_{\text{wing}} + \sum_0^\infty \frac{\left(\frac{2}{\beta}\right)^n \sin n\theta}{4\pi^2 R^{n+2}} \int_0^{2\pi} d\psi \int_{-L_0}^x dx_1 (x - x_1)^n \cos n\psi S_w^n(x, \psi) \quad (47a)$$

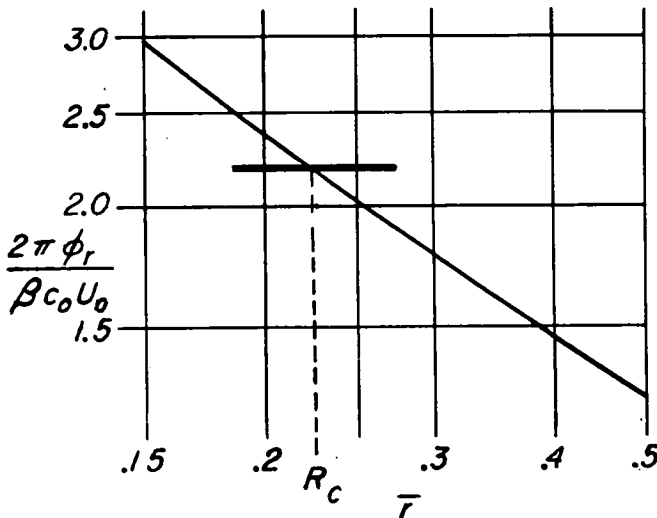
$$\frac{dR}{dx} = \left[ \frac{\phi_r(x, R, \theta)}{U_0} \right]_{\text{wing}} + \sum_0^{\infty} \frac{\left( \frac{2}{\beta} \right)^n \cos n\theta}{4\pi^2 R^{n+1}} \int_0^{2\pi} d\psi \int_{-L_0}^x dx_1 (x - x_1)^n \cos n\psi S_w''(x, \psi) \quad (47b)$$

Approximate methods for finding  $(\phi_\theta/U_0 R^2)_{\text{wing}}$  and  $(\phi_r/U_0)_{\text{wing}}$ , the velocities induced by the wing, can often be used also, but these

**Source distribution given by**

$$a_0 = c_0 U_0 (1 - \bar{x}^2) \bar{x}$$

apply to individual cases and cannot be discussed here.

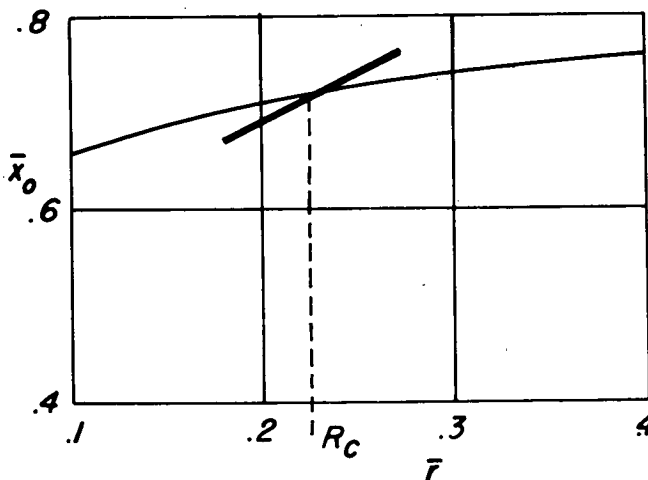


Theory for Large  $\bar{r}_e$

The asymptotic values for magnitude and position of the first wave crest obtained by placing equations (44) into equations (21) are also shown in figures 2, 3, and 4. For  $n \leq 4$  it is clear that this theory can be used when  $\bar{r}_e$  is greater than about 2.

Control-Surface Theory

**Amplitude of first crest**



**Position of first crest**  
Sketch (m)

The approximations inherent in ordinary control-surface theory can also be estimated by inspecting figures 3 and 4, where by control-surface theory one means that the exact linearized theory is used to evaluate induced velocities along a given surface and these values are assumed constant for all  $\bar{r}$  in the vicinity of the surface. As shown in sketch (m), this amounts to assuming  $\phi_r$  and  $\phi_\theta$  are given by a straight horizontal line in figure 3 and by straight lines with a unit negative slope in figure 4. Obviously, the error in the body shape calculated by this theory

increases as the amplitudes of the disturbing multipoles increase and as the radius of the control surface diminishes.

One of the simplest applications of control-surface theory arises in the study of quasi-cylindrical bodies. In such cases the expression for the body surface can be derived immediately from equation (42). Thus, if the amplitudes of the cancellation multipoles are small enough and  $R_c$ , the radius of the control surface, is large enough for control-surface theory to be considered a good approximation, the body shape,  $r = R(x, \theta)$ , corresponding to the combined wing and optimum cancellation multipoles is determined by (using equations (19c), (16b), and (36) together with equation (42))

$$\frac{dR}{dx} = \left[ \frac{\varphi_r(x, R_c, \theta)}{U_0} \right]_{\text{wing}} + \sum_0^{\infty} \frac{\sigma_n \cos n\theta}{4\pi^2 R_c} \int_{-L_0}^{x-\beta R_c} \frac{(x-\xi) \cosh\left(n \cosh^{-1} \frac{x-\xi}{\beta R_c}\right) d\xi}{\sqrt{(x-\xi)^2 - \beta^2 R_c^2}} \int_0^{2\pi} S_w''(\xi, \psi) \cos n\psi d\psi \quad (48)$$

where  $\sigma_n = 1$  for  $n = 0$  and  $\sigma_n = 2$  for  $n > 0$ .

A study of optimum fuselage shapes using control-surface theory has been carried out by Nielsen (ref. 9) for a constant-chord sweptback wing having a biconvex section and a sonic leading edge. The set of interfering singularities used in reference 9 are equivalent (the singularities are limited to the  $x$  axis) to the multipoles used herein. The fuselage shapes calculated by Nielsen are thus the same - within the accuracy of control-surface theory - as those given by equation (48).

#### Modified Control-Surface Theory

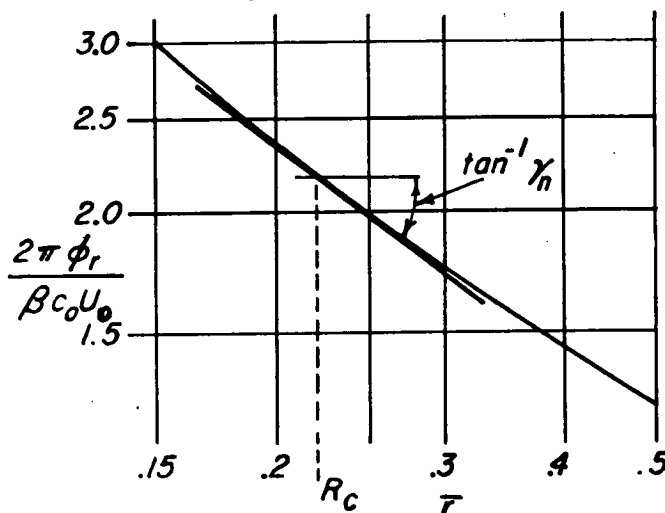
A method of modifying control-surface theory to increase its accuracy is illustrated in sketch (n). Induced velocities computed by this method are based on those calculated along a given control surface but extended away from this surface varying in magnitude as  $(\bar{r})^{\gamma_n}$  where the value of  $\gamma_n$  is fixed by the slope of the curves in figure 3 at

$\bar{r} = \bar{r}_e$ ,  $\bar{r}_e$  being defined by equation (46) (see sketch (n)). With this modification equation (48) becomes

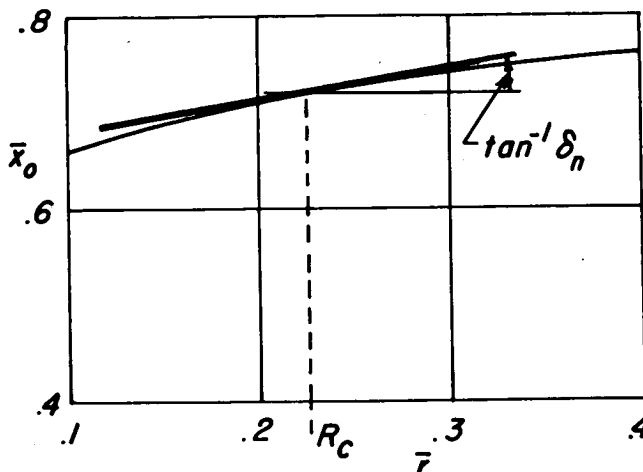
$$\frac{dR}{dx} = \left[ \frac{\phi_r(x, R_c, \theta)}{U_0} \right]_{\text{wing}} + \sum_0^{\infty} \left( \frac{R_c}{R} \right)^{\gamma_n} \frac{\sigma_n \cos n\theta}{4\pi^2 R_c} \int_{-L_0}^{x - \beta R_c} \frac{(x - \xi) \cosh \left( n \cosh^{-1} \frac{x - \xi}{\beta R_c} \right) d\xi}{\sqrt{(x - \xi)^2 - \beta^2 R_c^2}} \int_0^{2\pi} S_w''(\xi, \psi) \cos n\psi d\psi \quad (49)$$

Source distribution given by

$$a_0 = c_0 U_0 (1 - \bar{x}^2) \bar{x}$$



Amplitude of first crest



Position of first crest

Sketch (n)

which can be solved using numerical techniques.

A further refinement of equation (49) can be obtained if the position of the induced velocities is also varied according to the slope (again at  $\bar{r} = \bar{r}_e$ ) of the curves in figure 4. Defining this slope as  $\delta_n$ , see sketch (n), and  $x_\delta$  as

$$x_\delta = x - \beta(1 + \delta_n)(R - R_c)$$

one can see this refinement simply amounts to replacing the value of  $x$  in the right-hand term of equation (49) with  $x_\delta$ .

#### ILLUSTRATIVE EXAMPLE - ELLIPTIC WING

In order that one may be able to assess the practical significance of the preceding sections, the concepts presented therein will now be applied to the solution of a particular problem. For the basic wing plan form in this particular example an ellipse will be



chosen. There are two good reasons for this choice; first, the ellipse is effectively unswept and places a severe test on the role of body interference in reducing the wave drag at a supersonic speed, and, second, for a given volume, the optimum section (i.e., the one yielding minimum wave drag) for these wings when considered separately has been discovered (see ref. 10) so the reduction in wave drag brought about by the body will reduce the minimum value possible for such wings when flying alone. The drag reductions for the first few cancellation-multipole distributions will be calculated and compared with the total drag of the wing alone, the wing mounted on an infinite cylinder, and the wing mounted on a basic body of revolution. Finally the details of calculating a body shape simulated by the wing source sheet, a source line representing a basic body of revolution, and the first two optimum cancellation multipole distributions will be carried out.

### The Elliptic Wing

Consider the elliptic lens specified by the equation

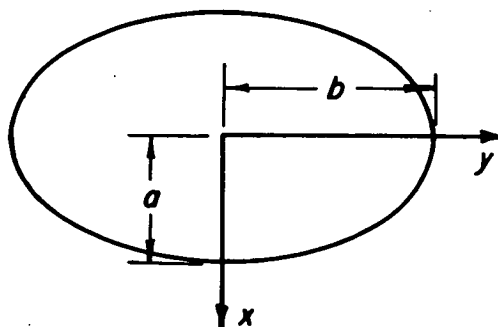
$$z = \pm \frac{t}{2} \left( 1 - \frac{x^2}{a^2} - \frac{y^2}{b^2} \right) \quad (50)$$

where the thickness, span, and chord are shown in sketch (o). The stream-wise slope of the upper surface is seen to be

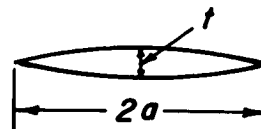
$$\left. \frac{\partial z}{\partial x} \right|_u = \lambda_u(x, y) = - \frac{tx}{a^2} \quad (51)$$

and the total wing plan-form area  $S$  and volume  $V$  are, respectively,

$$\left. \begin{aligned} S &= \pi ab \\ V &= \frac{\pi}{2} tab \end{aligned} \right\} \quad (52)$$



Wing plan form



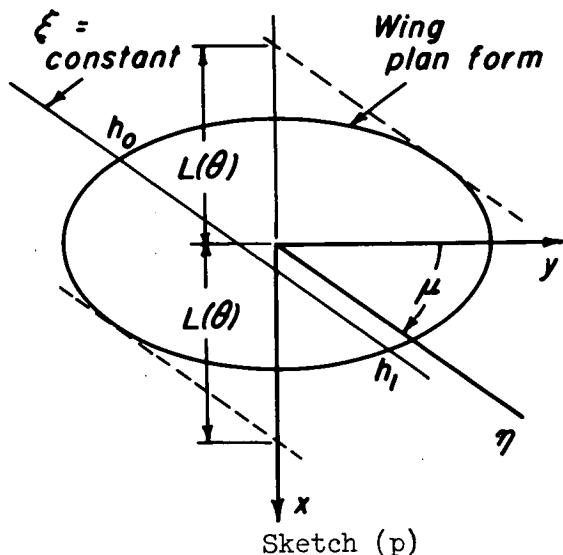
Root section

Sketch (o)

Wave drag.— The wave drag of the elliptic wing represented by equation (50) can be calculated by means of equation (30) in which, since one wishes now to find the wave drag of the wing alone, the  $a_n$ 's are set equal to zero. The value of  $S_w''(x, \theta)$

follows by placing equation (51) into equation (28) and integrating. Thus

$$U_0 S_w'(x, \theta) = 2U_0 \cos \mu \int_{h_0}^{h_1} \left( -\frac{t}{a^2} \right) (\xi + \eta \sin \mu) d\eta = -\frac{2tU_0 \cos \mu}{a^2} \left( \xi \eta + \frac{\eta^2 \sin \mu}{2} \right)_{h_0}^{h_1}$$



where, by referring the equation of the plan form to the  $\xi, \eta$  coordinates (see eq. (26)) and solving for the points where the straight line  $\xi = \text{constant}$  intercepts the wing edges, one finds - see sketch (p)

$$\left. \begin{array}{l} h_1 \\ h_0 \end{array} \right\} = \frac{-b^2 \xi \sin \mu \pm ab \sqrt{a^2 \cos^2 \mu + b^2 \sin^2 \mu - \xi^2 \cos^2 \mu}}{a^2 \cos^2 \mu + b^2 \sin^2 \mu}$$

Hence,

$$S_w'(x, \theta) = - \frac{4xtab}{(a^2 + b^2 \beta^2 \cos^2 \theta)^2} \sqrt{a^2 + b^2 \beta^2 \cos^2 \theta - x^2} \quad (53)$$

From the relation

$$L^2(\theta) = a^2 + b^2 \beta^2 \cos^2 \theta \quad (54)$$

the wave drag can be expressed in the form (integrating once by parts)

$$\frac{D}{q} = - \frac{1}{4\pi^2} \int_0^{2\pi} d\theta \int_{-L(\theta)}^{L(\theta)} d\xi_1 \int_{-L(\theta)}^{L(\theta)} d\xi_2 \left[ \frac{4xtab}{L^4(\theta)} \right]^2 \left[ \frac{L^2(\theta) - 2\xi_1^2}{\sqrt{L^2(\theta) - \xi_1^2}} \right] \frac{\xi_2 \sqrt{L^2(\theta) - \xi_2^2}}{\xi_1 - \xi_2}$$

Further integration yields

$$\frac{D}{q} = t^2 a^2 b^2 \int_0^{2\pi} \frac{d\theta}{(a^2 + b^2 \beta^2 \cos^2 \theta)^2}$$

Finally, the wave drag can be expressed in coefficient form, based on the total wing area  $\pi ab$ , as

$$C_D = \frac{4}{\beta} \left( \frac{t}{2a} \right)^2 \frac{1 + 2 \left( \frac{a}{b\beta} \right)^2}{\left[ 1 + \left( \frac{a}{b\beta} \right)^2 \right]^{3/2}} \quad (55)$$

Equation (55) represents the lowest value of wave drag possible for a wing having an elliptic plan form and fixed volume. This equation was first derived by Jones in reference 10.

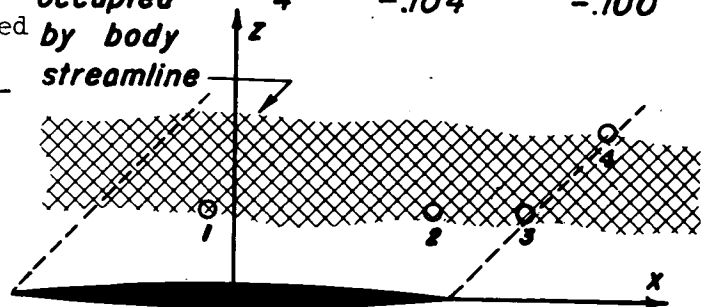
The velocities induced by the wing source sheet in the vicinity of the fuselage.— Later, when one wishes to calculate a stream surface in the presence of the source sheet that simulates the wing given by equation (50), it is necessary to know the velocities induced by these sources at the body surface. Hence, the value of  $\phi_r$  induced by the source sheet was calculated at the four points indicated in sketch (q).

As it turns out, these values are so close (see the sketch for a numerical comparison) to those obtained by assuming the source sheet to be two-dimensional with a chordwise intensity identical to that along the root section of the elliptical sheet (i.e., using the Ackeret wave generated by the root section) that the effect of the wing can be assumed to be given everywhere in the vicinity of the body by the latter velocity field if (as will be the case in subsequent application) the surface of the body passes through the region shaded in the sketch. That is, the effect of the wing in the equations for the fuselage shape (such as eqs. (47), (48), or (49)) is assumed to be

Values of  $\phi_r / U_0$

Point number	Exact linearized theory	Ackeret wave — $t(x-r)/a^2$
1	.044	.050
2	-.053	-.050
3	-.102	-.100
4	-.104	-.100

Region to be occupied by body streamline



Sketch (q)

$$\left. \begin{aligned} \frac{1}{U_0} \phi_r &= \mp \frac{t}{a^2} (x \mp \beta r \sin \theta) \sin \theta, & \begin{aligned} &- \text{ for } 0 \leq \theta \leq \pi \\ &+ \text{ for } \pi \leq \theta \leq 2\pi \end{aligned} \\ \frac{1}{rU_0} \phi_\theta &= \mp \frac{t}{a^2} (x \mp \beta r \sin \theta) \cos \theta, & \begin{aligned} &- \text{ for } 0 < \theta < \pi \\ &+ \text{ for } \pi < \theta < 2\pi \end{aligned} \end{aligned} \right\} \quad (56)$$

### The Optimum Cancellation Multipole

One can now find the strengths of the multipoles along the  $x$  axis which induce around a cylinder of infinite radius a momentum field identical to that created there by the elliptic wing. The negatives of these variations are, according to equation (36), the optimum cancellation multipoles. Hence, combining equations (53) and (36)

$$\alpha_n^{(n)}(x) = -\sigma_n \frac{2tabU_0x}{\pi(-\beta)^n} \int_0^{2\pi} \frac{\sqrt{a^2 + b^2\beta^2\cos^2\theta - x^2}}{(a^2 + b^2\beta^2\cos^2\theta)^2} \cos n\theta \, d\theta \quad (57)$$

where  $\sigma_n = 1$  for  $n = 0$  and  $\sigma_n = 2$  for  $n > 0$ . Particular variations of  $\alpha_n^{(n)}(x)$  are shown in figure 5. These results are for  $n = 0, 2$ , and  $4$ , since  $\alpha_n^{(n)}(x)$  for any odd  $n$  is zero by symmetry, and apply when the wing plan form and free-stream Mach number are related by

$$\frac{a}{b\beta} = \frac{4}{3\pi} \quad (58)$$

which contains the particular case for which the Mach number is  $\sqrt{2}$  and the aspect ratio is 3. It is apparent that there are at least  $n + 1$  roots to  $\alpha_n^{(n)}(x)$  for  $-L_0 < x < L_0$ . This follows immediately from equation (38) and is true in general. As a result the curves for the higher values of  $n$  become increasingly wavy and, correspondingly, increasingly difficult to evaluate numerically.

Figure 6 presents the values of  $\alpha_n(x)$  for the same elliptic-wing Mach number relation given by equation (58). Notice that each of these curves has only one root (they necessarily have at least one) in the interval  $-L_0 < x < L_0$  and is increasingly smooth with increasing  $n$ . The latter follows from equation (37) and the fact that the first  $n$  derivatives of these curves must, in general, be continuous. For example, at  $x = \pm L_0$  the first four derivatives of  $\alpha_4(x)$  must vanish.

Wave drag. - One can now calculate how much the wing-alone drag is reduced when combined with each successive optimum cancellation-multipole distribution. If  $\bar{D}_n$  denotes the drag saved by the  $n$ th-order cancellation multipoles, then by equation (35)

$$\frac{\bar{D}_n}{q} = - \frac{\beta^{2n}}{4\pi U_0^2} \int_{-L_0}^{L_0} dx_1 \int_{-L_0}^{L_0} dx_2 \alpha_n^{(n+1)}(x_1) \alpha_n^{(n+1)}(x_2) \ln|x_1 - x_2| \quad (59)$$

where  $L_0$  is the maximum value of  $L(\theta)$  as given by equation (54)

$$L_0^2 = a^2 + b^2 \beta^2 \quad (60)$$

The total drag saved by means of the first  $m$  multipole distributions, would, by equation (34), be

$$\bar{D} = 2\bar{D}_0 + \sum_{n=1}^m \bar{D}_n \quad (61)$$

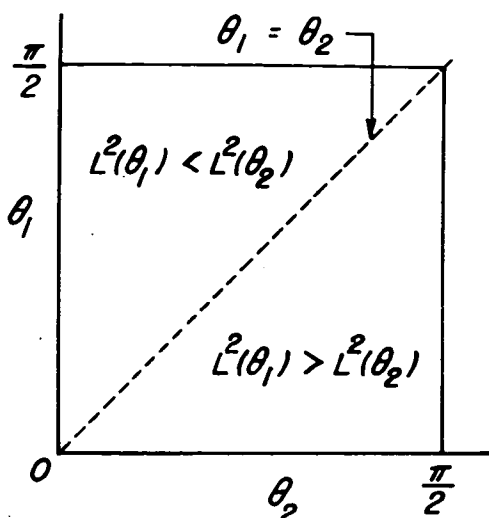
Using equations (53) and (36) to define the  $\alpha_n^{(n+1)}(x)$  in equation (59), reversing the order of integration, and integrating once by parts, one finds

$$\frac{\bar{D}_n}{q} = \frac{-4}{\pi^2} \int_0^{\pi/2} \cos n\theta_1 d\theta_1 \int_0^{\pi/2} \cos n\theta_2 d\theta_2 \int_{-L(\theta_1)}^{L(\theta_1)} d\xi_1 \int_{-L(\theta_2)}^{L(\theta_2)} d\xi_2$$

$$\frac{(4\text{tab})^2}{L^4(\theta_1)L^4(\theta_2)} \frac{L^2(\theta_1) - 2\xi_1^2}{\sqrt{L^2(\theta_1) - \xi_1^2}} \frac{\xi_2 \sqrt{L^2(\theta_2) - \xi_2^2}}{\xi_1 - \xi_2}$$

$$= - \frac{64(\text{tab})^2}{\pi^3} \int_0^{\pi/2} \cos n\theta_1 d\theta_1 \int_0^{\pi/2} \cos n\theta_2 d\theta_2$$

$$\begin{cases} -\pi^2/4L^4(\theta_2), & L^2(\theta_1) \leq L^2(\theta_2) \\ -\pi^2/4L^4(\theta_1), & L^2(\theta_1) \geq L^2(\theta_2) \end{cases}$$



Sketch (r)

It is apparent from sketch (r) that this can be written

$$\frac{\bar{D}_n}{q} = \frac{16(\text{tab})^2}{\pi} \left[ \int_0^{\pi/2} \frac{\cos n\theta_1 d\theta_1}{L^4(\theta_1)} \int_{\theta_1}^{\pi/2} \cos n\theta_2 d\theta_2 + \int_0^{\pi/2} \cos n\theta_1 d\theta_1 \int_0^{\theta_1} \frac{\cos n\theta_2}{L^4(\theta_2)} d\theta_2 \right]$$

or

$$\frac{\bar{D}_n}{q} = \frac{32(\text{tab})^2}{\pi} \int_0^{\pi/2} \frac{\cos n\theta_1 d\theta_1}{(a^2 + b^2\beta^2\cos^2\theta_1)^2} \int_{\theta_1}^{\pi/2} \cos n\theta_2 d\theta_2 \quad (62)$$

The total drag saved by using all the cancellation multipoles is, by definition,

$$\frac{\bar{D}}{q} = \frac{16(\text{tab})^2}{\pi} \int_0^{\pi/2} \frac{d\theta_1}{(a^2 + b^2\beta^2\cos^2\theta_1)^2} \left( \frac{\pi}{2} - \theta_1 - \sum_{n=1}^{\infty} \frac{1}{n} \sin 2n\theta_1 \cos 2n\theta_1 \right)$$

and since

$$x = \frac{\pi}{4} - \sum_{n=1}^{\infty} \frac{1}{n} \sin 2nx \cos 2nx$$

this is equal to the drag of the wing alone, as it, of course, should be.

The reduction in wave drag as the wing is combined with the first three optimum cancellation multipoles is presented in figure 7. In studying figure 7, one sees, as the Mach number approaches one (i.e.,  $\beta \rightarrow 0$ ), more and more of the original wing wave drag is destroyed by a line of simple sources alone. Further, the value of  $\bar{r}_e$  which can be written - see equations (46), (54), and figures 5 and 6 -

$$\bar{r}_e = \frac{\beta r_e}{\sqrt{a^2 + b^2 \beta^2}} \quad (63)$$

tends (for a fixed average distance to the body surface  $r_e$ ) to zero as the Mach number approaches one; and this, in turn, means that as  $\beta$  goes to zero the effect of the multipole strengths on the body shape can be calculated using slender-body theory.

When various orders of multipoles are distributed along a line, one can show the cross-sectional area normal to the free stream of the simulated body as given by slender-body theory is a function of the source distribution only (see Appendix B). Coupled with the discussion in the preceding paragraph, this can be used to demonstrate that, for Mach numbers close to one, the "supersonic area rule" proposed in reference 11 and discussed in reference 12 gives a good approximation for the wave drag of an elliptic wing and body combination which is symmetrical with respect to the plane of the wing.

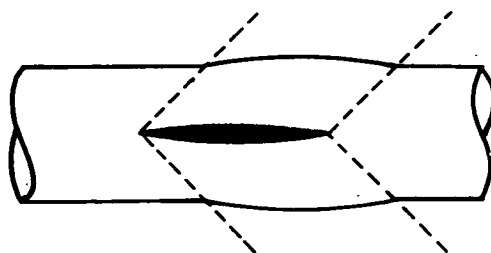
The induced velocity field.— A method for calculating the velocity field induced by the multipoles when  $\alpha_n(x)$  is given numerically is presented in Appendix C. By means of this method, velocities induced by the  $\alpha_0$  and  $\alpha_2$  multipole distributions shown in figure 6 have been calculated for  $\bar{r}$  equal to 0.148 and the results are shown in figure 8. Since the distributions in figure 6 were for the particular case  $a/b\beta = 4/3\pi$ , it is evident from equation (63) that the values in figure 8 apply to the case  $r_e/b$  equal to 0.161; that is, when the body radius is about 16 percent of the wing semispan.

For comparative purposes, the values given by slender-body theory are also shown in figure 8. The degree of agreement between the two curves is consistent with the results shown in figures 3 and 4.

#### Interpretation of Drag Reductions

Comparison with wing mounted on a circular cylinder.— With regard to figure 7 one should be careful to notice that the drag of the wing alone has been used for the reference drag. The drag reductions shown, therefore, represent gains brought about by interfering with the velocity field induced by a planar source sheet, or, in terms of a combination with an upstream cylindrical stream surface, gains made by modifying a body, shown in sketch (s), which bulges behind

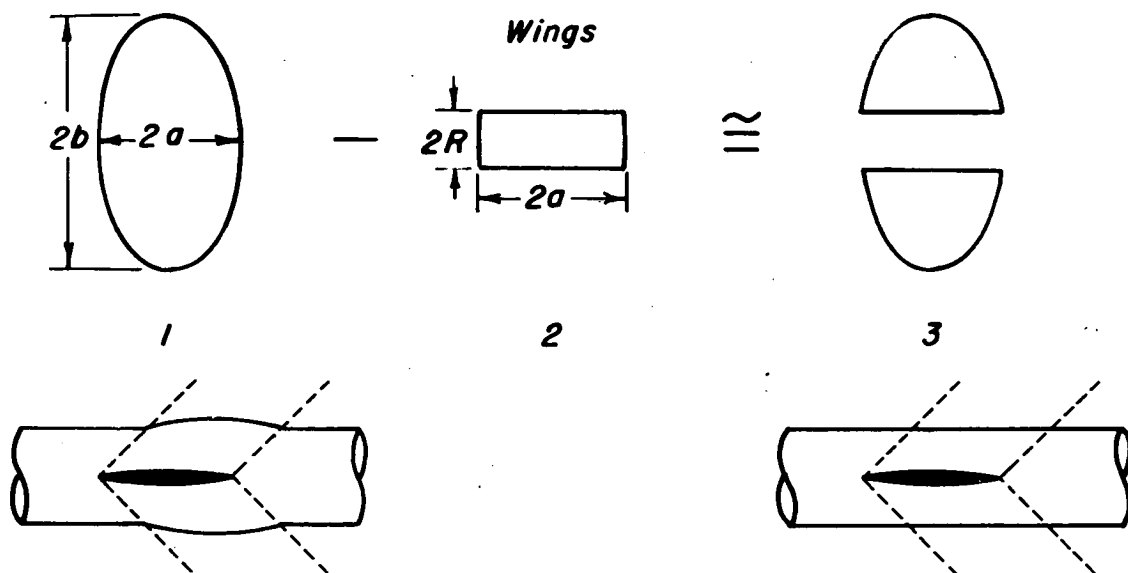
----- *Mach waves from wing root section*



Sketch (s)

the wing leading-edge Mach wave in accordance with the velocities induced there by the source sheet. Obviously, from this viewpoint, a considerable reduction in drag can be brought about merely by eliminating the bulge, thereby making the body a circular cylinder throughout. Mathematically, such a procedure amounts to using a certain set<sup>8</sup> of cancellation multipoles along the  $x$  axis behind the point  $-L_0$ , and, if the drag of this resulting combination were used as a reference, the gains shown in figure 7 would be diminished..

An approximate way to estimate the drag of a wing mounted on a circular cylinder is illustrated in sketch (t) and consists merely of subtracting from the wing source sheet those sources blanketed by the body.



Sketch (t)

Using the subscripts 1, 2, and 3 to designate the wave drags of the individual wings as indicated in the sketch, Jones (in an unpublished communication) has shown that if wing 1 is an elliptic wing with a biconvex section and wing 2 lies entirely within the plan form of wing 1, then

$$D_3 = D_1 \left( 1 + \frac{2V_2}{V_1} \right) + D_2 \quad (64)$$

where  $V_2$  and  $V_1$  are the volumes of wings 1 and 2, respectively.

<sup>8</sup>The exact evaluation of multipole distributions necessary to simulate a circular cylinder for the entire body length has been studied in reference 13.



For a supersonic Mach number,  $D_2$  is closely approximated by the wave drag of a rectangular wing having the same section and aspect ratio. If  $A_2$ ,  $4R_a$ , and  $\tau_2$  are, respectively, the aspect ratio, plan-form area, and thickness ratio of the rectangular wing, its drag can be expressed in the form

$$\frac{\beta D_2}{q\tau_2^2} = 4R_a N_2 \quad (65)$$

where

$$N_2 = \begin{cases} \frac{16}{\pi} \beta A_2 \left[ \frac{2}{3} \frac{\sin^{-1} \beta A_2}{\beta A_2} - \frac{\sqrt{1 - \beta^2 A_2^2}}{6} + \left(1 - \frac{\beta^2 A_2^2}{6}\right) \cosh^{-1} \frac{1}{\beta A_2} \right], & \beta A_2 \leq 1 \\ \frac{16}{3}, & \beta A_2 \geq 1 \end{cases} \quad (66)$$

Further, if  $A_1$  is the aspect ratio of the elliptic wing, one can show - see sketch (t) and equation (52) -

$$\beta A_2 = \frac{\pi}{4} \left( \frac{R}{b} \right) \beta A_1 \quad (67)$$

The drag of the elliptic wing follows from equation (55) and can be written

$$\frac{\beta D_1}{q\tau_2^2} = 4ab N_1 \quad (68)$$

where

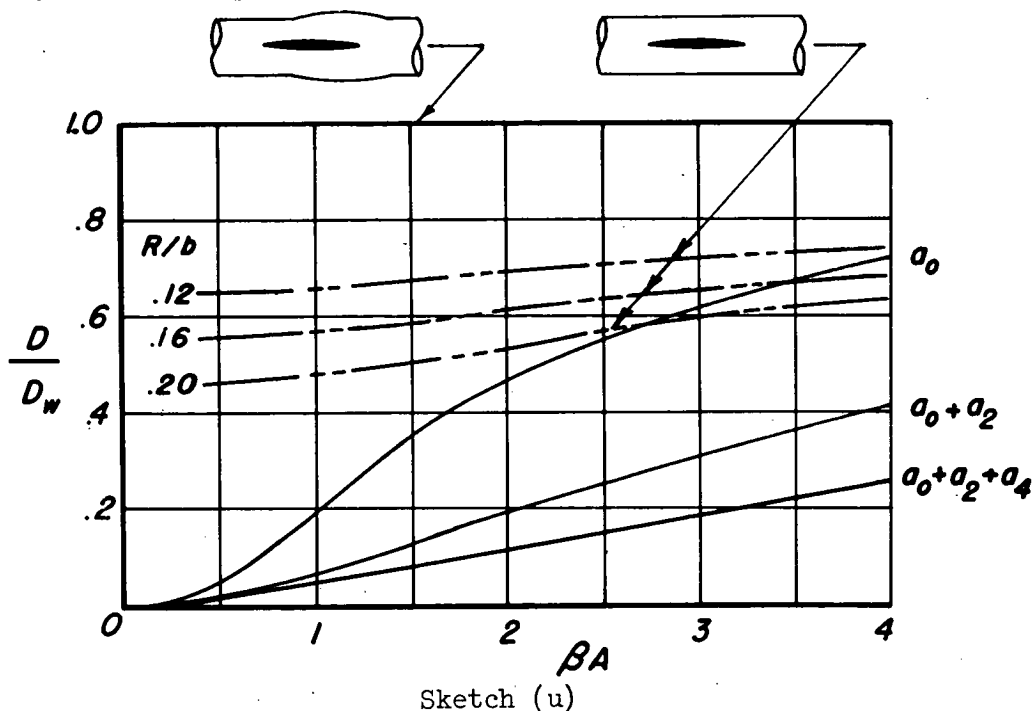
$$N_1 = \pi \frac{1 + 2 \left( \frac{4}{\pi \beta A_1} \right)^2}{\left[ 1 + \left( \frac{4}{\pi \beta A_1} \right)^2 \right]^{3/2}} \quad (69)$$

Finally, therefore, equation (64) can be put in the form

$$\frac{D_3}{D_1} = \left[ 1 - \frac{32}{3\pi} \left( \frac{R}{b} \right) \right] + \frac{R}{b} \frac{N_2}{N_1} \quad (70)$$

and the ratio  $N_2/N_1$  is a function of the parameters  $R/b$  and  $\beta A_1$  only.

By means of equation (70), the dashed curves shown in sketch (u) -



representing approximately the wave drag of a wing mounted centrally on a circular cylinder - were calculated. Though considerable drag reduction is indicated by adding just those multipoles necessary to make the body cylindrical, it is apparent the total wave drag can be reduced further, for the range of parameters shown, by using only the first two optimum cancellation-multipole distributions,  $\alpha_0(x)$  and  $\alpha_2(x)$ , given by equation (36).

#### Comparison with wing mounted on a basic body of revolution.-

Sketch (u) shows the effect on the wave drag of adding the optimum cancellation multipoles either to the wing alone or to the combination of an infinite circular cylinder and a centrally mounted wing. Estimates of their effect when added to a wing mounted on a basic body of revolution can also be carried out. In order to present these estimates, however, the results of the following two theorems due to R. T. Jones are needed.

1. Designate the closed body of revolution which, by a slender-body theory, has a minimum drag for a fixed volume and length as a Sears-Haack body. Then the total wave drag of a Sears-Haack body and any other body of revolution or any centrally mounted thin wing which lie entirely within the Sears-Haack body's enclosing Mach forecone and aftercone is given by the equation

$$D = D_{SH} \left( 1 + \frac{2V_2}{V_{SH}} \right) + D_2 \quad (71)$$

where:

$D_{SH}$  wave drag of Sears-Haack body alone

$D_2$  wave drag of other body or (exposed) wing alone

$V_{SH}$  volume of Sears-Haack body

$V_2$  volume of other body or (exposed) wing

2. Designate the closed body which, by slender-body theory, has a minimum drag for a fixed base diameter and length as a Kármán ogive. Then the total wave drag of a Kármán ogive and any other slender body of revolution or any centrally mounted thin wing which lie entirely within the ogive's enclosing Mach forecone and aftercone is given by the equation

$$D = D_K + D_2 \quad (72)$$

where:

$D_K$  wave drag of Kármán ogive alone

$D_2$  wave drag of other body or (exposed) wing alone

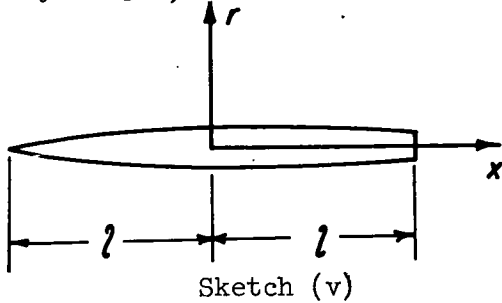
In order that the theoretical results could be tested by wind-tunnel experiments, a basic body of revolution having a finite base area was chosen. Such a body can be simulated by a combination of the source distributions which produce,<sup>9</sup> separately,

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<sup>9</sup>The source distributions simulate the Sears-Haack body and the Kármán ogive only when slender-body theory is used to calculate the body shapes. If linearized theory is used instead, the body shape will, of course, be somewhat different. However, the subsequent results and conclusions are by no means limited by the assumptions pertaining to slender-body theory. The latter theory is used only to obtain an estimate of the body volumes or to study cases for which it gives results that are not significantly different from those given by linearized theory.

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the Sears-Haack body and the Kármán ogive. Thus, if  $2l$  is to be the body length, the line of sources



$$\frac{a_0(x)}{U_0} = \frac{2}{\pi l^3} \left( V_K - 4V_{SH} \frac{x}{l} \right) \sqrt{l^2 - x^2} \quad (73)$$

simulates (by slender-body theory) a body of revolution (see sketch (v)) having a total volume  $V$  equal to  $V_{SH} + V_K$ , a cross-sectional area given by

$$S(x) = \frac{V_K}{\pi l^3} \left[ x \sqrt{l^2 - x^2} + l^2 \left( \frac{\pi}{2} + \sin^{-1} \frac{x}{l} \right) \right] + \frac{8V_{SH}}{3\pi l^4} (l^2 - x^2)^{3/2}, \quad -l \leq x \leq l \quad (74)$$

and a base area  $S(l)$  equal to  $V_K/l$ .

The wave drag of a wing mounted on this basic, unmodified body will now be calculated. Just as was the case in studying the wing attached to an infinite cylinder, the assumption is made that the wave drag of this combination is the same as the wave drag on the configuration simulated by superimposing the singularity distributions which create separately the exposed wing panels and the body of revolution. With this assumption, the wave drag can be written explicitly in terms of the wing and body geometry by applying equations (71) and (72). Hence,

$$D = D_K + D_{SH} \left( 1 + \frac{2V_3}{V_{SH}} \right) + D_3 \quad (75)$$

where  $D_3$  is the drag of the exposed wing panels alone, given by equation (70) and shown for various values of  $R/b$  in sketch (u), and  $V_3$  is their volume (see sketch (t))

$$V_3 = \text{tab} \left( \frac{\pi}{2} - \frac{8}{3} \frac{R}{b} \right) \quad (76)$$

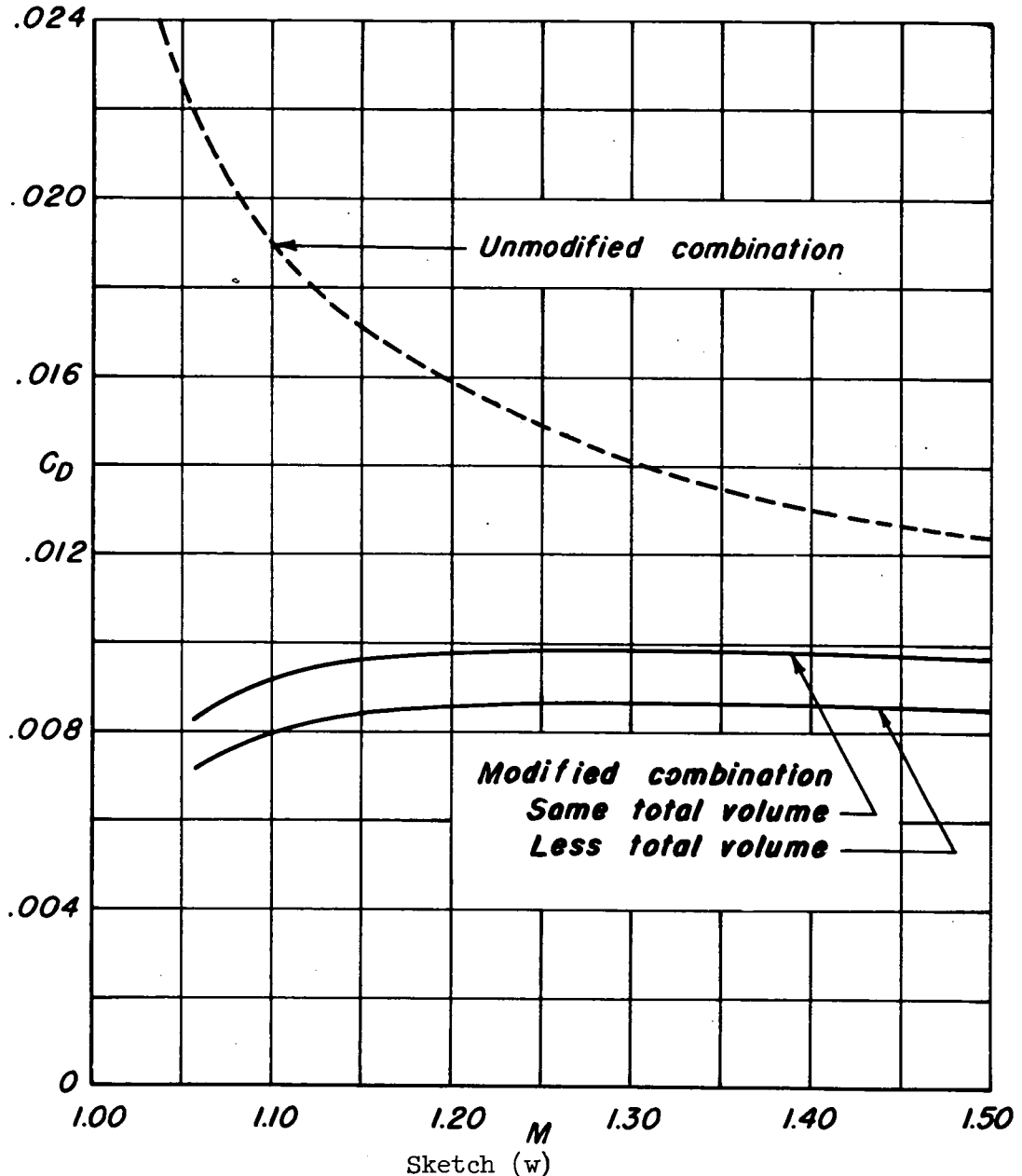
Since  $D_K$  and  $D_{SH}$ , the wave drags of a Kármán ogive and a Sears-Haack body flying alone, are well known to be

$$\left. \begin{aligned} D_K &= \frac{q}{\pi} \frac{V_K^2}{l^4} \\ D_{SH} &= \frac{8q}{\pi} \frac{V_{SH}^2}{l^4} \end{aligned} \right\} \quad (77)$$

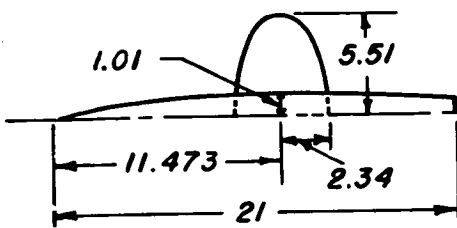
the wave drag coefficient of the unmodified combination, based on the complete wing area  $\pi ab$ , can be expressed as

$$\frac{D}{q\pi ab} = C_D = \frac{V_K^2 + 8V_{SH}^2}{\pi^2 l^4 ab} + \frac{16tV_{SH}}{\pi^2 l^4} \left( \frac{\pi}{2} - \frac{8}{3} \frac{R}{b} \right) + \frac{t^2 N_1}{\pi a^2 \beta} \left[ \left( 1 - \frac{32}{3\pi} \frac{R}{b} \right) + \frac{R}{b} \frac{N_2}{N_1} \right] \quad (78)$$

where  $N_1$  and  $N_2$  are defined in terms of Mach number and wing-body geometry in equations (66) and (69). An example of the variation of  $C_D$  with Mach number for the particular combination shown in sketch (x) ( $R/b$  was set equal to 0.181) is given by the dashed line in sketch (w).



It is now possible to find how much the drag of this unmodified combination can be reduced by means of the optimum cancellation-multipole distributions used to derive the results shown in figure 7. Again applying equations (71) and (72), one can show



**Maximum thickness of wing along center line,  $t$ , = 0.234**

**Total volume of body = 44.60**

$$V_{SH} = 31.72$$

$$V_K = 12.88$$

Sketch (x)

a specific value of  $\beta A_1$  and a specific number of multipole types, one can readily show

$$D_4 = \frac{t^2 b q}{\beta a} N_1 N_4 \quad (80)$$

where  $N_1$  is defined in equation (69). Hence, the drag of the unmodified combination can be reduced to either

$$\frac{D}{q \pi a b} = C_D = \frac{1}{\pi^2 a b l^4} \left\{ V_K^2 + 8 \left[ V_{SH} + t a b \left( \frac{\pi}{2} - \frac{8}{3} \frac{R}{b} \right) \right]^2 \right\} + \frac{t^2}{\pi a^2 \beta} N_1 N_4 \quad (81)$$

if the same total volume is maintained (maintained, as is obvious from an inspection of the equation, by increasing the value of the Sears-Haack portion of the basic body an amount equal to the volume of the exposed wing) or to

$$C_D = \frac{1}{\pi^2 a b l^4} \left( V_K^2 + 8 V_{SH}^2 \right) + \frac{t^2}{\pi a^2 \beta} N_1 N_4 \quad (82)$$

if the volume of the fuselage is reduced by an amount equal to the wing volume.

The results expressed by equations (80) and (81), when applied to the first two optimum cancellation-multipole distributions, are shown for the geometrical parameters presented in sketch (x) by the solid curves in sketch (w). The value of  $R/b$  used for the solid curves was 0.161 instead of the 0.181 value used to calculate the dashed curve. The smaller value was used since the modified body is drawn in along the sides by the cancellation multipoles (see fig. 9), decreasing the average body radius in the wing region from about 1.00 to about 0.89. One must be careful to notice that the solid curves represent minimum (relative to the special method being discussed) values which can be obtained by

a specific design at a specific Mach number and do not represent the variation of wave drag with Mach number for any given combination.

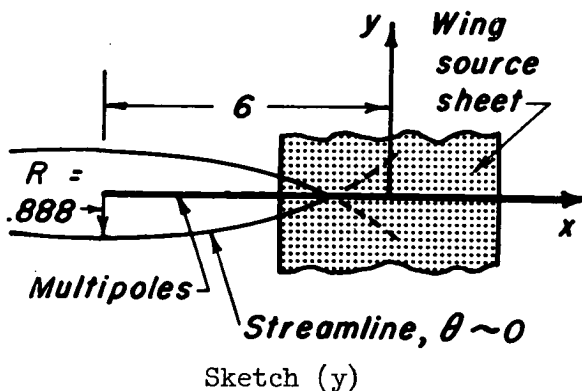
### The Body Shape - First Calculation

The final step in studying the effect of the optimum cancellation multipoles, defined in equation (36), is to find the distorted body shape which they produce in combination with the wing and a basic body. The decision was made to calculate a body shape which would be optimum at a Mach number equal to  $\sqrt{2}$ . The details of the wing and body geometry are given in sketch (x) and the basic body parameters  $V_K$  and  $V_S$  were interpreted in terms of source strength by equation (73).

It was apparent from the results of figure 8 that, for the values of  $r_e$  and  $b$  given by sketch (x), the velocity field induced by the first two optimum multipole distributions can be calculated with good accuracy using slender-body theory. Combining the values of  $\Phi_r$  and  $\Phi_\theta$  so calculated with those induced by the wing, given by equation (56), and those induced by the basic body, using also slender-body theory to interpret equation (73), one can find the body shape by solving the two simultaneous nonlinear differential equations presented as equations (43). These were solved numerically by the method outlined in Appendix D and the results were, unfortunately, unrealistic. Sketch (y) shows an example of a streamline close to the  $\theta = 0$  plane and the crossing of such streamlines obviously invalidates the solution.

### Body Shape - Second Calculation

The failure observed in the first calculation has a simple enough interpretation. For the chosen wing the basic body was too small in diameter at the wing-body juncture to permit the use of the first two cancellation multipoles in their entirety.



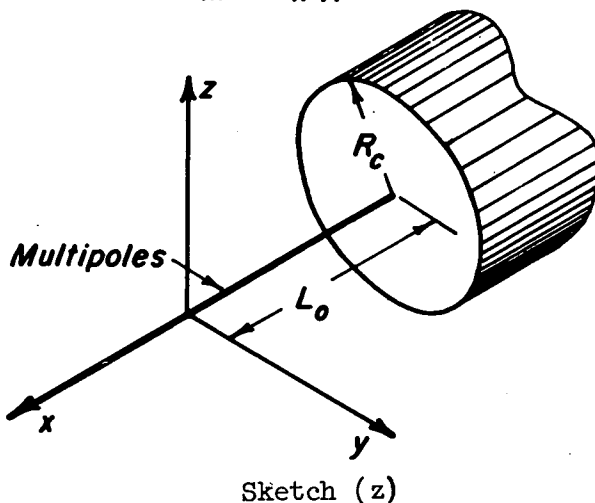
Several avenues of approach are yet available. One could, for example, maintain the same wing and basic body but reduce the Mach number, one could start with a larger basic body, or one could lower the thickness ratio or aspect ratio of the wing, thus diminishing the strength of the cancellation multipoles. All of these, however, are modifications of the basic conditions or basic restraints and as soon as such restrictions are abandoned it must be remarked that no matter how low the wave drag of a set of nonlifting, volume-enclosing surfaces has been made, another arrangement of the same volume within a finite space will give a lower

value, unless, of course, the wave drag of the first arrangement is already zero. Therefore, instead of modifying any of the initial restraints, consider the following alternative:

How much can the drag be reduced by using only a portion of the first two cancellation multipoles so that a real body would still be simulated?

In order to answer the above question, examine briefly the first calculation. Notice, from figure 8, that the cause of the body collapse is attributable to the large values of  $\varphi_r$  and  $\varphi_\theta$  induced by the second-order cancellation multipoles,  $\alpha_2(x)$ . Hence, let  $\alpha_0(x)$  be maintained at its full value and reductions permitted only in the magnitude of  $\alpha_2(x)$ . To carry out such a procedure efficiently, one must be able to determine the effect of a given variation of  $\alpha_2(x)$  on the body shape. Fortunately, Graham, in reference 14, has developed a method by means of which the relation between  $\alpha_2(x)$  and body shape can be quickly estimated. Graham has shown, if

$$M = 1.41$$



1. a rectilinear distribution of second-order multipoles of strength  $\alpha_2(x)$  is placed along the  $x$  axis (see sketch (z)) in a supersonic stream ( $M = \sqrt{2}$ ),

2. slender-body theory is used to evaluate  $\varphi_r$  and  $\varphi_\theta$ ,

3.  $R = R_c$  is the radius of a circularly cylindrical tube for  $-L_0 > x > -\infty$ ,

$$4. F^*(x) = \frac{4}{\pi U_0 R_c^4} \int_{-L_0}^x \alpha_2(x_2) dx_2$$

then

$$R = R_c \left\{ \frac{1 + 2F^*(x) \cos 2\theta + \sqrt{1 + 4F^*(x) \cos 2\theta + 4[F^*(x)]^2}}{2} \right\}^{1/4} \quad (83)$$

is the continuation of the stream tube for  $x > -L_0$ .

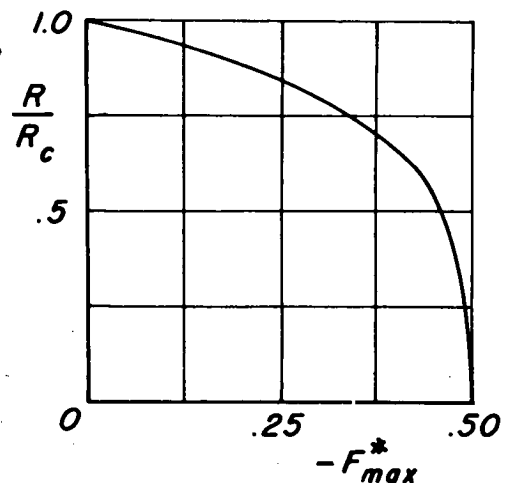
Since the initial strengths of the cancellation multipoles are negative,  $F^*(x)$  is negative and the critical value of  $R$  occurs along the plane  $\theta = 0$  or  $\pi$ . The variation of  $R/R_c$  with  $F_{\max}^*$  is given



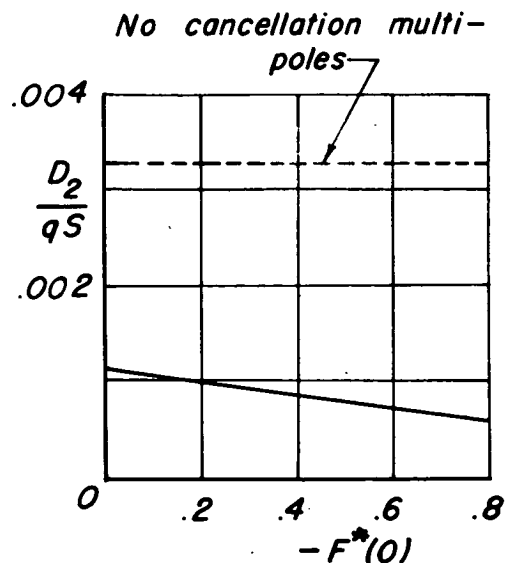
in sketch (aa) from which one can see that the maximum value of  $|F^*|$  must be less than 0.5 if the simulated stream tube behind the plane  $x = -L_0$  is to be real.

The problem can now be continued, using Graham's result as a guide, by assuming the critical body radius in the more complicated source and multipole arrangement is principally determined by  $F^*(0)$  - the parameter governing the body indentation at the center of the cutout and at the wing-body juncture. In the first place, since there is no interference between different orders of multipoles, it is necessary to consider only the drag produced by the second-order multipole. Appendix E presents a method for finding the optimum distribution of the second-order cancellation multipoles for a given wing and a fixed value of  $F^*(0)$ . The resulting wave drag is given in equation (E11). At a Mach number equal to  $\sqrt{2}$  and for the basic wing and body parameters presented in sketch (x),  $F_w^*(0)$  (defined by eq. E8) equals -2.90 and the reduction in  $D_2/qS$ , the amount of drag caused by the wing second-order multipoles alone - see equation (62) and figure 7 - is shown in sketch (ab) for a range of  $F^*(0)$ . Variations on the strength of various combinations of second-order multipoles are shown in sketch (ac) on page 48. It is important to notice that for a given percentage reduction in the maximum strength of the multipoles the resulting percentage reduction in  $D_2$  is much larger.

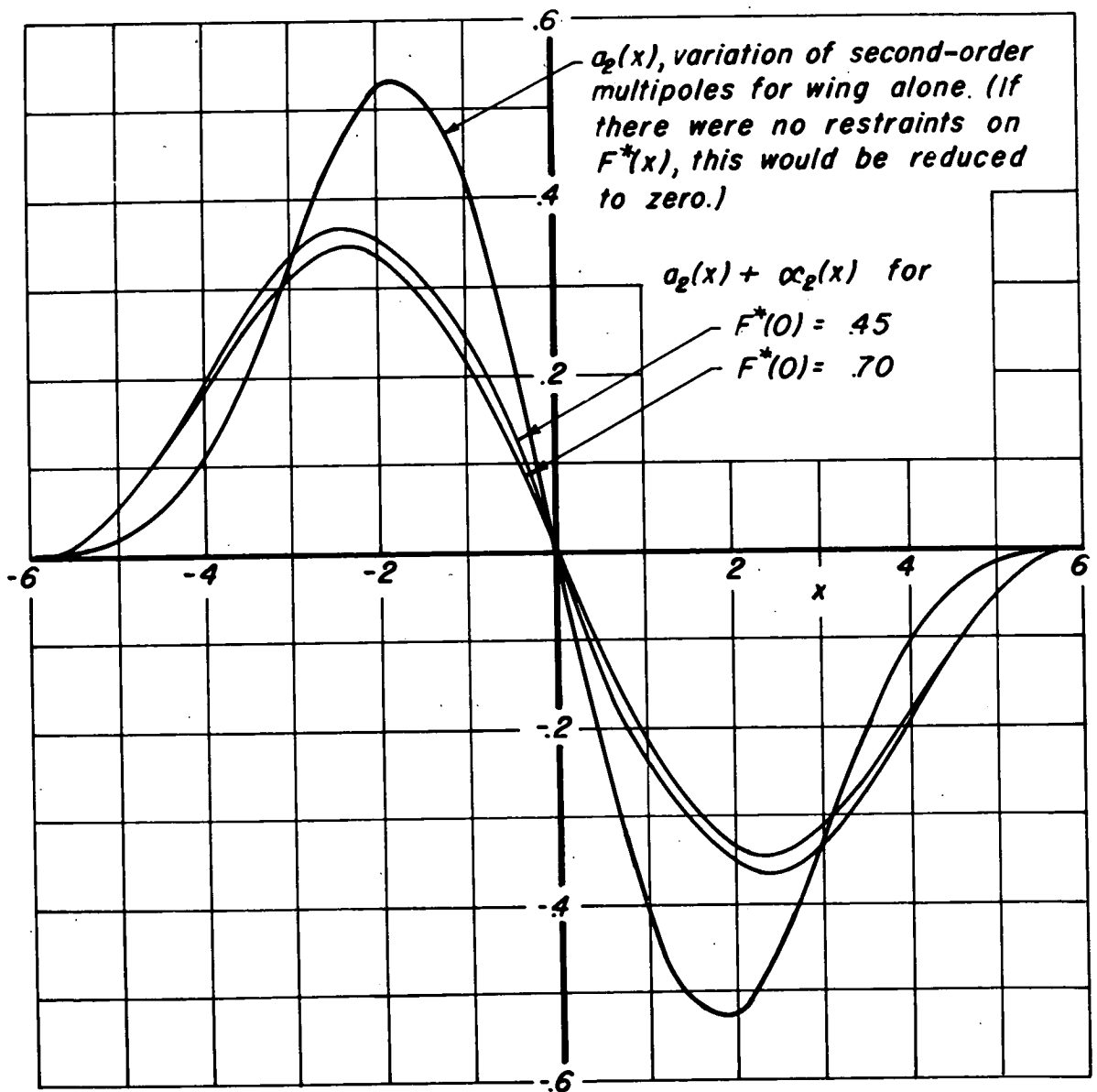
The strengths of  $\alpha_2(x)$  shown in sketch (ac) must now be combined with the zero-order multipoles and wing source sheet, and the combined velocity field used to calculate the shape of the new body. Using again slender-body theory to evaluate the velocity field induced by the multipoles and the numerical methods given in Appendix D to compute the streamlines, one finds, by restricting the



Sketch (aa)



Sketch (ab)

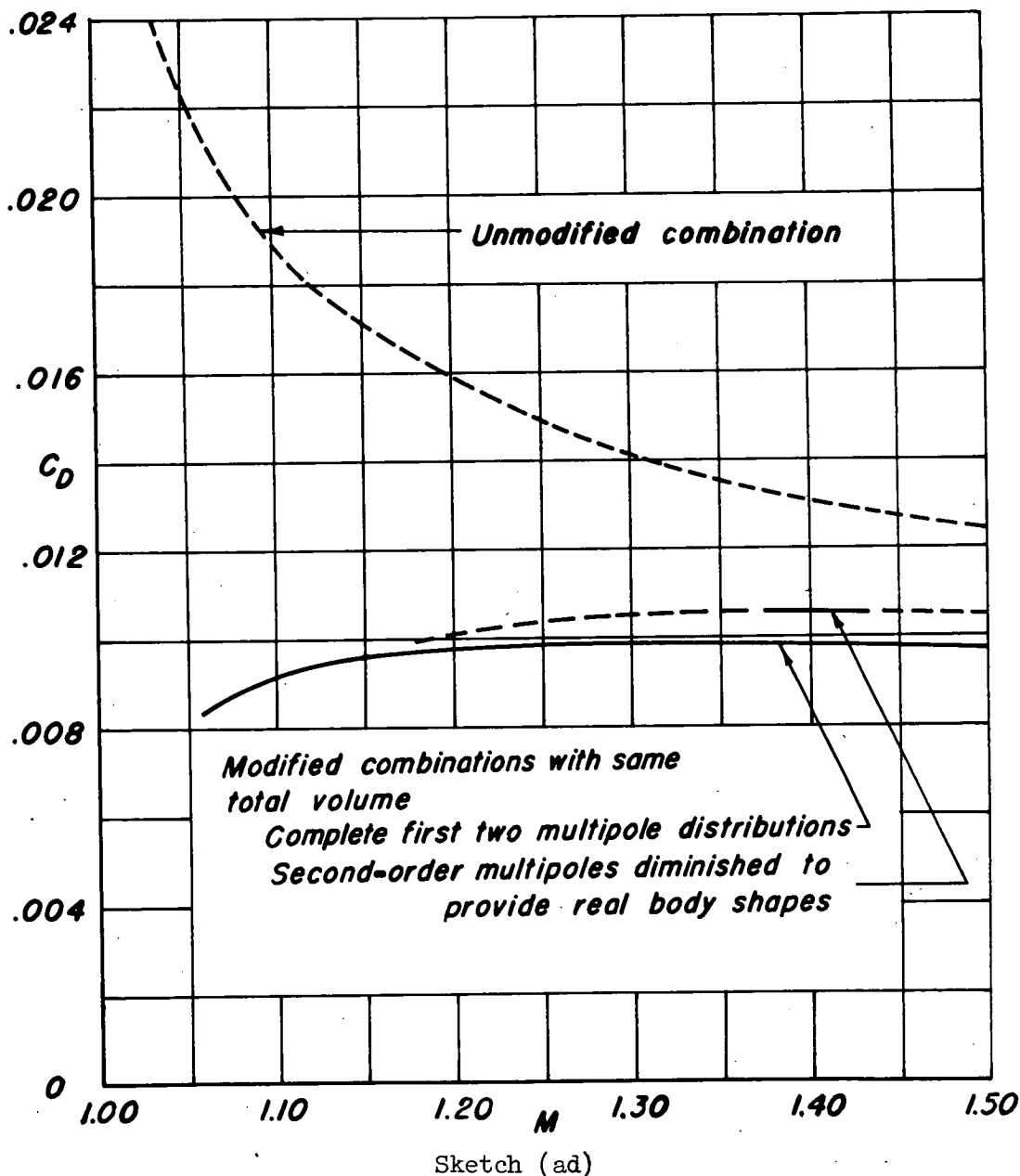


Sketch (ac)

distribution and strength of the second-order cancellation multipoles to their optimum values corresponding to the restraint<sup>10</sup>  $F^*(0) = -0.6$ , that a real as well as reasonable body shape results. The details of

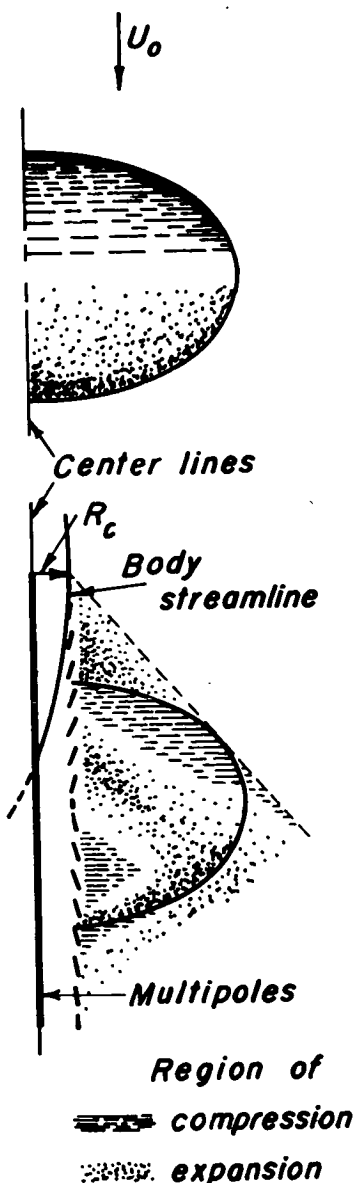
<sup>10</sup>Sketch (aa) gives 0.5 as the maximum permissible value of  $-F^*(x)$ . However, that value is based on a distribution of  $\alpha_2(x)$  alone, and in our more general case the added velocity field caused by the presence of the other singularities permits the larger value.

this shape are presented in figure 9 and their general interpretation is discussed in the next section. Finally, using the value  $F^*(0) = -0.6$ , the drag curves shown in sketch (w) were reinterpreted, and the results - which represent an estimate of the amount the wave drag of an elliptic wing mounted on a basic body of revolution can be reduced by realistic body distortions - are shown in sketch (ad).



## Discussion of Results

It is possible to gain some insight into the reasons for the various body distortions shown in figure 9 by inspecting, in another light, the body shape first calculated. Consider first the elliptic wing at the top of sketch (ae). The air over the forward part of this wing, when it is alone in a supersonic stream, is compressed (mathematically, the sign of  $\phi_x$  is negative), the compression being greatest near the leading edge. On the other hand, the air over the after portion of the wing is undergoing an expansion, the magnitude of which is greatest near the trailing edge. Consider now, in combination with this wing, a body which is to have a shape providing favorable interference. It is apparent that the body should cast expansion waves over the forward portion of the wing, destroying the compression there, and absorb the expansion waves coming from the wing after portion. Or in another light, the positive pressure on the forward region of the wing (one can use the equation  $C_p = (p-p_0)/q = -2\phi_x/U_0$  for the pressure coefficient) should be reduced as far as possible by a wave shed from the body and having large negative pressures where it comes in contact with the wing forward region.

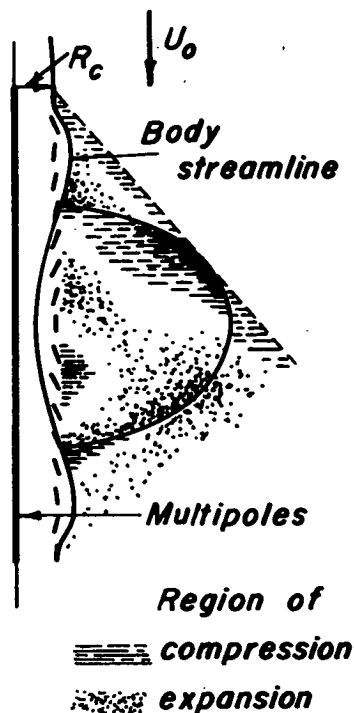


Sketch (ae)

Since waves in a supersonic flow field are fundamentally associated with the slope of the disturbing surface, the aforementioned favorable interference fields would be created by a body having, longitudinally along its surface, slopes such as those shown in the lower part of sketch (ae). This is exactly what the solution obtained from the calculation of the first body shape tried to establish since the fuselage near the plane of the wing (the portion most strongly affecting and being affected by the pressures on the wing) and ahead of the wing chordwise center line was distorted in a manner that caused an expansion across the wing entire forward portion. The difficulty arose because the fuselage was not wide enough to provide the longitudinal extent of favorable slopes necessary to create the positive pressure called for by the wing forward compression region, and the body streamline near the wing root, following a path such as that shown by the line in sketch (ae), crossed the body center line before it reached the wing chordwise center.

Consider now the second body calculated in the previous section. In this case an additional restraint was imposed which, effectively, fixed the maximum body indentation. Subject to such a condition, an optimum interference field was discovered. If the resulting fuselage shape is inspected near the plane of the wing, surface slopes are found similar to those shown in sketch (af). The following discussion is intended to show that, from a physical viewpoint, this arrangement is reasonable.

Most of the wing pressure drag occurs on the wing inboard portions. Hence, for a fixed maximum fuselage indentation, it is beneficial, from an over-all point of view, to create initially a compression wave, which increases the pressure drag on the forward portion of the wing tip but provides a succeeding extent of fuselage having slopes that generate a strong expansion wave over the forward portion of the wing inboard section. Similarly, the final portion of the body is forced to have a region of unfavorable interferences where the expansion waves from the wing tips combine with body expansion waves to increase the local drag (i.e., increase the local suction pressure) in order that the over-all interference effects are as beneficial, under the given restraints, as possible. This arrangement (i.e., unfavorable interference near the wing tip and favorable interference near the wing root) is given further support by the attenuation property inherent in three-dimensional waves. Thus the pressures induced by the body on the wing tips are not as strong, for a given generating surface slope, as those induced on the inner portion of the wing, simply because the tips are farther from the disturbing surface.

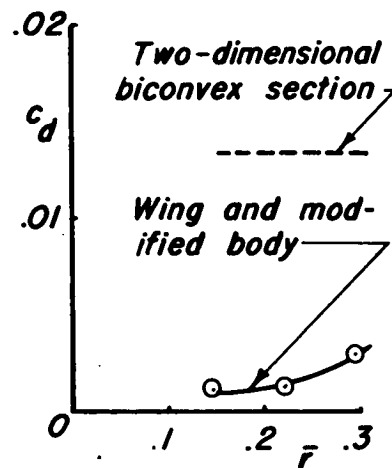
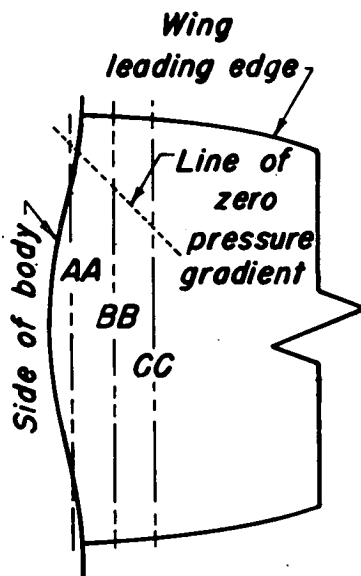
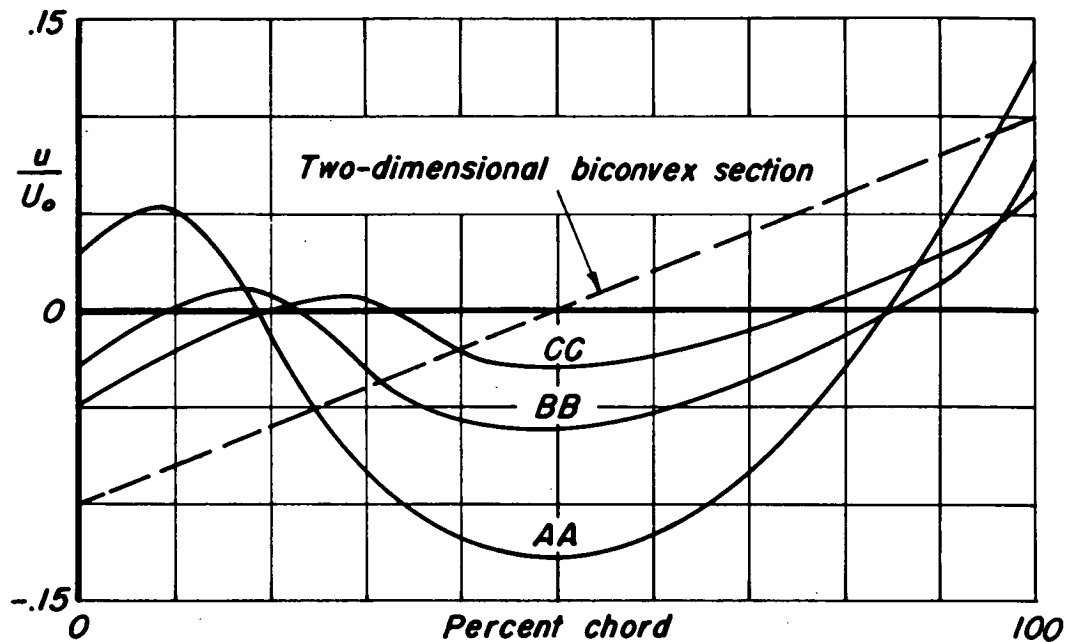


Sketch (af)

Although these considerations are somewhat oversimplified (the shape of the upper part of the body has been completely ignored in estimating the effect of the waves), the longitudinal variation of surface slopes near the plane of the wing and the resulting body streamlines there are, from a physical point of view, reasonable.

In order to support the above conclusions, the source and multipole distributions simulating the final modified body shown in figure 9 were used to calculate (see Appendix C)  $u/U_0$  in the plane of the wing near the root section. The values of  $u/U_0$  induced by the wing sources along these sections were assumed to be the same as those induced by a two-dimensional biconvex section having the same local chord; that is, tip effects were neglected. These values for body and wing were added and

the resulting pressure distributions, shown in sketch (ag) ( $C_p = -2u/U_0$ ), were obtained. The results are similar to the estimates presented in sketch (af). The large drag saving near the root section is illustrated



Sketch (ag)

in sketch (ag) by the graph showing the low values of section drag coefficient along the inner portion of the wing.

Another important characteristic of wing-body combinations designed to have low wave drag is also illustrated in sketch (ag). As shown

in the graph of  $u/U_0$ , over the surface of a two-dimensional biconvex section the air is everywhere accelerating in the streamwise direction. In studies concerning the effects of viscosity on the fluid flow and, in particular, studies concerning the boundary layer, this positive fluid acceleration is referred to as a favorable pressure gradient. If the flow is laminar in the vicinity of the leading edge of a smooth wing and the pressure gradient is everywhere favorable, the flow tends to remain laminar and unseparated over most of the wing chord. Notice that the modified wing-body combination has a line of zero pressure gradient extending along a Mach line downstream from a point near the body and wing leading-edge juncture. Immediately behind this line the pressure gradient is unfavorable which gives rise to the possibility of flow separation or, at least, transition from laminar to turbulent flow there.

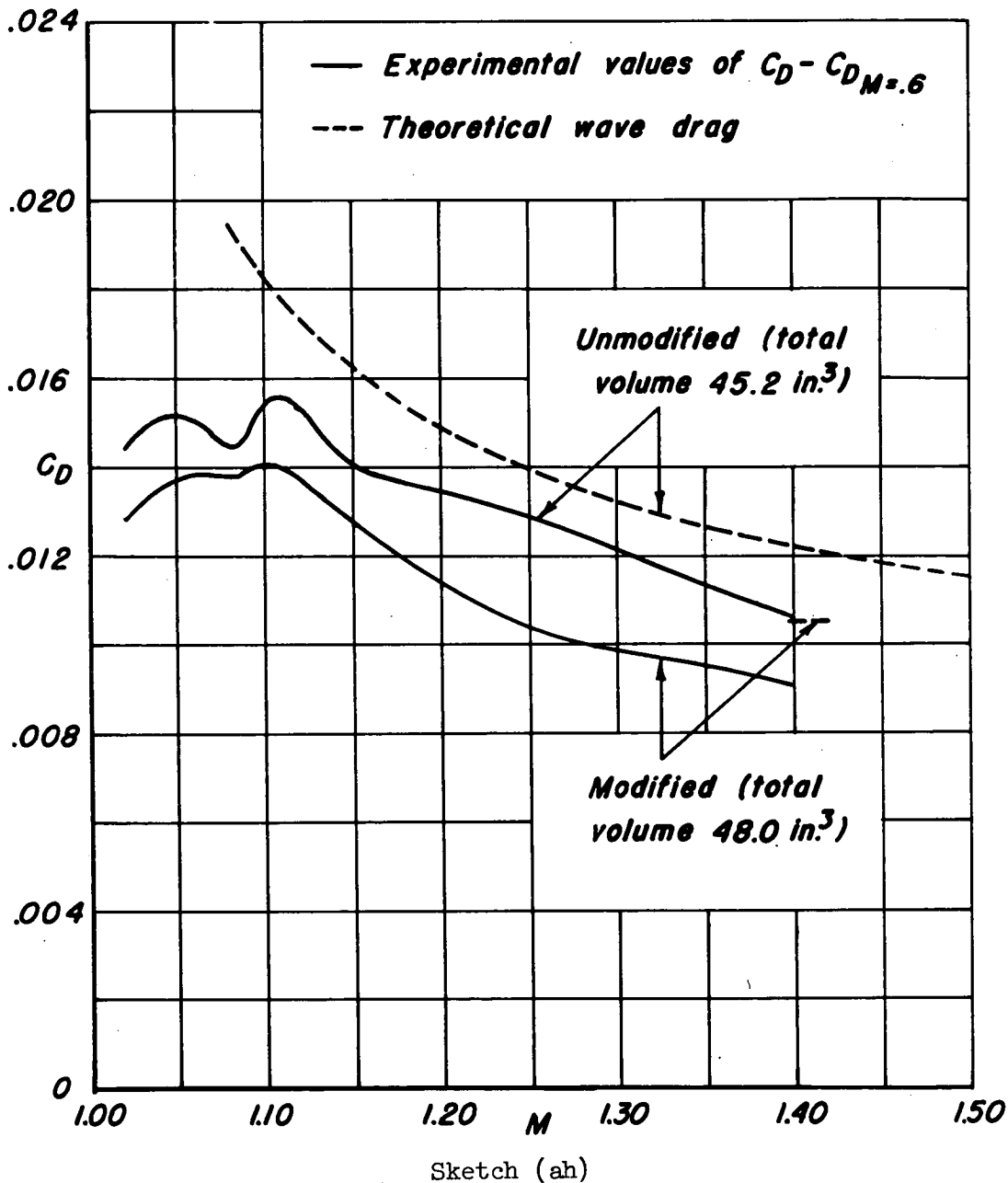
#### Comparison With Experiment

The modified wing-body combination shown in figure 9 was tested in the Ames 2- by 2-foot transonic wind tunnel. The Reynolds number of the test, based on the mean aerodynamic chord, was approximately  $1.5 \times 10^6$ . This combination had an exposed wing volume of 3.44 cubic inches and a body volume equal to 44.60 cubic inches, for a total volume of 48.04 cubic inches. As a control, an unmodified combination composed of the same elliptic wing mounted on a body of revolution (the area distribution of which was determined from equation (74) with  $l = 10.5$ ,  $V_K = 12.88$ , and  $V_{SH} = 29.02$  cubic inches) was tested. The exposed wing area in the unmodified combination was 3.32 cubic inches and the body volume was 41.90 cubic inches, for a total volume of 45.22 cubic inches. Thus, the unmodified combination had the same body length as the modified one but less volume.

The wave drag at  $M = 1.41$  of the combination shown in figure 9 has already been calculated and presented in sketch (ad) by the curve pertaining to real body shapes. By use, in equation (78), of the values of  $V_K$  and  $V_{SH}$  mentioned above and a value of 0.176 for  $R/b$ , the wave drag for the unmodified body was calculated throughout a supersonic Mach number range. The theoretical results obtained for body configurations are shown by the dashed curves in sketch (ah).

The wind-tunnel results for the total drag on both configurations are shown in figure 10 for  $0.6 \leq M \leq 1.4$ . Notice that three groups of data are shown. The lower one represents the unmodified body alone, the middle one represents the modified and unmodified combinations with no fixed transition, and the upper one represents both combinations with transition fixed along the leading edge. The models tested with natural transition did not show the predicted drag reduction. As was pointed out in the discussion of sketch (ag), however, the adverse pressure gradients on the modified model could be inducing transition in the vicinity of

the  $45^\circ$  line behind the juncture of the wing leading edge with the fuselage. This, in turn, would cause the wing of the modified model to have a larger area covered with a turbulent boundary layer and, hence, cause the drag of the model to increase. In order to separate the potential and viscous effects, the transition-fixed tests were made. If the experimental wave drag is taken to be the difference between the drag at a supersonic Mach number and the drag at  $M = 0.6$ , the resulting values of experimental wave drag are as shown in sketch (ah).





Sketch (ah) shows that the experimental reduction in wave drag brought about by the modification agrees with that predicted by theory. Both theory and experiment show a reduction of about 0.0015 in the drag coefficient at the design Mach number (1.41), and the experiment further shows an average reduction of 0.0020 over the Mach number range  $1.2 < M < 1.4$ . A further study of figure 10 shows that the difference between the experimental and theoretical wave drags shown in sketch (ah) for the wing-body combinations is nearly the same as the difference between experiment and theory for the body alone.

Ames Aeronautical Laboratory  
National Advisory Committee for Aeronautics  
Moffett Field, Calif., Feb. 16, 1955

## APPENDIX A

## DERIVATION OF THE OPERATIONAL FORM OF THE WAVE EQUATION

For convenience, take the normalized form of the wave equation in Cartesian coordinates, thus

$$\frac{\partial^2 \phi}{\partial x^2} - \frac{\partial^2 \phi}{\partial y^2} - \frac{\partial^2 \phi}{\partial z^2} = 0 \quad (A1)$$

and define the Laplace transform of  $\phi(x, y, z)$  by

$$\bar{\phi}(s, y, z) = \int_0^\infty e^{-sx} \phi(x, y, z) dx \quad (A2)$$

Now if  $x = f(y, z)$  is the equation of the foremost Mach cone or Mach cone envelope and  $f(y, z) \geq 0$ , it is apparent

$$\frac{\partial^2 \bar{\phi}}{\partial y^2} = \frac{\partial^2}{\partial y^2} \int_f^\infty \phi(x, y, z) e^{-sx} dx = \int_f^\infty e^{-sx} \frac{\partial^2 \phi}{\partial y^2} dx - \frac{\partial f}{\partial y} e^{-sf} \left( \frac{\partial \phi}{\partial y} \right)_{x=f} \quad (A3)$$

since  $(\phi)_{x=f}$  is, but  $\left( \frac{\partial \phi}{\partial y} \right)_{x=f}$  is not necessarily zero. From equation (A3) we see

$$\int_0^\infty e^{-sx} \frac{\partial^2 \phi}{\partial y^2} dx = \frac{\partial^2 \bar{\phi}}{\partial y^2} + \frac{\partial f}{\partial y} e^{-sf} \left( \frac{\partial \phi}{\partial y} \right)_{x=f} \quad (A4)$$

$$\int_0^\infty e^{-sx} \frac{\partial^2 \phi}{\partial z^2} dx = \frac{\partial^2 \bar{\phi}}{\partial z^2} + \frac{\partial f}{\partial z} e^{-sf} \left( \frac{\partial \phi}{\partial z} \right)_{x=f} \quad (A5)$$

Further, integrating by parts gives

$$\int_0^\infty e^{-sx} \frac{\partial^2 \phi}{\partial x^2} dx = s^2 \bar{\phi} - e^{-sf} \left( \frac{\partial \phi}{\partial x} \right)_{x=f} \quad (A6)$$

Hence,

$$\int_0^{\infty} e^{-sx} \left( \frac{\partial^2 \phi}{\partial x^2} - \frac{\partial^2 \phi}{\partial y^2} - \frac{\partial^2 \phi}{\partial z^2} \right) dx = s^2 \bar{\phi} - \frac{\partial^2 \bar{\phi}}{\partial y^2} - \frac{\partial^2 \bar{\phi}}{\partial z^2} - e^{-sf} \left( \frac{\partial \phi}{\partial x} + \frac{\partial \phi}{\partial y} \frac{\partial f}{\partial y} + \frac{\partial \phi}{\partial z} \frac{\partial f}{\partial z} \right)_{x=f} \quad (A7)$$

The last term on the right is the directional derivative of the perturbation potential along the surface  $x = f(y, z)$ . This is, of course, along the so-called conormal. Since  $\phi$  is a constant on the forward envelope, its gradient along the envelope is zero and

$$\int_0^{\infty} e^{-sx} \left( \frac{\partial^2 \phi}{\partial x^2} - \frac{\partial^2 \phi}{\partial y^2} - \frac{\partial^2 \phi}{\partial z^2} \right) dx = s^2 \bar{\phi} - \frac{\partial^2 \bar{\phi}}{\partial y^2} - \frac{\partial^2 \bar{\phi}}{\partial z^2} = 0. \quad (A8)$$

## APPENDIX B

## ON THE VOLUME OF BODIES CALCULATED USING SLENDER-BODY THEORY

The following proof shows that in a rectilinear distribution of singularities, only the sources contribute to the total cross-sectional area of the simulated body and, hence, to its volume.

According to slender-body theory, the velocities induced in the field by distributions of multipoles along the  $x$  axis can be written

$$\varphi_{n_r} = \begin{cases} \frac{a_0(x)}{2\pi r} & , \quad n = 0 \\ \frac{(-2)^n n! a_n(x) \cos n\theta}{4\pi r^{n+1}} & , \quad n > 0 \end{cases} \quad (\text{B1a})$$

$$\frac{1}{r} \varphi_{n_\theta} = \frac{(-2)^n n! a_n(x) \sin n\theta}{4\pi r^{n+1}} \quad (\text{B1b})$$

Further we have derived - see equation (41) - neglecting only second-order effects, the equation representing the boundary condition for the body, thus

$$U_0 \frac{\partial R}{\partial x} = \left( \varphi_r - \frac{\varphi_\theta}{r^2} \frac{\partial R}{\partial \theta} \right)_{r=R(x,\theta)} \quad (\text{B2})$$

Combine equations (B1) and (B2)

$$2\pi U_0 R \frac{\partial R}{\partial x} = a_0(x) + \sum_{n=1}^{\infty} (-2)^n n! a_n(x) \left( \frac{\cos n\theta}{R^n} - \frac{\sin n\theta}{R^{n+1}} \frac{\partial R}{\partial \theta} \right)$$

multiply by  $d\theta$ , and integrate

$$2\pi U_0 \frac{\partial}{\partial x} \int_0^{2\pi} \frac{R^2}{2} d\theta = 2\pi a_0(x) + \sum_{n=1}^{\infty} (-2)^n n! a_n(x) \int_0^{2\pi} \left( \frac{R \cos n\theta - \sin n\theta \frac{\partial R}{\partial \theta}}{R^{n+1}} \right) d\theta$$

or

$$2\pi U_0 \frac{\partial}{\partial x} S(x) = 2\pi a_0(x) + \sum_{n=1}^{\infty} (-2)^n (n-1)! a_n(x) \int_0^{2\pi} \frac{d}{d\theta} \left( \frac{\sin n\theta}{R^n} \right) d\theta \quad (B3)$$

Since the integrand in equation (B3) is a periodic function in  $\theta$ , we have

$$\frac{\partial S}{\partial x} = \frac{a_0(x)}{U_0} \quad (B4)$$

which shows the simulated-body normal cross-sectional area to be dependent only on the source strength. Further, the total volume is given by

$$V = \int_{-l}^{l'} S(x) dx = \int_{-l}^{l'} (l' - x) S'(x) dx + (l' + l) S(-l)$$

and when  $S(l') = S(-l) = 0$ , there results

$$V = - \frac{1}{U_0} \int_{-l}^{l'} x a_0(x) dx \quad (B5)$$

## APPENDIX C

ON THE CALCULATION OF VELOCITIES INDUCED BY ARBITRARY  
SOURCE DISTRIBUTIONS

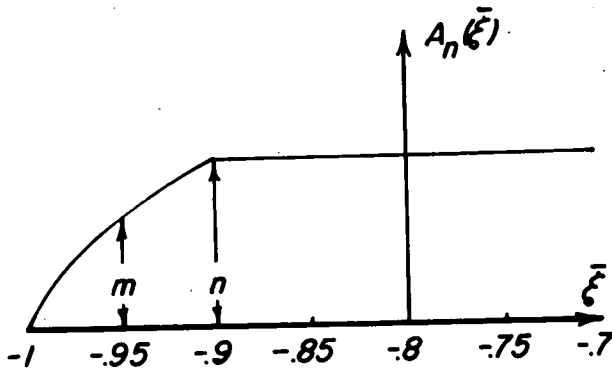
The potential and velocity fields represented by equations (18) and (19) are difficult to evaluate analytically even if  $A_n(\xi)$  is a simple function. However, the calculations can be reduced to a relatively simple process. First, let equation (18) be expressed in terms of the dimensionless variables  $\bar{x}$ ,  $\bar{\xi}$ , and  $\bar{r}$  where

$$\left. \begin{aligned} \bar{x} &= x/L_0 \\ \bar{\xi} &= \xi/L_0 \\ \bar{r} &= \beta r/L_0 \end{aligned} \right\} \quad (C1)$$

Then

$$\varphi_0(\bar{x}, \bar{r}, \theta) = -\frac{1}{2\pi} \int_{-1}^{\bar{x}-\bar{r}} \frac{A_0(\bar{\xi}) d\bar{\xi}}{\sqrt{(\bar{x} - \bar{\xi})^2 - \bar{r}^2}} \quad (C2a)$$

$$\varphi_2(\bar{x}, \bar{r}, \theta) = -\frac{\cos 2\theta}{2\pi} \int_{-1}^{\bar{x}-\bar{r}} \frac{A_2(\bar{\xi}) [2(\bar{x} - \bar{\xi})^2 - \bar{r}^2] d\bar{\xi}}{\bar{r}^2 \sqrt{(\bar{x} - \bar{\xi})^2 - \bar{r}^2}} \quad (C2b)$$



Sketch (ai)

and so forth. Consider next the variation of  $A_n(\xi)$  shown in sketch (ai) and represented by the equation

$$A_n(\bar{\xi}) = \begin{cases} ((190n - 360m) + (390n - 760m)\bar{\xi} + (200n - 400m)\bar{\xi}^2), & -1 \leq \bar{\xi} \leq -0.9 \\ n, & -0.9 \leq \bar{\xi} \end{cases} \quad (C3)$$

As seen in the sketch,  $A_n$  vanishes at  $\bar{\xi} = -1$ , is a parabola between  $-1$  and  $-0.9$  (assuming the values  $m$  at  $\bar{\xi} = -0.95$  and  $n$  at  $\bar{\xi} = -0.9$ ), and

the straight line,  $A_n(\xi) = n$ , for  $\xi$  greater than  $-0.9$ . The velocities induced by a multipole distribution given by equation (C3) can be calculated in a straightforward manner in the two regions  $-1 + \bar{r} \leq \bar{x} \leq -0.9 + \bar{r}$  and  $-0.9 + \bar{r} \leq \bar{x}$ . For example, if

$$\frac{\pi \bar{r} M_{O\bar{r}}(\bar{x})}{200} = \begin{cases} -(\bar{x} + 0.9) \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2} + \bar{r}^2 \ln \frac{\bar{x} + 1.0 + \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2}}{\bar{r}}, & -1 + \bar{r} < \bar{x} < -0.9 + \bar{r} \\ -(\bar{x} + 0.9) \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2} + (\bar{x} + 1.0) \sqrt{(\bar{x} + 0.9)^2 - \bar{r}^2} + \bar{r}^2 \ln \frac{\bar{x} + 1.0 + \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2}}{\bar{x} + 0.9 + \sqrt{(\bar{x} + 0.9)^2 - \bar{r}^2}}, & -0.9 + \bar{r} < \bar{x} \end{cases} \quad (C4)$$

$$\frac{\pi \bar{r} N_{O\bar{r}}(x)}{100} = \begin{cases} (\bar{x} + 0.95) \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2} - \bar{r}^2 \ln \frac{\bar{x} + 1.0 + \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2}}{\bar{r}}, & -1 + \bar{r} < \bar{x} < -0.9 + \bar{r} \\ (\bar{x} + 0.95) \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2} - (\bar{x} + 1.05) \sqrt{(\bar{x} + 0.9)^2 - \bar{r}^2} - \bar{r}^2 \ln \frac{\bar{x} + 1.0 + \sqrt{(\bar{x} + 1.0)^2 - \bar{r}^2}}{\bar{x} + 0.9 + \sqrt{(\bar{x} + 0.9)^2 - \bar{r}^2}}, & -0.9 + \bar{r} < \bar{x} \end{cases} \quad (C5)$$

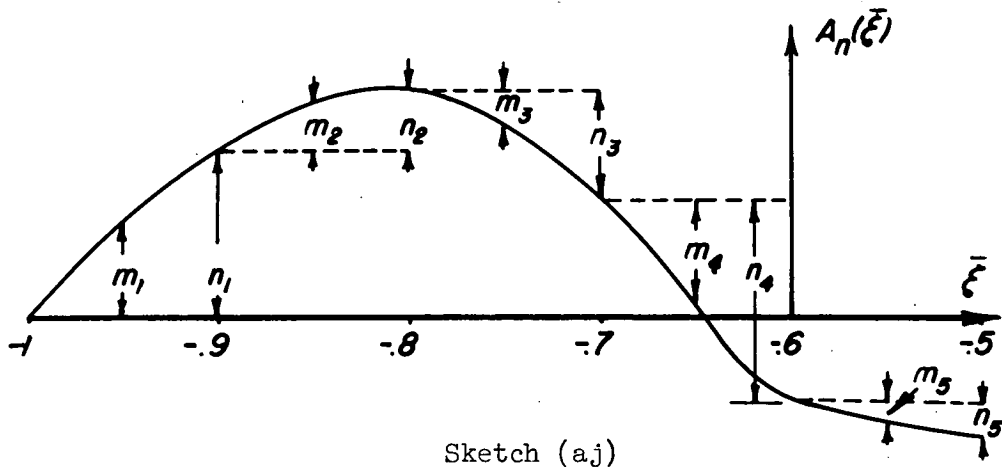
then  $\Phi_{O\bar{r}}$  can be written

$$\Phi_{O\bar{r}} = m M_{O\bar{r}}(\bar{x}) + n N_{O\bar{r}}(\bar{x}) \quad (C6)$$

Now, if one is given a distribution of sources that is composed of, or is adequately approximated by, a series of 20 equally spaced parabolic arcs, equation (C6) can be used for each individual arc and the results superimposed for the complete solution. To this effect, define  $m_1$  and  $n_1$  in terms of  $A_0(x)$  by

$$\left. \begin{aligned} m_1 &= A_0 \left( \frac{1 - 0.5}{10} - 1 \right) - A_0 \left( \frac{1 - 1}{10} - 1 \right) \\ n_1 &= A_0 \left( \frac{1}{10} - 1 \right) - A_0 \left( \frac{1 - 1}{10} - 1 \right) \end{aligned} \right\} \quad (C7)$$

so they represent the magnitudes shown in sketch (aj). Then, if  $[\bar{x}]$  denotes the greatest interger contained in  $\bar{x}$  (e.g.,  $[6.34]$  equals 6),



Sketch (aj)

the equation for the radial velocity becomes

$$\varphi_{0\bar{r}} = \sum_{i=1}^{[10(\bar{x}-\bar{r})+11]} \left[ m_i M_{0\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) + n_i N_{0\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) \right] \quad (C8)$$

Values of  $M_{0\bar{r}}$  and  $N_{0\bar{r}}$  are tabulated in table I for  $\bar{r}$  equal to 0.074, 0.148, 0.222, and 0.296. The asymptotic magnitudes of these functions are given by slender-body theory. Hence, one can easily show for large  $\bar{x}$

$$\left. \begin{aligned} M_{0\bar{r}} &\approx 0 \\ M_{0\bar{r}} &\approx \frac{1}{2\pi\bar{r}} \end{aligned} \right\} \quad (C9)$$

Notice that both functions have essentially reached their asymptotic values for large  $x$  by the time  $\bar{x} = -1 + \bar{r} + 0.5$ . By applying simple tabulative procedures to equation (C8) - for example, listing  $m_1$  and  $n_1$



in reverse order and accumulating multiplications of adjacent terms - the value of  $\phi_{0\bar{r}}$  for any  $A_0(\bar{x})$  representable by equation (C7) is readily calculated.

The velocities induced by higher order multipoles can be calculated in a similar fashion. Because of the asymptotic behavior of the  $M$ 's and  $N$ 's, however, one is led into the numerically inefficient process of obtaining small numbers from differences of large numbers. For the velocities  $\phi_r$  and  $\phi_\theta$ , the following is a method for circumventing this difficulty.

It follows from equations (9) or (19), that for small  $\bar{r}$ ,  $\phi_{n\bar{r}}$  and  $\phi_{n\theta}$  can be expressed in terms of the multipole strengths  $a_n(\bar{x})$  - as defined by equation (7) - by the equations

$$r^{n+1} \left( \frac{\phi_{n\bar{r}}}{\cos n\theta} \right) = C_0 + C_1 r + \dots + C_\nu r^\nu + \dots \quad (C10a)$$

$$r^{n+1} \left( \frac{\phi_{n\theta}}{r \sin n\theta} \right) = D_0 + D_1 r + \dots + D_\nu r^\nu + \dots \quad (C10b)$$

where for  $\nu \leq n$ ,  $n \geq 1$

$$C_\nu = \begin{cases} \frac{(-1)^{n+\frac{\nu}{2}} \beta^\nu 2^{n-\nu}}{4\pi} \frac{(n-\nu)\Gamma(n-\frac{\nu}{2})}{\Gamma(1+\frac{\nu}{2})} a_n^{(\nu)}(x), & \nu \text{ even} \\ 0, & \nu \text{ odd} \end{cases} \quad (C11a)$$

$$D_\nu = \begin{cases} \frac{(-1)^{n+\frac{\nu}{2}} \beta^\nu 2^{n-\nu}}{4\pi} \frac{n\Gamma(n-\frac{\nu}{2})}{\Gamma(1+\frac{\nu}{2})} a_n^{(\nu)}(x), & \nu \text{ even} \\ 0, & \nu \text{ odd} \end{cases} \quad (C11b)$$

Consider now the velocities  $\phi_{2\bar{r}}$  and  $\phi_{2\theta}$  induced by the multipole strength defined by equation (C3); thus

$$\frac{\Phi_{2\bar{r}}}{\cos 2\theta} = mM_{2\bar{r}}(\bar{x}) + nN_{2\bar{r}}(\bar{x}) \quad (C12a)$$

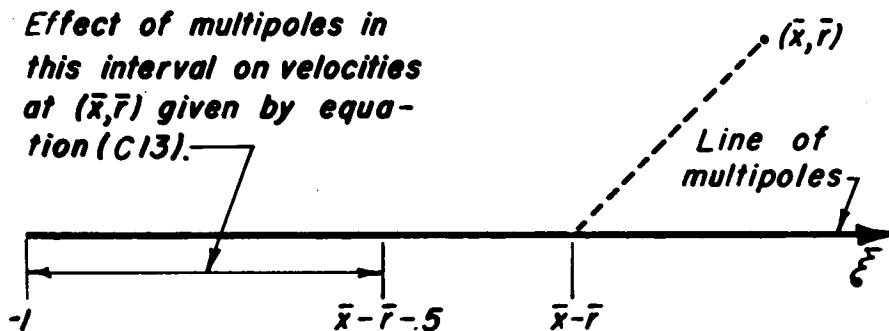
$$\frac{\Phi_{2\theta}}{\bar{r} \sin 2\theta} = mM_{2\theta}(\bar{x}) + nN_{2\theta}(\bar{x}) \quad (C12b)$$

where values of the M's and N's are listed in tables II and III. Their asymptotic values, as given by equations (C10) and (C11), are

$$\left. \begin{aligned} M_{2\bar{r}} &= \frac{19 + 20\bar{x}}{150\pi\bar{r}^3} \\ N_{2\bar{r}} &= \frac{150\bar{x}^2 + 275\bar{x} + 126}{150\pi\bar{r}^3} \\ M_{2\theta} &= \frac{19 + 20\bar{x}}{150\pi\bar{r}^3} \\ N_{2\theta} &= \frac{150\bar{x}^2 + 275\bar{x} + 126}{150\pi\bar{r}^3} - \frac{1}{2\pi\bar{r}} \end{aligned} \right\} \quad (C13)$$

and these are also given in the tables.

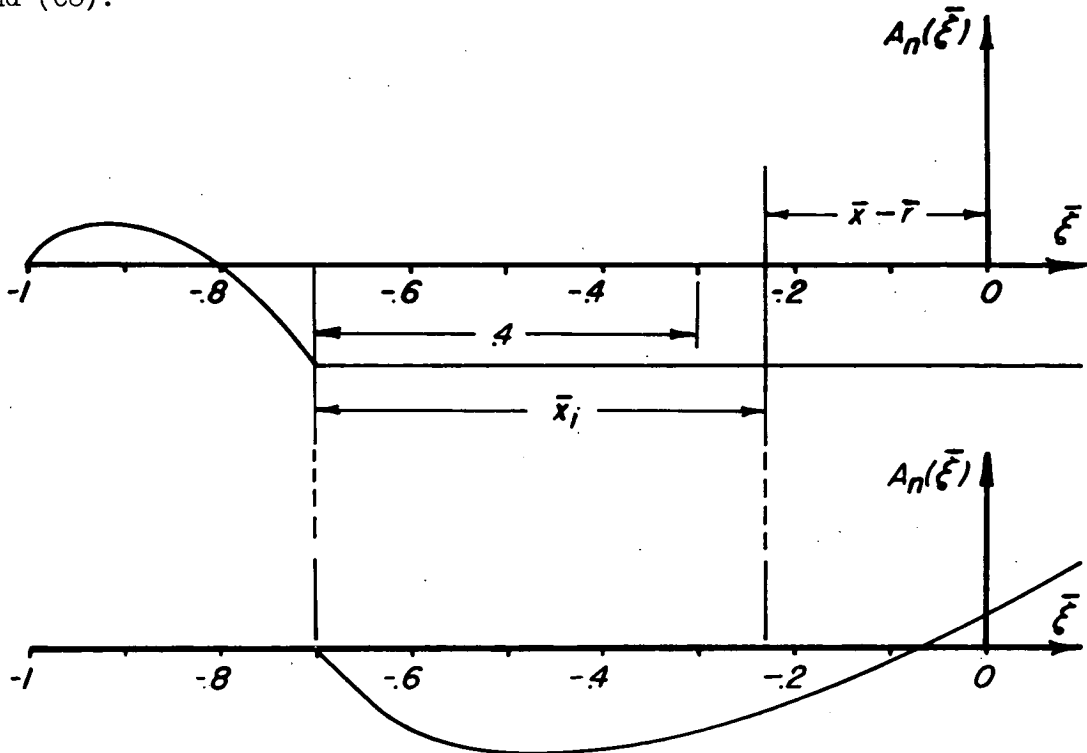
As the tables show, equations (C13) are sufficiently accurate approximations to M and N for practical calculating purposes when  $\bar{x} > -1 + \bar{r} + 0.5$ . Hence, referring to sketch (ak) one can see that the



Sketch (ak)

velocities at the point  $\bar{x}, \bar{r}$  induced by the multipoles in the interval  $-1 < \xi < \bar{x} - \bar{r} - 0.5$  can be calculated using equations (C13). In terms

of the distribution for  $A_2(\bar{\xi})$  - which is equal to  $a_2^{(2)}(\bar{\xi})$ , see equation (16) - this means the multipole distribution shown in the upper part of sketch (a1) can be calculated by means of the asymptotic formulas and the result added to that obtained for the distribution shown in the lower part of sketch (a1) by use of equations (C12b) and tables II and III in a manner identical to the one represented by equations (C6), (C7), and (C8).



Sketch (a1)

The value of  $\varphi_{2\theta}(\bar{x}, \bar{r})$  induced by a multipole distribution such as that shown in the upper part of sketch (a1) is, on the basis of equations (C10) and (C11),

$$\frac{\varphi_{2\theta}}{\bar{r} \sin 2\theta} = H(\bar{x}, \bar{r}) = \frac{2}{\pi \bar{r}^3} \int_{-1}^{\bar{x}} (\bar{x} - \bar{\xi}) A_2(\bar{\xi}) d\bar{\xi} - \frac{A_2(\bar{x})}{2\pi \bar{r}}$$

so

$$H(\bar{x}, \bar{r}) = \frac{2}{\pi \bar{r}^3} a_2(\bar{x} - \bar{r} - \bar{x}_1) + \frac{2(\bar{r} + \bar{x}_1)}{\pi \bar{r}^3} a_2^{(1)}(\bar{x} - \bar{r} - \bar{x}_1) +$$

$$a_2^{(2)}(\bar{x} - \bar{r} - \bar{x}_1) \left[ \frac{(\bar{r} + \bar{x}_1)^2}{\pi \bar{r}^3} - \frac{1}{2\pi \bar{r}} \right] \quad (C14)$$

where  $\beta^2 a_2^{(2)}(x) = A_2(x)$  and  $x_1$  is shown in sketch (a1) and defined by the equation

$$\bar{x}_1 = 0.4 + \bar{x} - \bar{r} - \frac{[10(\bar{x} - \bar{r})]}{10} \quad (C15)$$

the symbol  $[10(\bar{x} - \bar{r})]$  meaning, as before, the highest integer value contained in  $10(\bar{x} - \bar{r})$ . A similar result can be derived for  $\phi_{2\bar{r}}$  and one has finally for  $-1 \leq [10(\bar{x} - \bar{r}) + 11] \leq 5$

$$\frac{\phi_{2\theta}(\bar{x})}{\bar{r} \sin 2\theta} = \sum_1^{[10(\bar{x}-\bar{r})+11]} \left[ m_1 M_{2\theta} \left( \bar{x} - \frac{i-1}{10} \right) + n_1 N_{2\theta} \left( \bar{x} - \frac{i-1}{10} \right) \right] \quad (C16a)$$

$$\frac{\phi_{2\bar{r}}(\bar{x})}{\cos 2\theta} = \sum_1^{[10(\bar{x}-\bar{r})+11]} \left[ m_1 M_{2\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) + n_1 N_{2\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) \right] \quad (C16b)$$

and for  $[10(\bar{x} - \bar{r}) + 11] \geq 6$

$$\frac{\phi_{2\theta}(\bar{x})}{\bar{r} \sin 2\theta} = \sum_{[10(\bar{x}-\bar{r})+11]-5}^{[10(\bar{x}-\bar{r})+11]} \left[ m_1 M_{2\theta} \left( \bar{x} - \frac{i-1}{10} \right) + n_1 N_{2\theta} \left( \bar{x} - \frac{i-1}{10} \right) \right] + H(\bar{x}, \bar{r}) \quad (C17a)$$

$$\frac{\phi_{2\bar{r}}(\bar{x})}{\cos 2\theta} = \sum_{[10(\bar{x}-\bar{r})+11]-5}^{[10(\bar{x}-\bar{r})+11]} \left[ m_1 M_{2\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) + n_1 N_{2\bar{r}} \left( \bar{x} - \frac{i-1}{10} \right) \right] + H(\bar{x}, \bar{r}) - \frac{A_2(\bar{x} - \bar{r} - \bar{x}_1)}{2\pi\bar{r}} \quad (C17b)$$

The streamwise gradients of induced velocities can also be defined in terms of M's and N's as were the velocities  $\phi_{\bar{r}}$  and  $\frac{1}{\bar{r}} \phi_{\theta}$ . Thus

$$\Phi_{O\bar{x}} = mM_{O\bar{x}} + nN_{O\bar{x}}$$

$$\frac{\Phi_{2\bar{x}}}{\cos 2\theta} = mM_{2\bar{x}} + nN_{2\bar{x}}$$

Values of  $M_{O\bar{x}}$ ,  $N_{O\bar{x}}$ ,  $M_{2\bar{x}}$ , and  $N_{2\bar{x}}$  for  $\bar{r}$  equal to 0.148, 0.222, and 0.296 are given in tables IV and V.

## APPENDIX D

## NUMERICAL METHOD USED TO CALCULATE BODY SHAPE

The method used to calculate the body shape was a standard step-by-step solution to the two simultaneous total differential equations (eq. (43) in the text)

$$\left. \begin{aligned} \frac{d\theta}{dx} &= \frac{1}{U_0 R^2} \varphi_\theta(x, R, \theta) \\ \frac{dR}{dx} &= \frac{1}{U_0} \varphi_R(x, R, \theta) \end{aligned} \right\} \quad (D1)$$

The essentials of the process are recognized from the following computing-sheet heading set up for initial values of  $\theta$  and  $\bar{R}$  equal to  $30^\circ$  and 0.148, respectively, where  $\bar{x} = x/L_0$  and  $\bar{R} = \beta R/L_0$

①	②	③	④	⑤	⑥	⑦
n	$\bar{x}$	$\textcircled{13}_n \times 0.05 +$ $\textcircled{3}_{n-1}$ $\theta$	$\textcircled{14}_n \times 0.05 +$ $\textcircled{4}_{n-1}$ $\bar{R}$	$\left(\frac{1}{U_0} \frac{\partial \varphi}{\partial \theta}\right)$ for $\textcircled{3}$ and $\textcircled{4}$	$\left(\frac{d\theta}{d\bar{x}}\right)_1$ $\frac{\textcircled{5}}{\textcircled{4}^2}$	$\left(\frac{1}{U_0} \frac{\partial \varphi}{\partial \bar{R}}\right)$ for $\textcircled{3}$ and $\textcircled{4}$
0	-0.852	0.524	0.148	- - -	- - -	- - -
1	-.802	- - -	- - -	- - -	- - -	- - -
2	-.752	- - -	- - -	- - -	- - -	- - -

⑧	⑨	⑩	⑪	⑫	⑬	⑭
$\textcircled{6}_{n-1} \times 0.05 +$ $\textcircled{3}_{n-1}$ $\theta_1$	$\textcircled{7}_{n-1} \times 0.05 +$ $\textcircled{4}_{n-1}$ $\bar{R}_1$	$\left(\frac{1}{U_0} \frac{\partial \varphi}{\partial \theta}\right)$ for $\textcircled{8}$ and $\textcircled{9}$	$\left(\frac{d\theta}{d\bar{x}}\right)_2$ $\frac{\textcircled{10}}{\textcircled{9}^2}$	$\left(\frac{1}{U_0} \frac{\partial \varphi}{\partial \bar{R}}\right)$ for $\textcircled{8}$ and $\textcircled{9}$	$\left(\frac{d\theta}{d\bar{x}}\right)_{av}$ $\frac{\textcircled{6}_{n-1} + \textcircled{11}_n}{2}$	$\left(\frac{d\bar{R}}{d\bar{x}}\right)_{av}$ $\frac{\textcircled{7}_{n-1} + \textcircled{12}_n}{2}$
- - -	- - -	- - -	- - -	- - -	- - -	- - -

## APPENDIX E

OPTIMUM VARIATION OF  $\alpha_2(x)$  FOR A FIXED VALUE OF  $\int_{-L_0}^0 \alpha_2(x) dx$

Given

$$D_2 = - \frac{q}{4\pi U_0^2} \int_{-L_0}^{L_0} \int_{-L_0}^{L_0} \left[ a_2^{(3)}(x_1) + \alpha_2^{(3)}(x_1) \right] \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \ln \left| \frac{x_1 - x_2}{L_0} \right| dx_1 dx_2 \quad (E1)$$

where the variation of  $a_2^{(3)}(x)$  is fixed, pose the restraint

$$\frac{1}{U_0} \int_{-L_0}^0 \alpha_2(x) dx = F^*(0) \frac{\pi}{4} R_c^4 = \text{constant} \quad (E2)$$

and ask for the function  $\alpha_2(x)$  which minimizes  $D_2$  for a given value of the constant.

If  $f(x) = f(-x)$ , then

$$\int_{-1}^1 \int_{-1}^1 f(x_1) f(x_2) \ln |x_1 - x_2| dx_1 dx_2 = 2 \int_{-1}^0 \int_{-1}^0 f(x_1) f(x_2) \ln |x_1^2 - x_2^2| dx_1 dx_2$$

and since  $\alpha_2(-L_0) = \alpha_2^{(1)}(-L_0) = \alpha_2^{(-2)}(-L_0) = 0$

$$\int_{-L_0}^0 \alpha_2(x) dx = - \frac{1}{6} \int_{-L_0}^0 x^3 \alpha_2^{(3)}(x) dx$$

Therefore, the standard variational problem

$$\delta \left[ D_2 + \lambda \int_{-L_0}^0 \frac{\alpha_2(x) dx}{U_0} \right] = 0 \quad (E3)$$

reduces to

$$\delta \left\{ \frac{-q}{2\pi U_0^2} \int_{-L_0}^0 \int_{-L_0}^0 \left[ a_2^{(3)}(x_1) + \alpha_2^{(3)}(x_1) \right] \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \right. \\ \left. \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_1 dx_2 - \frac{\lambda}{6U_0} \int_{-L_0}^0 x_1^3 \alpha_2^{(3)}(x_1) dx_1 \right\} = 0$$

and this becomes

$$\int_{-L_0}^0 \delta \left[ \frac{\alpha_2^{(3)}(x_1)}{U_0} \right] dx_1 \left\{ \frac{q}{\pi U_0} \int_{-L_0}^0 \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \right. \\ \left. \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 + \frac{\lambda x_1^3}{6} \right\} = 0$$

Integrating three times by parts, using the relations

$$\delta \alpha_2(-L_0) = \delta \alpha_2^{(1)}(-L_0) = \delta \alpha_2^{(2)}(-L_0) = 0$$

$$\delta \alpha_2(0) = \delta \alpha_2^{(2)}(0) = 0, \quad \text{by symmetry}$$

and

$$\lim_{x_1 \rightarrow 0} \frac{\partial}{\partial x_1} \int_{-L_0}^0 \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 \\ = \lim_{x_1 \rightarrow 0} 2x_1 \int_{-L_0}^0 \frac{a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2)}{x_1 - x_2} dx_2 = 0$$



yields

$$\int_{-L_0}^0 \delta \left[ \frac{a_2^{(3)}(x_1)}{U_0} \right] dx_1 \frac{\partial^3}{\partial x_1^3} \left\{ \int_{-L_0}^0 \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 + U_0 \lambda_0 x_1^3 \right\} = 0$$

where

$$\lambda_0 = \frac{\lambda \pi}{6q} \quad (E4)$$

By the fundamental lemma of the calculus of variations

$$\frac{\partial^3}{\partial x_1^3} \left\{ \int_{-L_0}^0 \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 + U_0 \lambda_0 x_1^3 \right\} = 0, \quad 0 > x_1 > -L_0$$

One can also show

$$\frac{\partial^3}{\partial x_1^3} \left\{ \int_0^{L_0} \left[ a_2^{(3)}(x_2) + \alpha_2^{(3)}(x_2) \right] \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 - U_0 \lambda_0 x_1^3 \right\} = 0, \quad L_0 > x_1 > 0$$

Hence,

$$\int_{-L_0}^0 \frac{a_2^{(3)}(x_2)}{U_0} \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 = \gamma_0 + \gamma_2 x_1^2 - \lambda_0 x_1^3 \int_{-L_0}^0 \frac{a_2^{(3)}(x_2)}{U_0} \ln \left| \frac{x_1^2 - x_2^2}{L_0^2} \right| dx_2 \quad (E5)$$

Integrating by parts and changing the notation so that

$$\eta_2 = \frac{x_2^2}{L_0^2}, \quad f(\eta_2) = \frac{a_2^{(2)}(x_2)}{U_0}$$

$$\eta_1 = \frac{x_1^2}{L_0^2}, \quad g(\eta_2) = \frac{a_2^{(2)}(x_2)}{U_0}$$

one has

$$\int_0^1 \frac{f(\eta_2) d\eta_2}{\eta_1 - \eta_2} = \gamma_0 + \gamma_2 \eta_1 - \lambda_0 \eta_1^{3/2} - \int_0^1 \frac{g(\eta_2) d\eta_2}{\eta_1 - \eta_2} \quad (E6)$$

Equation (E6) is the familiar singular integral equation known, in aerodynamic applications, as the airfoil equation. Its inversion is discussed, for example, in reference 3. If one solves equation (E6) and applies the conditions

$$\alpha_2^{(2)}(0) = \alpha_2^{(2)}(L_0) = 0$$

then

$$\gamma_0 = -\frac{4\lambda_0 L_0^3}{15\pi}, \quad \gamma_2 = \frac{48\lambda_0 L_0}{15\pi}$$

and

$$\frac{\alpha_2(x)}{U_0} + \frac{a_2(x)}{U_0} = \frac{\lambda_0 L_0^4 x}{60\pi^2} \left\{ \left[ 10 \left( \frac{x}{L_0} \right)^2 - 4 \right] \sqrt{1 - \left( \frac{x}{L_0} \right)^2} + 3 \left( \frac{x}{L_0} \right)^4 \ln \frac{L_0 - \sqrt{L_0^2 - x^2}}{L_0 + \sqrt{L_0^2 - x^2}} \right\} \quad (E7)$$

Now set

$$\int_{-L_0}^0 \frac{a_2(x)}{U_0} dx = F_w^*(0) \frac{\pi}{4} R_c^4 \quad (E8)$$

so that  $F_w^*(0)$  is a known constant. Then

$$\int_{-L_0}^0 \frac{\alpha_2(x) dx}{U_0} = F^*(0) \frac{\pi}{4} R_c^4 = -F_w^*(0) \frac{\pi}{4} R_c^4 + \frac{2\lambda_0 L_0^6}{225\pi^2} \quad (E9)$$

Using the above expressions, one can show

$$\begin{aligned} \frac{\alpha_2(x)}{U_0} + \frac{a_2(x)}{U_0} &= \frac{15\pi R_c^4 x}{32L_0^2} \left[ F^*(0) + F_w^*(0) \right] \left\{ \left[ 10 \left( \frac{x}{L_0} \right)^2 - 4 \right] \sqrt{1 - \left( \frac{x}{L_0} \right)^2} + 3 \left( \frac{x}{L_0} \right)^4 \ln \frac{L_0 - \sqrt{L_0^2 - x^2}}{L_0 + \sqrt{L_0^2 - x^2}} \right\} \\ & \quad (E10) \end{aligned}$$

The wave drag can be calculated by combining equations (E5) and (E1).

$$D_2 = -\frac{q}{2\pi} \int_0^{L_0} \left( \gamma_0 + \gamma_2 x_1^2 - \lambda_0 x_1^3 \right) \left[ \frac{a_2^{(3)}(x_1)}{U_0} + \frac{\alpha_2^{(3)}(x_1)}{U_0} \right] dx_1$$

Integrate three times by parts and there results, finally

$$D_2 = \frac{675}{32} q L_0^2 \pi \left( \frac{R_c}{L_0} \right)^4 \left[ F^*(0) + F_w^*(0) \right]^2 \quad (E11)$$

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TABLE I. - VALUES OF  $M_{0F}$  AND  $N_{0F}$ .

$\bar{x}$	$M_{0F}$		$N_{0F}$		$\bar{x}$	$M_{0F}$		$N_{0F}$	
	Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic	Exact	Asymp-totic
$\bar{F} = 0.074$					$\bar{F} = 0.148$				
-0.926	0	---	0	---	-0.852	0	---	0	---
-0.876	3.16	---	.56	---	-0.802	2.00	---	.42	---
-0.826	-2.96	---	4.86	---	-0.752	-2.26	---	3.24	---
-0.776	-.24	---	2.52	---	-0.702	-.22	---	1.50	---
-0.726	-.08	---	2.34	---	-0.652	-.10	---	1.30	---
-0.676	-.04	---	2.26	---	-0.602	-.06	---	1.20	---
-0.626	-.02	---	2.22	---	-0.552	-.04	---	1.18	---
-0.576	-.02	---	2.20	---	-0.502	-.02	---	1.14	---
-0.526	-.02	0	2.20	2.15	-0.452	-.02	0	1.14	1.08
-0.476	0	0	2.18	2.15	-0.402	0	0	1.12	1.08
-0.426	0	0	2.18	2.15	-0.352	0	0	1.10	1.08
$\bar{F} = 0.222$					$\bar{F} = 0.296$				
-0.778	0	---	0	---	-0.704	0	---	0	---
-0.728	1.56	---	.34	---	-0.654	1.32	---	.30	---
-0.678	-1.90	---	2.62	---	-0.604	-1.66	---	2.24	---
-0.628	-.22	---	1.12	---	-0.554	-.20	---	.92	---
-0.578	-.10	---	.94	---	-0.504	-.08	---	.78	---
-0.528	-.06	---	.88	---	-0.454	-.06	---	.70	---
-0.478	-.04	---	.84	---	-0.404	-.04	---	.66	---
-0.428	-.02	---	.80	---	-0.354	-.02	---	.64	---
-0.378	-.02	0	.78	0.72	-0.304	-.02	0	.62	0.54
-0.328	-.02	0	.78	.72	-0.254	-.02	0	.60	.54
-0.278	0	0	.76	.72	-0.204	0	0	.60	.54

TABLE II. - VALUES OF  $M_{2F}$  AND  $N_{2F}$ .

$\bar{x}$	$M_{2F}$		$N_{2F}$		$\bar{x}$	$M_{2F}$		$N_{2F}$	
	Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic	Exact	Asymp-totic
$\bar{F} = 0.074$					$\bar{F} = 0.148$				
-0.926	0	---	0	---	-0.852	0	---	0	---
-0.876	9.77	---	-.16	---	-0.802	3.86	---	2.31	---
-0.826	10.61	---	8.31	---	-0.752	.68	---	4.38	---
-0.776	18.09	---	15.53	---	-0.702	3.11	---	4.73	---
-0.726	23.44	---	28.41	---	-0.652	3.85	---	6.97	---
-0.676	28.72	---	45.32	---	-0.602	4.53	---	9.77	---
-0.626	33.95	---	66.17	---	-0.552	5.19	---	13.08	---
-0.576	39.15	---	90.98	---	-0.502	5.85	---	16.90	---
-0.526	44.38	144.41	119.70	119.66	-0.452	6.51	6.52	21.20	21.17
-0.476	49.62	149.64	152.35	152.32	-0.402	7.17	7.17	26.01	25.98
-0.426	54.87	154.88	188.91	188.89	-0.352	7.83	7.83	31.30	31.28
$\bar{F} = 0.222$					$\bar{F} = 0.296$				
-0.778	0	---	0	---	-0.704	0	---	0	---
-0.728	2.49	---	.26	---	-0.654	1.90	---	.25	---
-0.678	-.60	---	3.20	---	-0.604	-.92	---	2.62	---
-0.628	1.11	---	2.66	---	-0.554	.51	---	1.86	---
-0.578	1.38	---	3.46	---	-0.504	.67	---	2.22	---
-0.528	1.61	---	4.47	---	-0.454	.87	---	2.72	---
-0.478	1.81	---	5.65	---	-0.404	.87	---	3.29	---
-0.428	2.01	---	6.99	---	-0.354	.96	---	3.93	---
-0.378	2.21	2.22	8.47	8.44	-0.304	1.05	1.06	4.64	4.60
-0.328	2.40	2.41	10.10	10.07	-0.254	1.13	1.14	5.42	5.39
-0.278	2.60	2.61	11.88	11.86	-0.204	1.22	1.22	6.26	6.23

TABLE III. - VALUES OF  $M_{2g}$  AND  $N_{2g}$ .

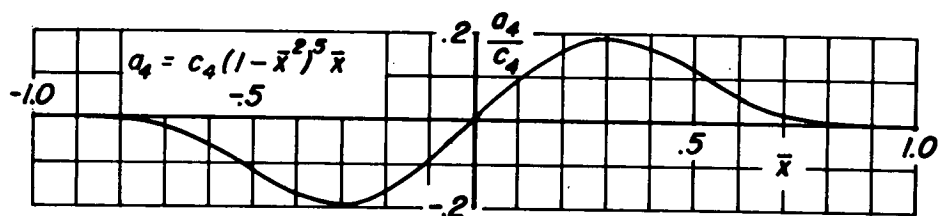
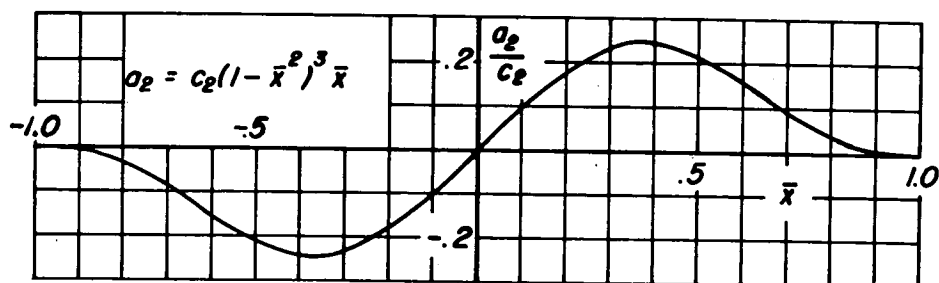
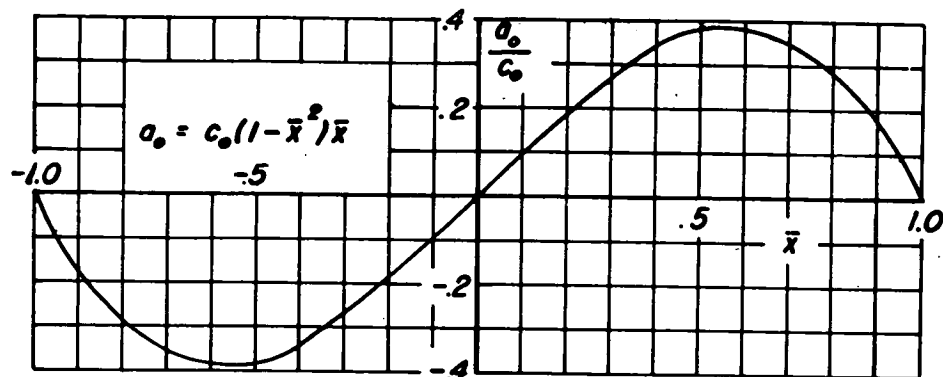
$\bar{x}$	$M_{2g}$		$N_{2g}$		$\bar{x}$	$M_{2g}$		$N_{2g}$	
	Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic	Exact	Asymp-totic
$\bar{F} = 0.074$					$\bar{F} = 0.148$				
-0.926	0	---	0	---	-0.852	0	---	0	---
-0.876	6.62	---	-.73	---	-0.802	1.86	---	-.19	---
-0.826	13.59	---	3.42	---	-0.752	2.93	---	1.11	---
-0.776	18.38	---	12.97	---	-0.702	3.34	---	3.25	---
-0.726	23.48	---	26.12	---	-0.652	3.93	---	5.68	---
-0.676	28.70	---	43.10	---	-0.602	4.58	---	8.55	---
-0.626	33.92	---	63.97	---	-0.552	5.22	---	11.91	---
-0.576	39.15	---	88.80	---	-0.502	5.89	---	15.74	---
-0.526	44.47	44.41	117.48	117.51	-0.452	6.49	6.52	20.07	20.09
-0.476	49.63	49.64	150.15	150.17	-0.402	7.16	7.17	24.89	24.90
-0.426	54.85	54.88	186.77	186.74	-0.352	7.83	7.83	30.18	30.20
$\bar{F} = 0.222$					$\bar{F} = 0.296$				
-0.778	0	---	0	---	-0.704	0	---	0	---
-0.728	.93	---	-.09	---	-0.654	.58	---	-.05	---
-0.678	1.29	---	.59	---	-0.604	.74	---	.37	---
-0.628	1.32	---	1.54	---	-0.554	.71	---	.93	---
-0.578	1.48	---	2.51	---	-0.504	.76	---	1.45	---
-0.528	1.66	---	3.60	---	-0.454	.83	---	2.02	---
-0.478	1.85	---	4.82	---	-0.404	.91	---	2.63	---
-0.428	2.04	---	6.18	---	-0.354	.98	---	3.29	---
-0.378	2.23	2.22	7.69	7.72	-0.304	1.06	1.06	4.03	4.07
-0.328	2.42	2.41	9.33	9.35	-0.254	1.15	1.14	4.82	4.85
-0.278	2.61	2.61	11.11	11.14	-0.204	1.23	1.22	5.67	5.69

TABLE IV. - VALUE OF  $M_{0\bar{x}}$  AND  $N_{0\bar{x}}$ .

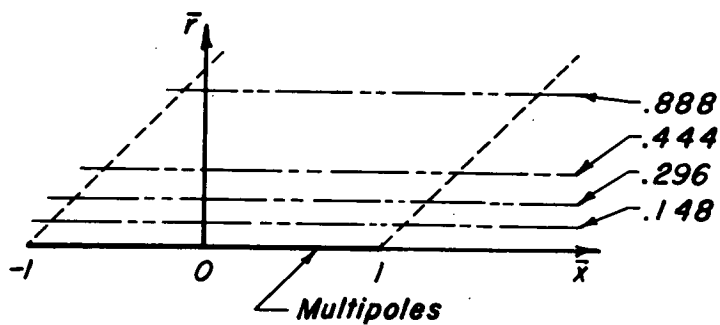
$\bar{x}$	$M_{0\bar{x}}$		$N_{0\bar{x}}$		$\bar{x}$	$M_{0\bar{x}}$		$N_{0\bar{x}}$	
	Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic	Exact	Asymp-totic
$\bar{F} = 0.148$					$\bar{F} = 0.222$				
-0.852	0	---	0	---	-0.778	0	---	0	---
-0.802	-1.663	---	-.442	---	-0.728	-1.379	---	-.360	---
-0.752	2.529	---	-3.024	---	-0.678	2.051	---	-2.489	---
-0.702	.369	---	-1.019	---	-0.628	.297	---	-.859	---
-0.652	.191	---	-.723	---	-0.578	.155	---	-.620	---
-0.602	.121	---	-.572	---	-0.528	.099	---	-.498	---
-0.552	.085	---	-.477	---	-0.478	.070	---	-.420	---
-0.502	.063	---	-.410	---	-0.428	.053	---	-.365	---
-0.452	.049	---	-.361	---	-0.378	.042	---	-.324	---
-0.402	.040	---	-.323	---	-0.328	.034	---	-.292	---
-0.352	.033	---	-.292	---	-0.278	.028	---	-.266	---
-0.302	.027	---	-.267	---	-0.228	.024	---	-.243	---
-0.252	.023	---	-.245	---	-0.178	.020	---	-.226	---
-0.202	.020	---	-.227	---	-0.128	.018	---	-.210	---
-0.152	.018	---	-.212	---	-0.078	.015	---	-.197	---
-0.102	.015	---	-.199	---	-0.028	.014	---	-.185	---
-0.052	.014	---	-.187	---	.022	.012	---	-.174	---
-.002	.012	---	-.176	---	.072	.011	---	-.165	---
.048	.011	---	-.167	---	.122	.010	---	-.157	---
.098	.010	---	-.158	---	.172	.009	---	-.149	---
.148	.009	---	-.151	---	.222	.008	---	-.142	---
.198	.008	---	-.144	---	.272	.007	---	-.136	---
.248	.007	---	-.138	---	.322	.007	---	-.131	---
.298	.007	---	-.132	---	.372	.006	---	-.125	---
.348	.006	---	-.127	---	.422	.006	---	-.120	---
.398	.006	---	-.122	---					
.448	.005	---	-.117	---					
$\bar{F} = 0.296$					$\bar{F} = 0.296$				
-0.704	0	---	0	---	-0.704	0	---	0	---
-0.654	-1.204	---	-.654	---	-0.654	-1.204	---	-.654	---
-0.604	1.769	---	1.769	---	-0.604	1.769	---	1.769	---
-0.554	.295	---	.295	---	-0.554	.295	---	.295	---
-0.504	.133	---	.133	---	-0.504	.133	---	.133	---
-0.454	.085	---	.085	---	-0.454	.085	---	.085	---
-0.404	.061	---	.061	---	-0.404	.061	---	.061	---
-0.354	.046	---	.046	---	-0.354	.046	---	.046	---
-0.304	.036	---	.036	---	-0.304	.036	---	.036	---
-0.254	.030	---	.030	---	-0.254	.030	---	.030	---
-0.204	.025	---	.025	---	-0.204	.025	---	.025	---
-0.154	.021	---	.021	---	-0.154	.021	---	.021	---
-0.104	.018	---	.018	---	-0.104	.018	---	.018	---
-0.054	.016	---	.016	---	-0.054	.016	---	.016	---
-.004	.014	---	.014	---	-.004	.014	---	.014	---
.046	.012	---	.046	---	.046	.012	---	.046	---
.096	.011	---	.096	---	.096	.011	---	.096	---
.146	.010	---	.146	---	.146	.010	---	.146	---
.196	.009	---	.196	---	.196	.009	---	.196	---
.246	.008	---	.246	---	.246	.008	---	.246	---
.296	.007	---	.296	---	.296	.007	---	.296	---
.346	.007	---	.346	---	.346	.007	---	.346	---
.396	.006	---	.396	---	.396	.006	---	.396	---
.446	.006	---	.446	---	.446	.006	---	.446	---

TABLE V. - VALUES OF  $M_{2\bar{x}}$  AND  $N_{2\bar{x}}$ .

$\bar{x}$	$M_{2\bar{x}}$		$N_{2\bar{x}}$		$\bar{x}$	$M_{2\bar{x}}$		$N_{2\bar{x}}$		$\bar{x}$	$M_{2\bar{x}}$		$N_{2\bar{x}}$	
	Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic	Exact	Asymp-totic		Exact	Asymp-totic		
$F = 0.148$					$F = 0.222$					$F = 0.296$				
-0.852	0	-	0	-	-0.778	0	-	0	-	-0.70b	0	-	0	-
- .802	-3.16	-	- .31	-	- .738	-2.18	-	- .29	-	- .65b	-1.72	-	- .27	-
- .752	- .92	-	- .4.05	-	- .678	1.22	-	-3.04	-	- .60b	1.25	-	-2.52	-
- .702	- .85	-	-3.28	-	- .668	- .30	-	-2.05	-	- .55b	- .13	-	-1.52	-
- .652	- .93	-	-3.91	-	- .598	- .38	-	-2.27	-	- .50b	- .19	-	-1.60	-
- .602	- .95	-	-4.61	-	- .528	- .41	-	-2.56	-	- .45b	- .22	-	-1.74	-
- .552	- .96	-	-5.28	-	- .478	- .42	-	-2.86	-	- .40b	- .23	-	-1.90	-
- .502	- .96	-	-6.04	-	- .428	- .42	-	-3.18	-	- .35b	- .23	-	-2.07	-
- .452	- .96	-0.97	-6.76	-6.75	- .378	- .42	-0.43	-3.49	-3.48	- .30b	- .24	-0.24	-2.24	-2.23
- .402	- .97	- .97	-7.49	-7.48	- .328	- .43	- .43	-3.81	-3.80	- .25b	- .24	- .24	-2.42	-2.41
- .352	- .97	- .97	-8.21	-8.21	- .278	- .43	- .43	-4.13	-4.12	- .20b	- .24	- .24	-2.60	-2.59

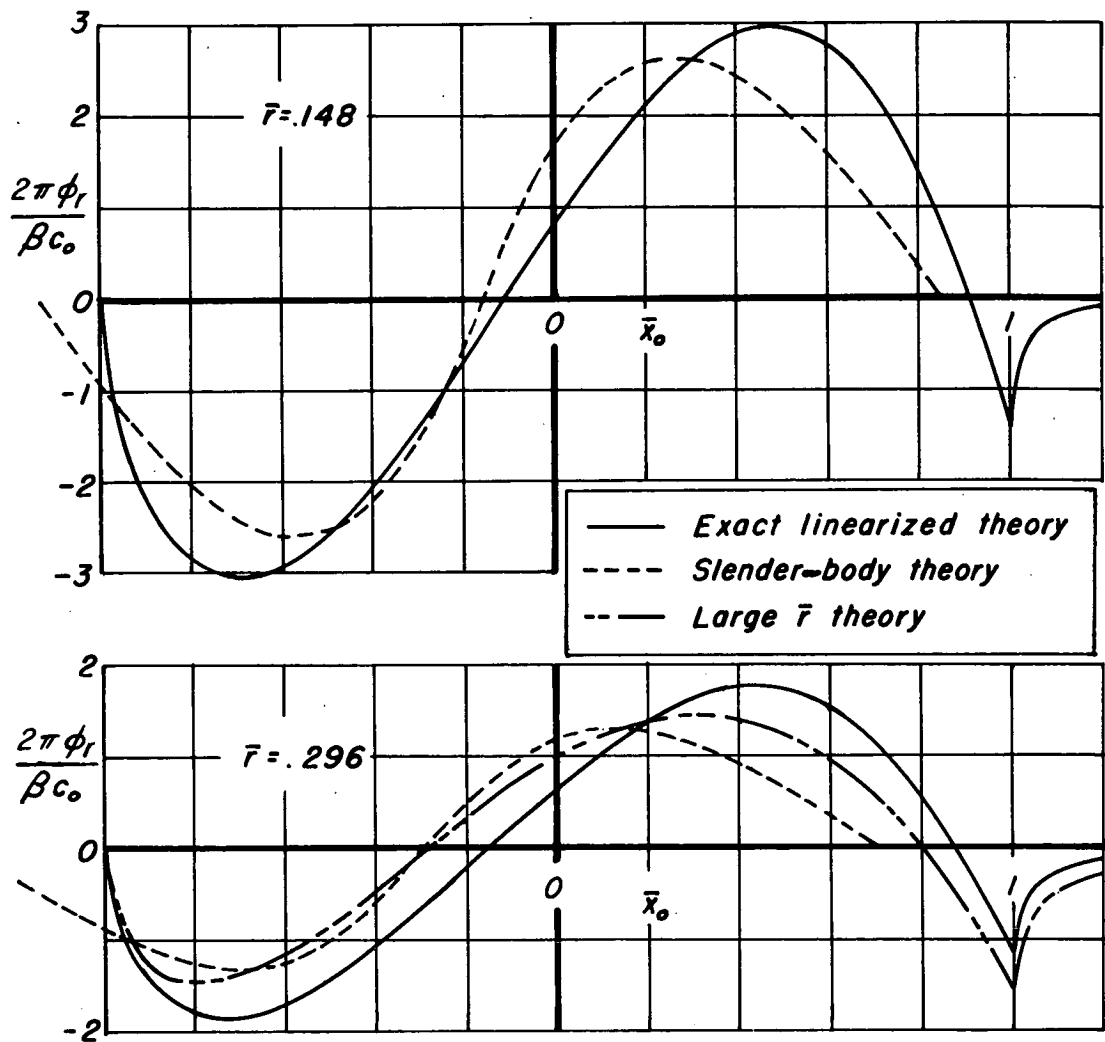


--- Radii at which velocities  $\phi_r$  and  $\phi_\theta$  are presented.



(a) Multipole distributions.

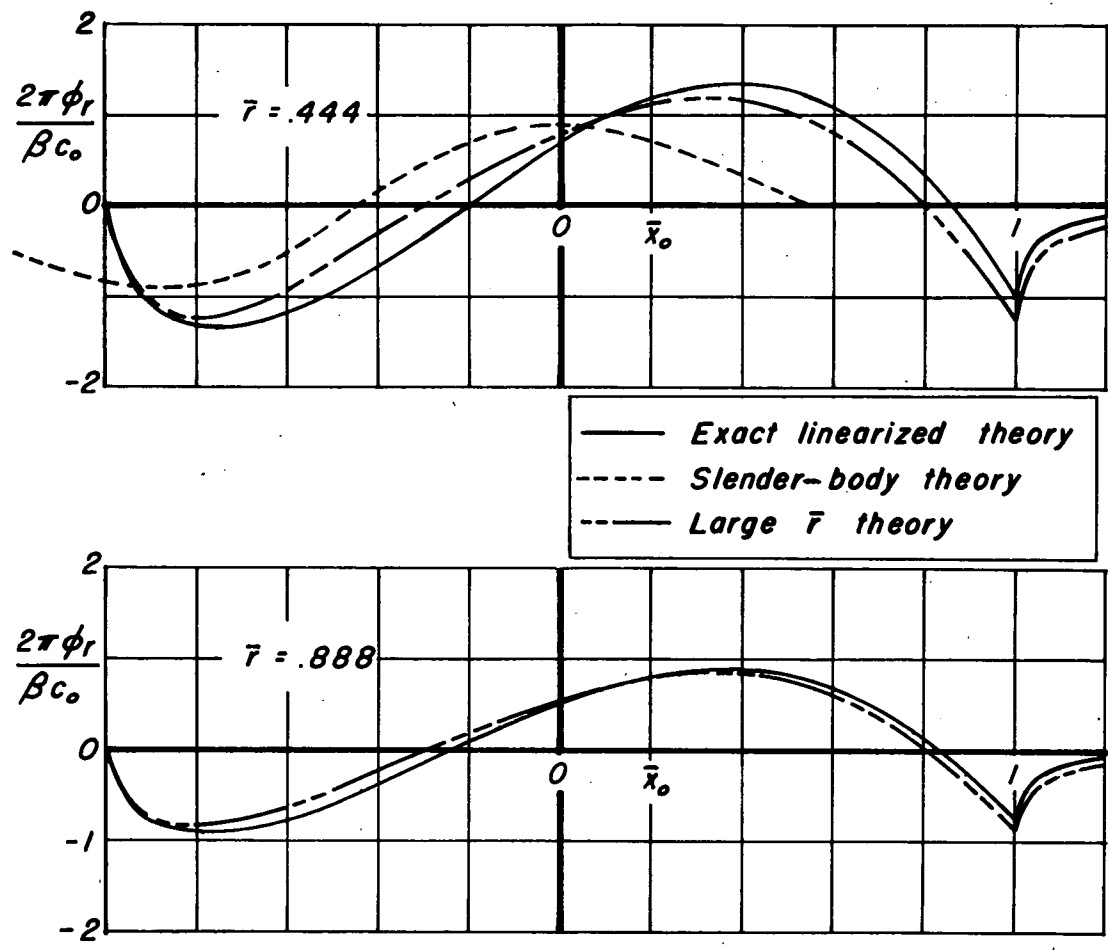
Figure 1.- Radial and tangential velocities induced by three different multipole distributions at four radii.



(b) Velocities,  $\phi_{or}$ .

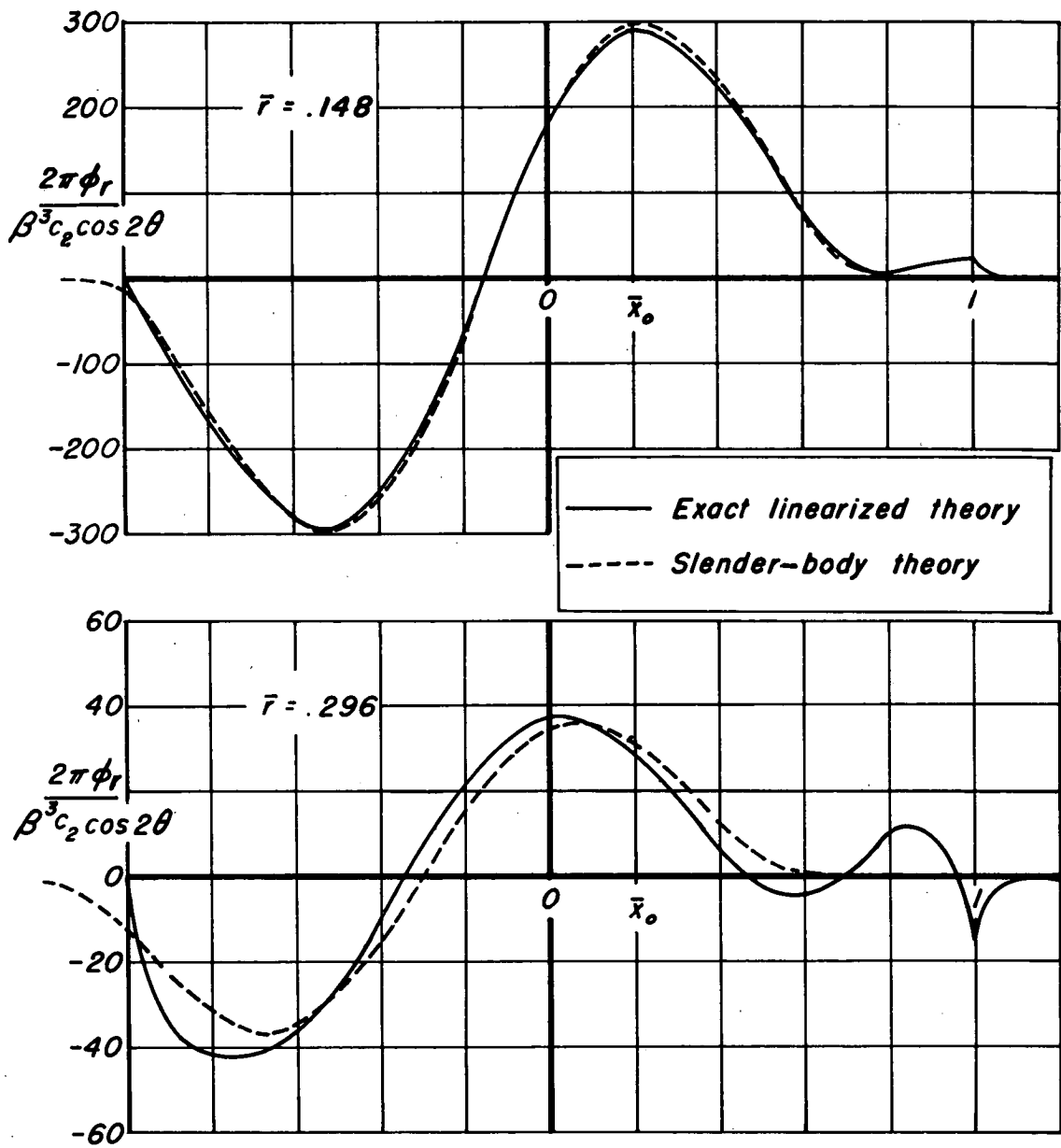
Figure 1.- Continued.





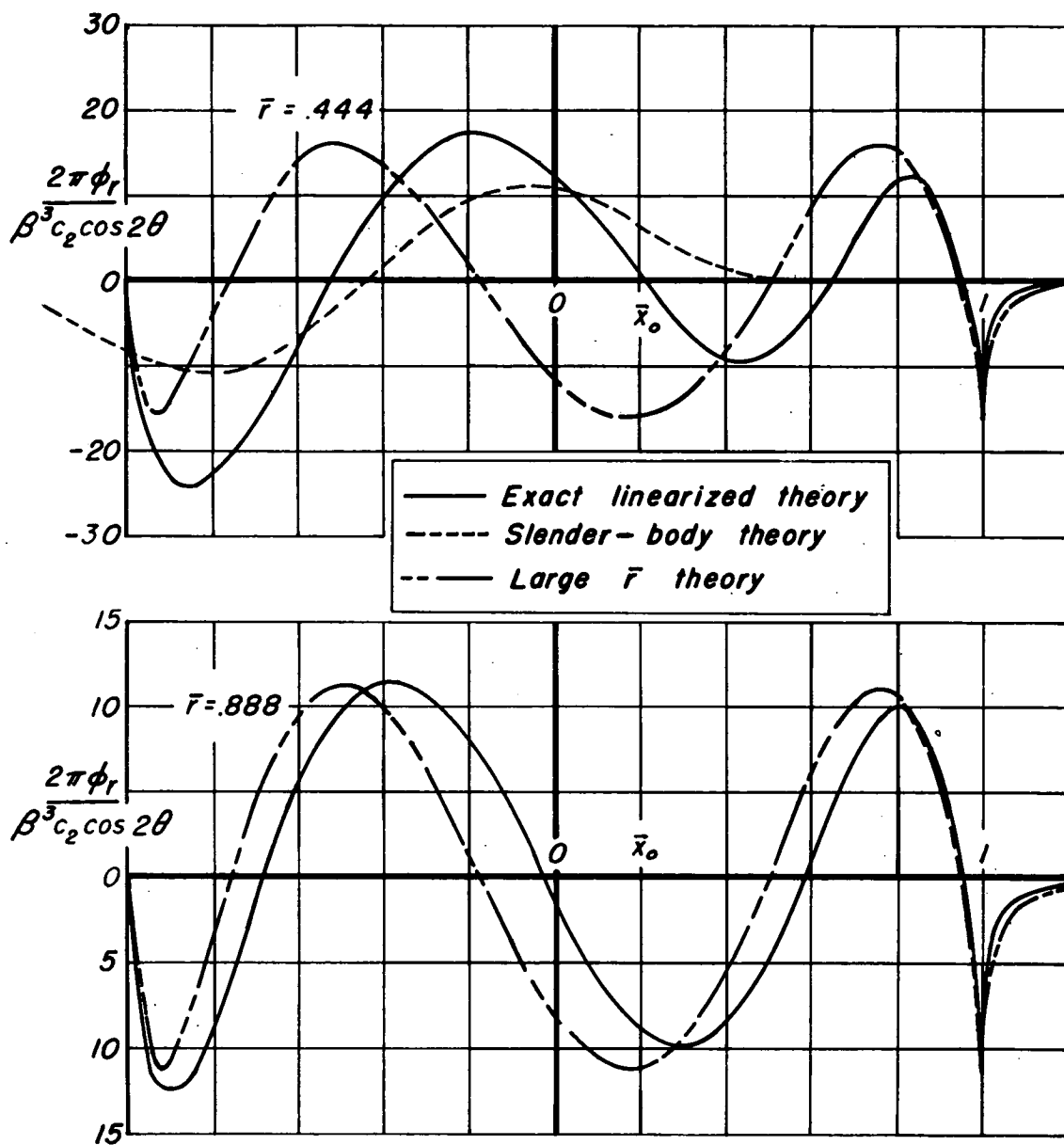
(b) Concluded.

Figure 1.- Continued.



(c) Velocities,  $\phi_{2r}$ .

Figure 1.- Continued.



(c) Concluded.

Figure 1.- Continued.

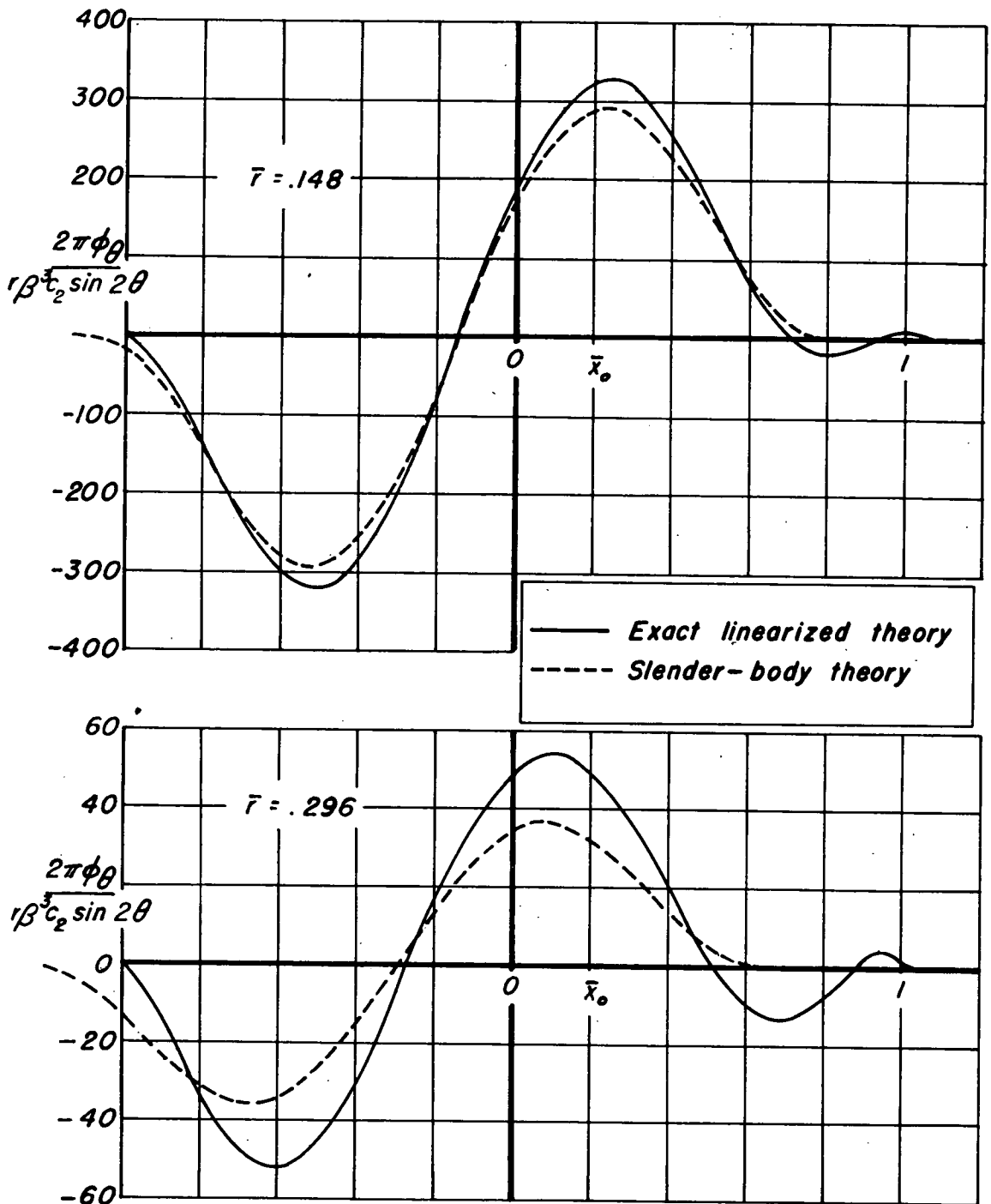
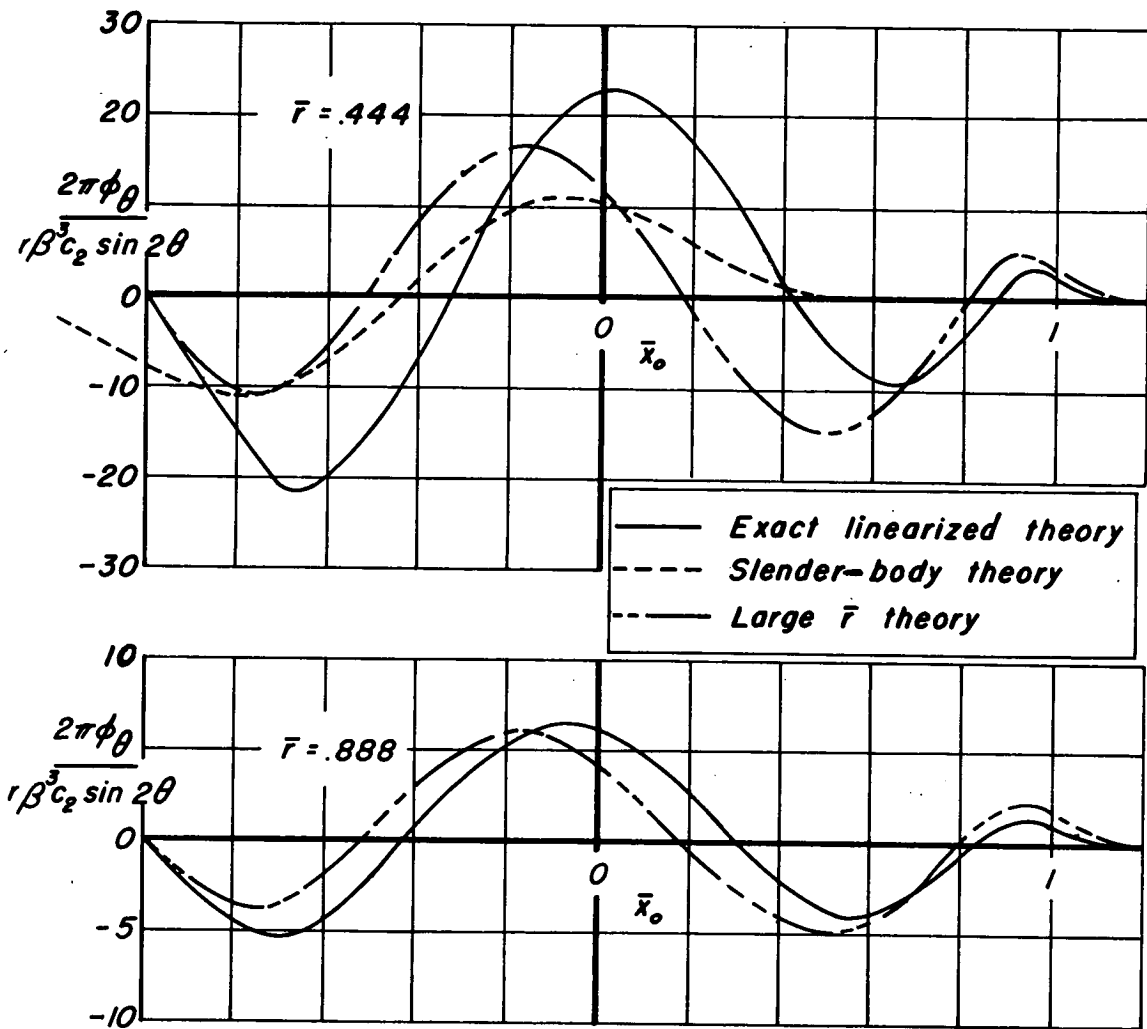
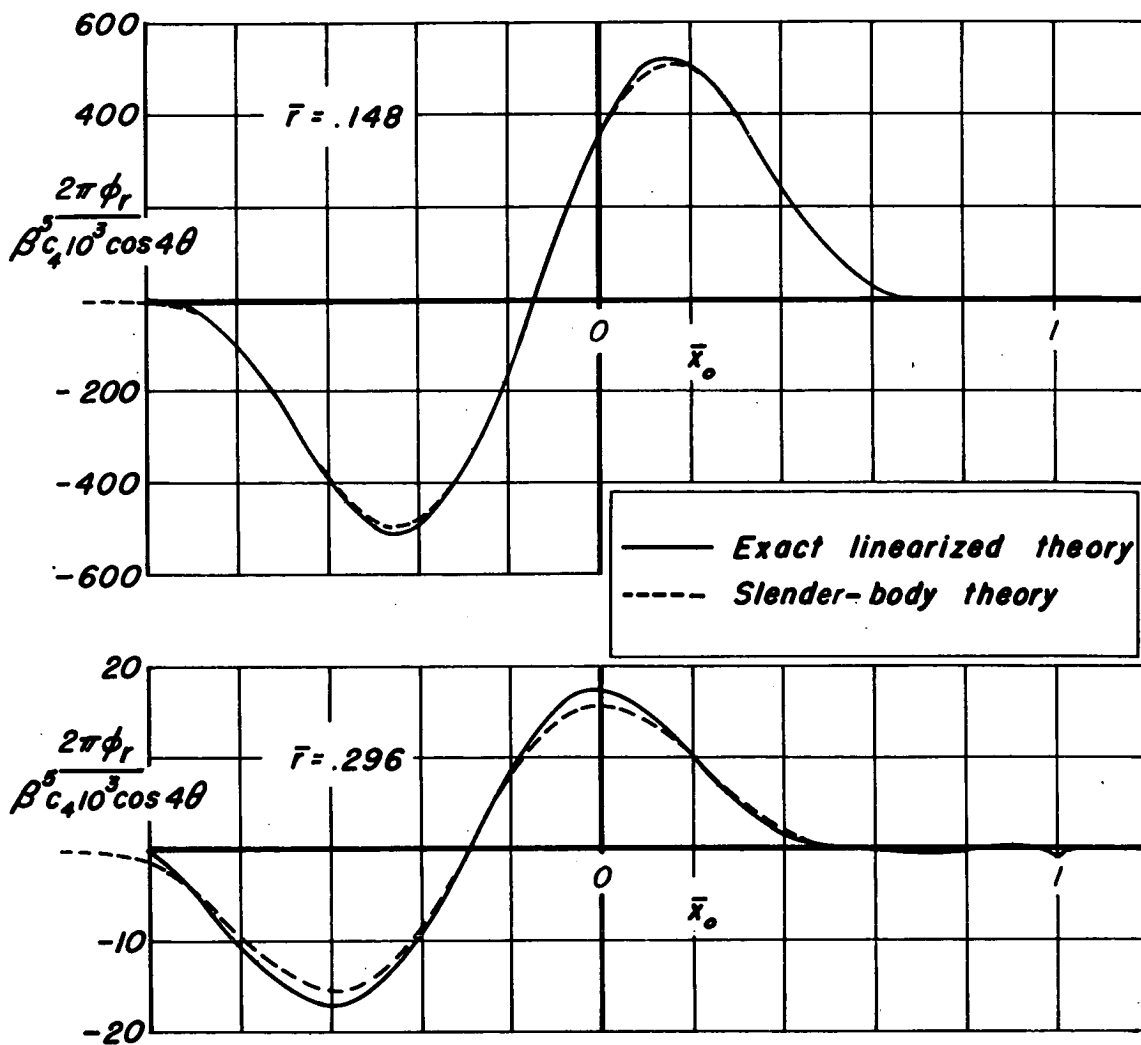
(d) Velocities,  $\phi_{2\theta}$ .

Figure 1.- Continued.



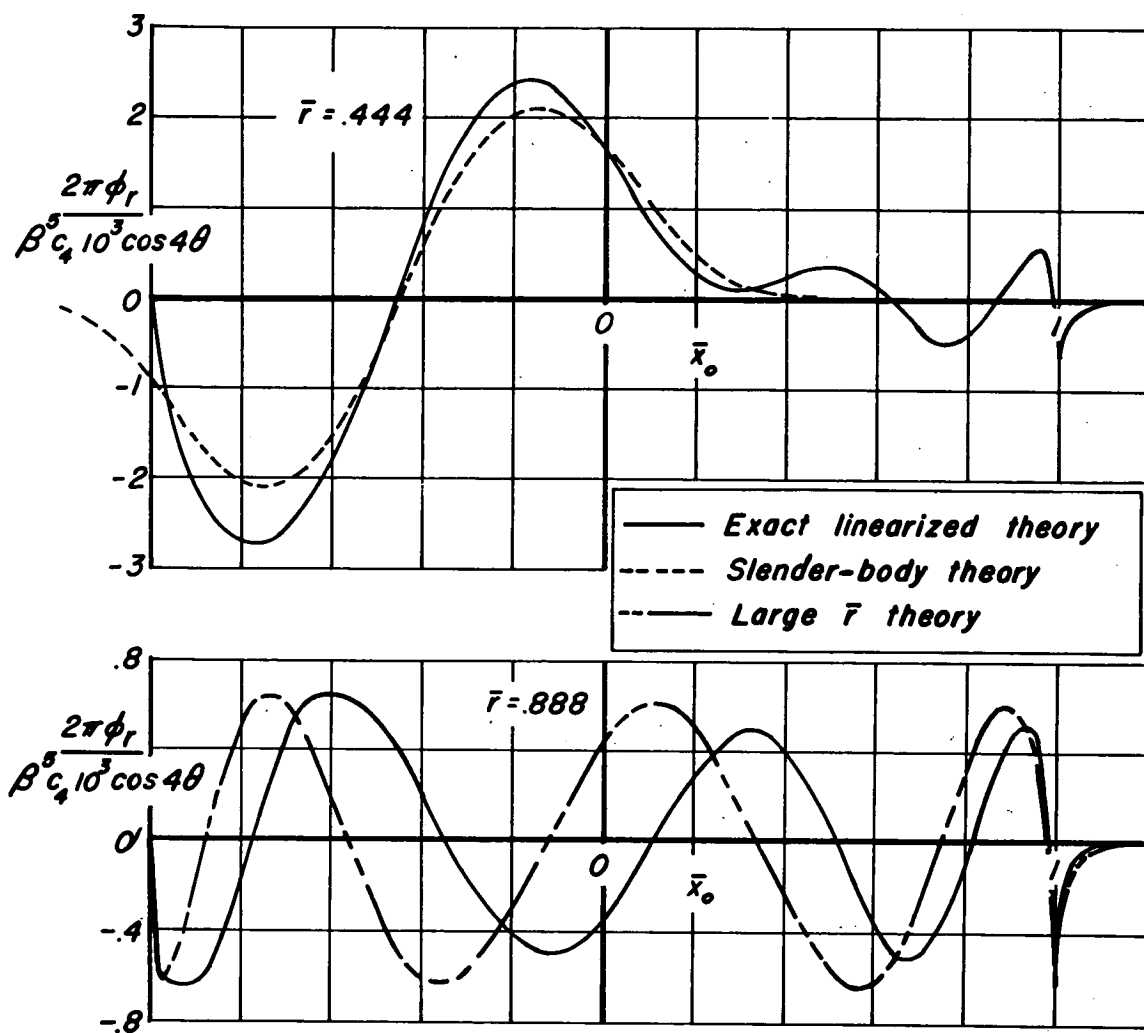
(d) Concluded.

Figure 1.- Continued.



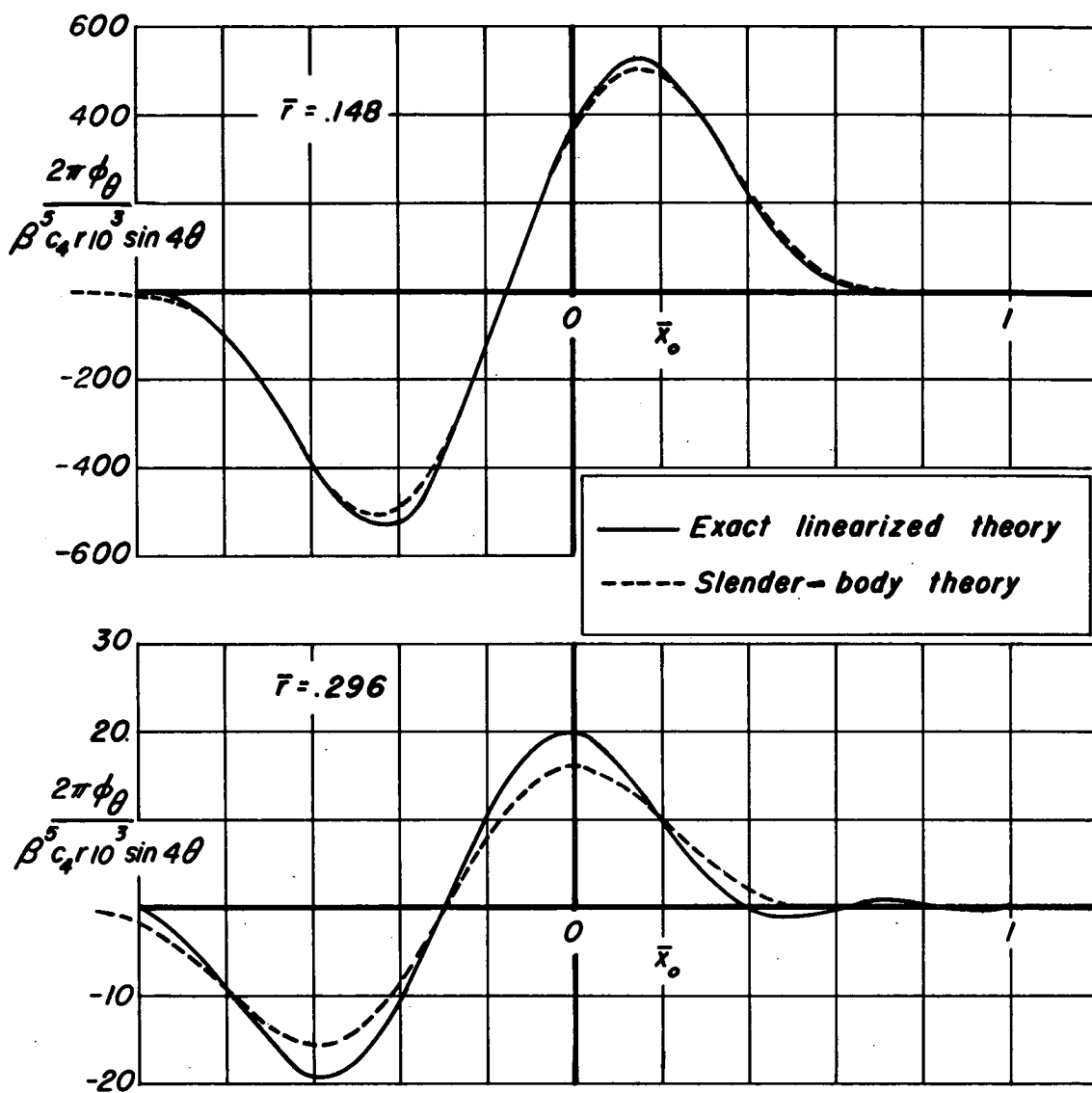
(e) Velocities,  $\phi_{4r}$ .

Figure 1.- Continued.



(e) Concluded.

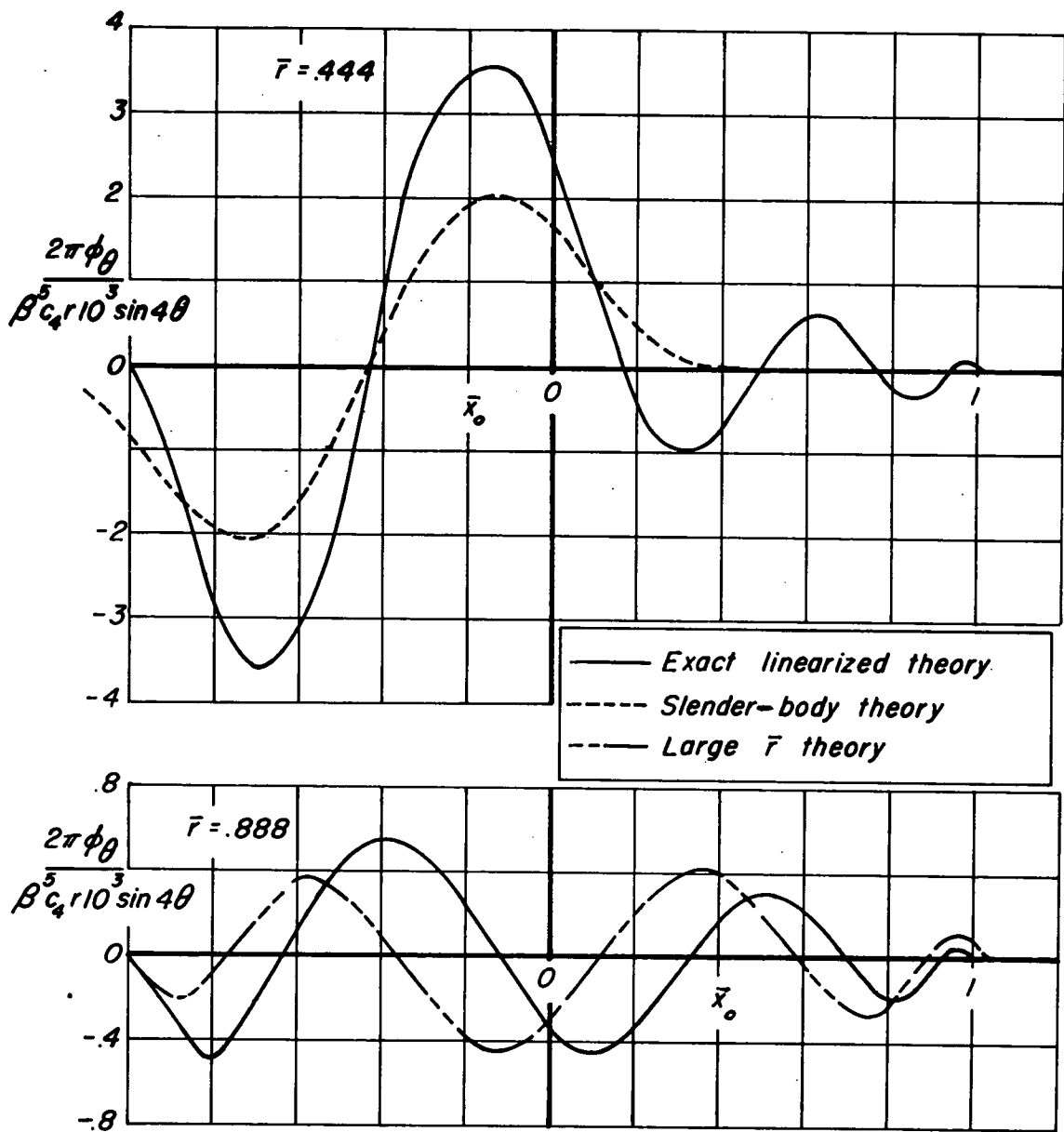
Figure 1.- Continued.



(f) Velocities,  $\phi_{4\theta}$ .

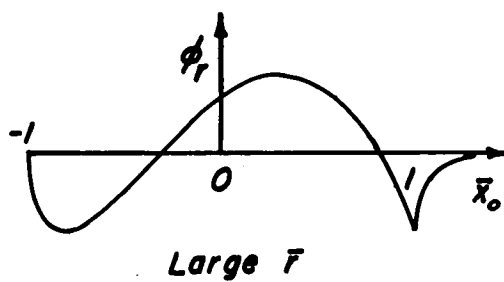
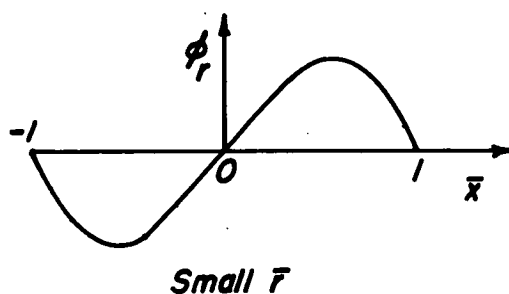
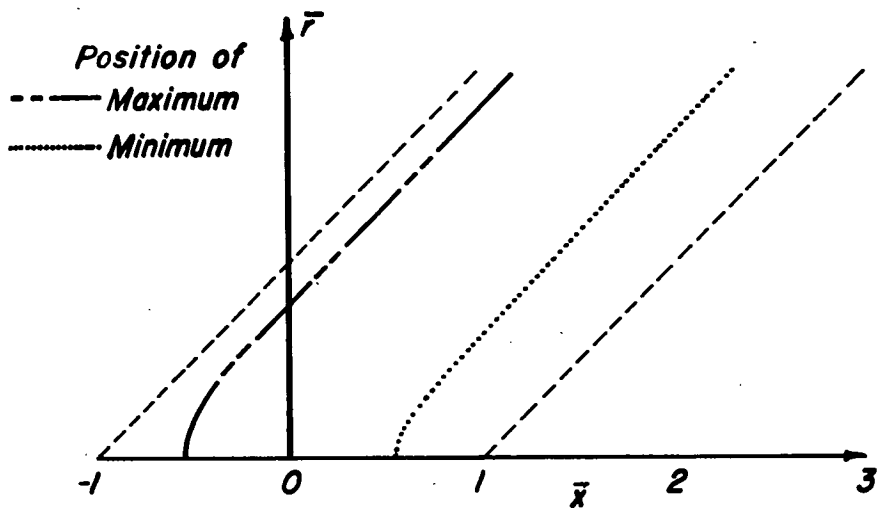
Figure 1.- Continued.





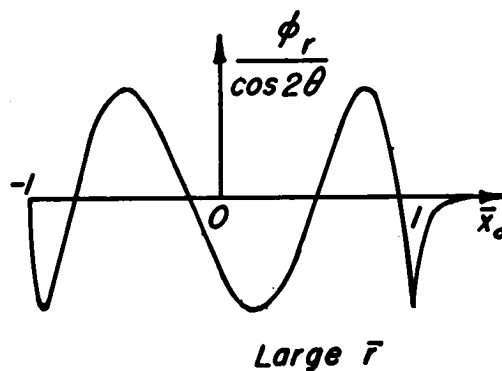
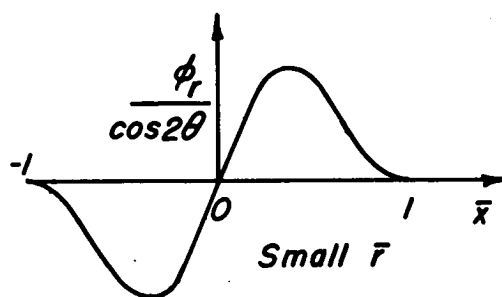
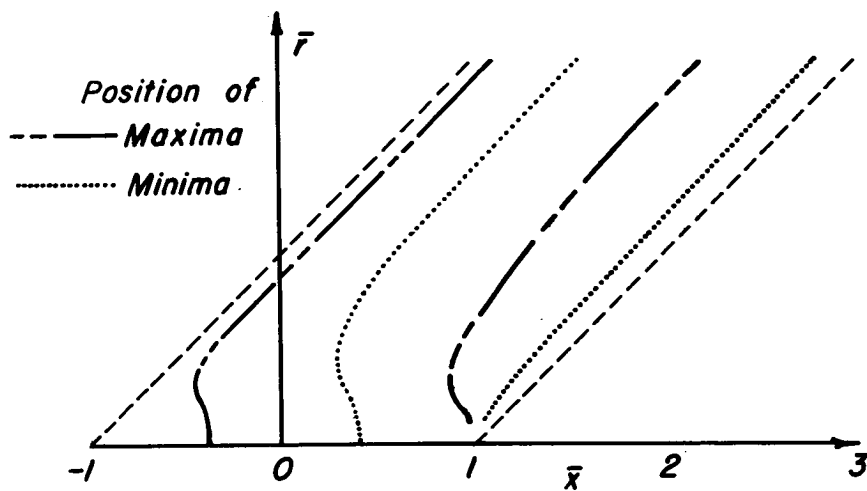
(f) Concluded.

Figure 1.- Concluded.



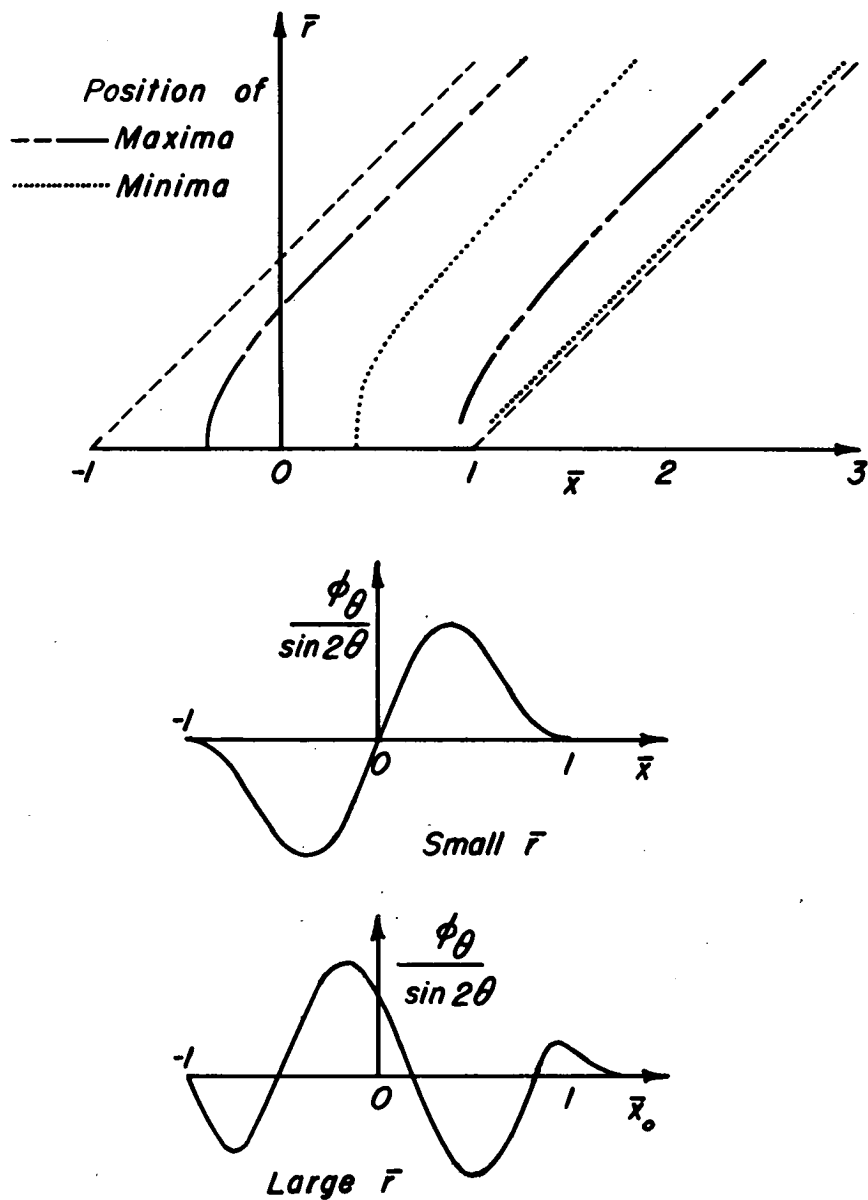
(a) Radial velocities induced by sources.

Figure 2.- Positions of crests of waves created by multipole distributions shown in figure 1.



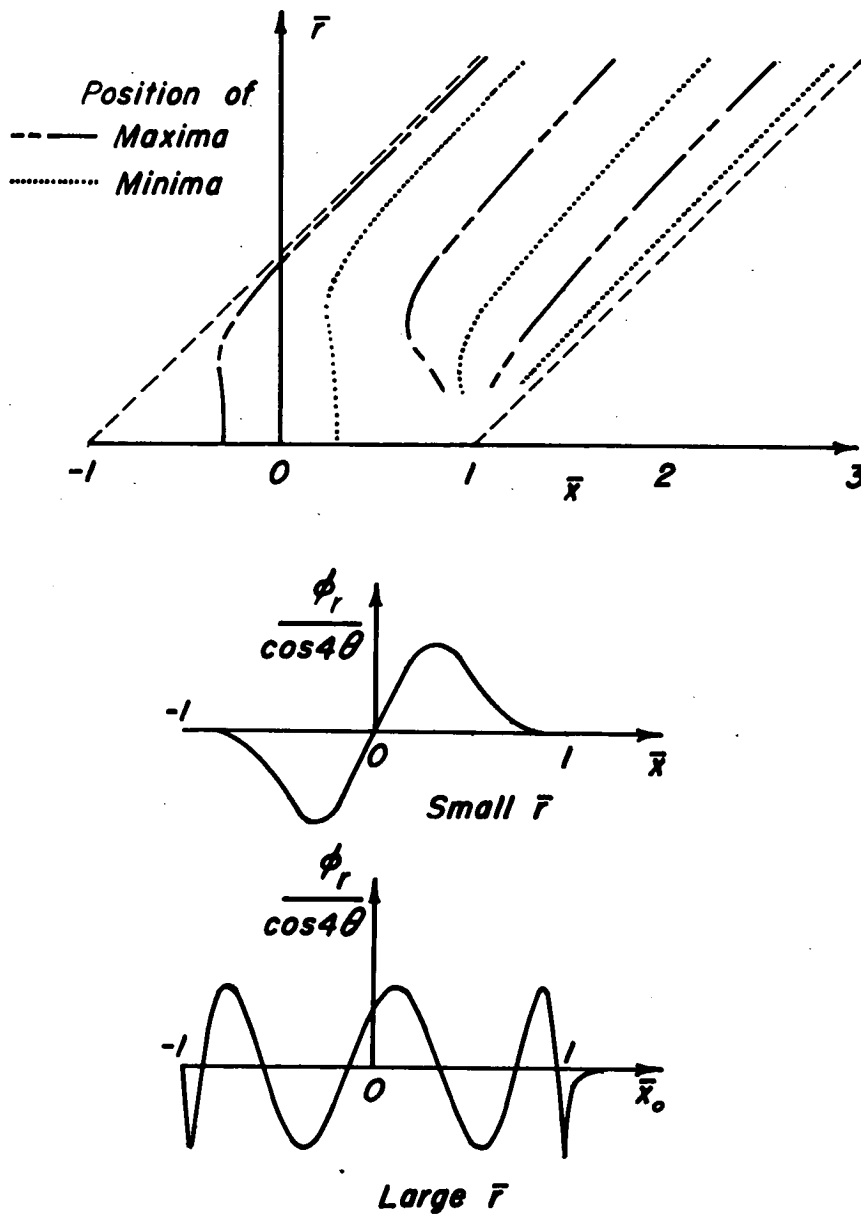
(b) Radial velocities induced by second-order multipoles.

Figure 2.- Continued.



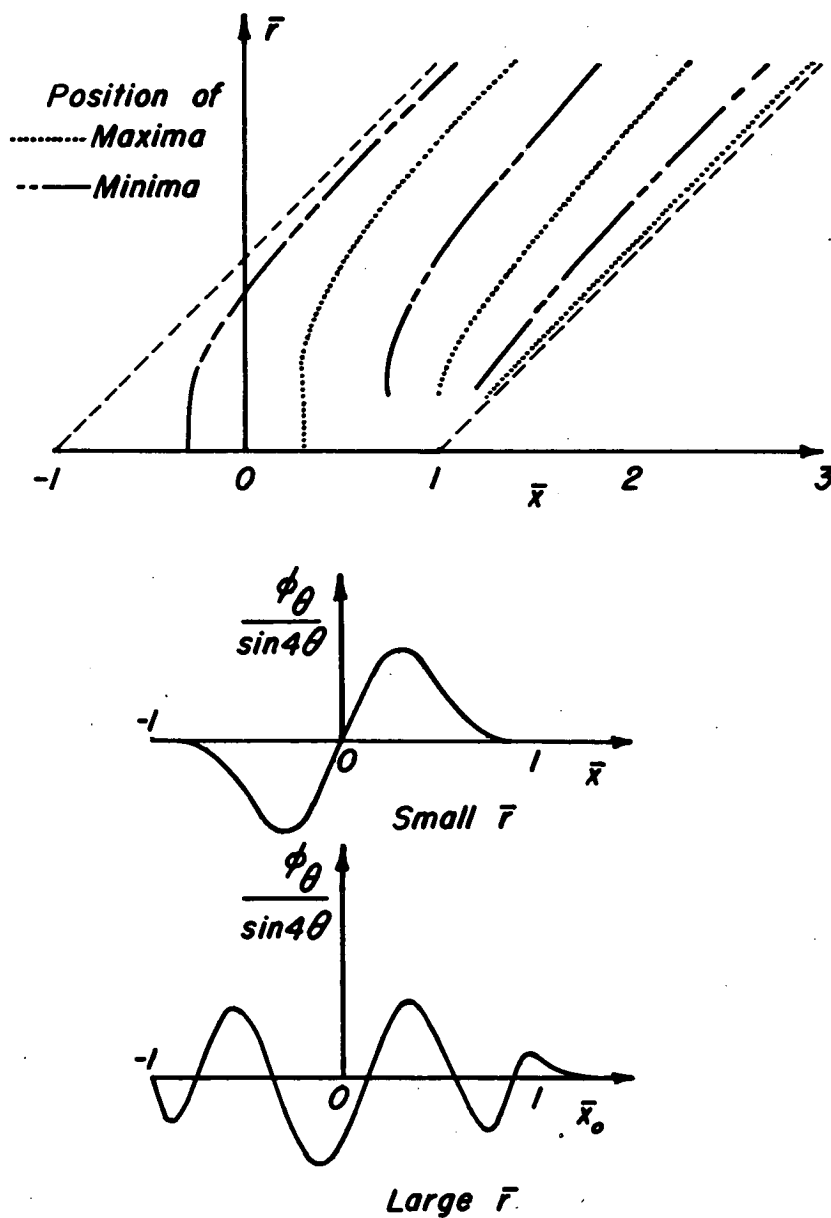
(c) Tangential velocities induced by second-order multipoles.

Figure 2.- Continued.



(d) Radial velocities induced by fourth-order multipoles.

Figure 2.- Continued.



(e) Tangential velocities induced by fourth-order multipoles.

Figure 2.- Concluded.

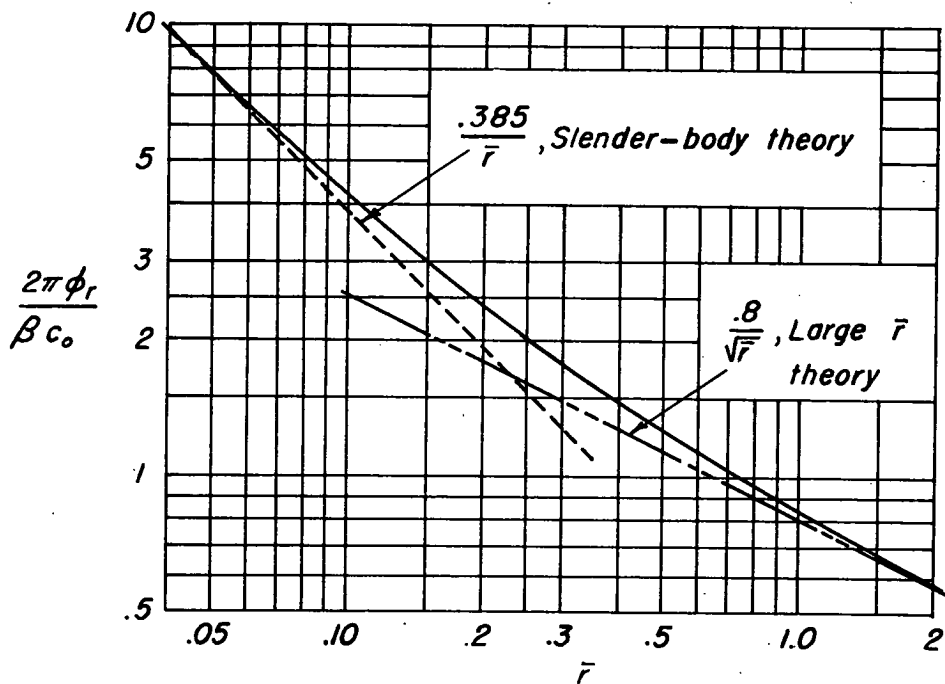
(a)  $\phi_{Or}$ 

Figure 3.- Attenuation of first crest of waves created by multipole distributions shown in figure 1.

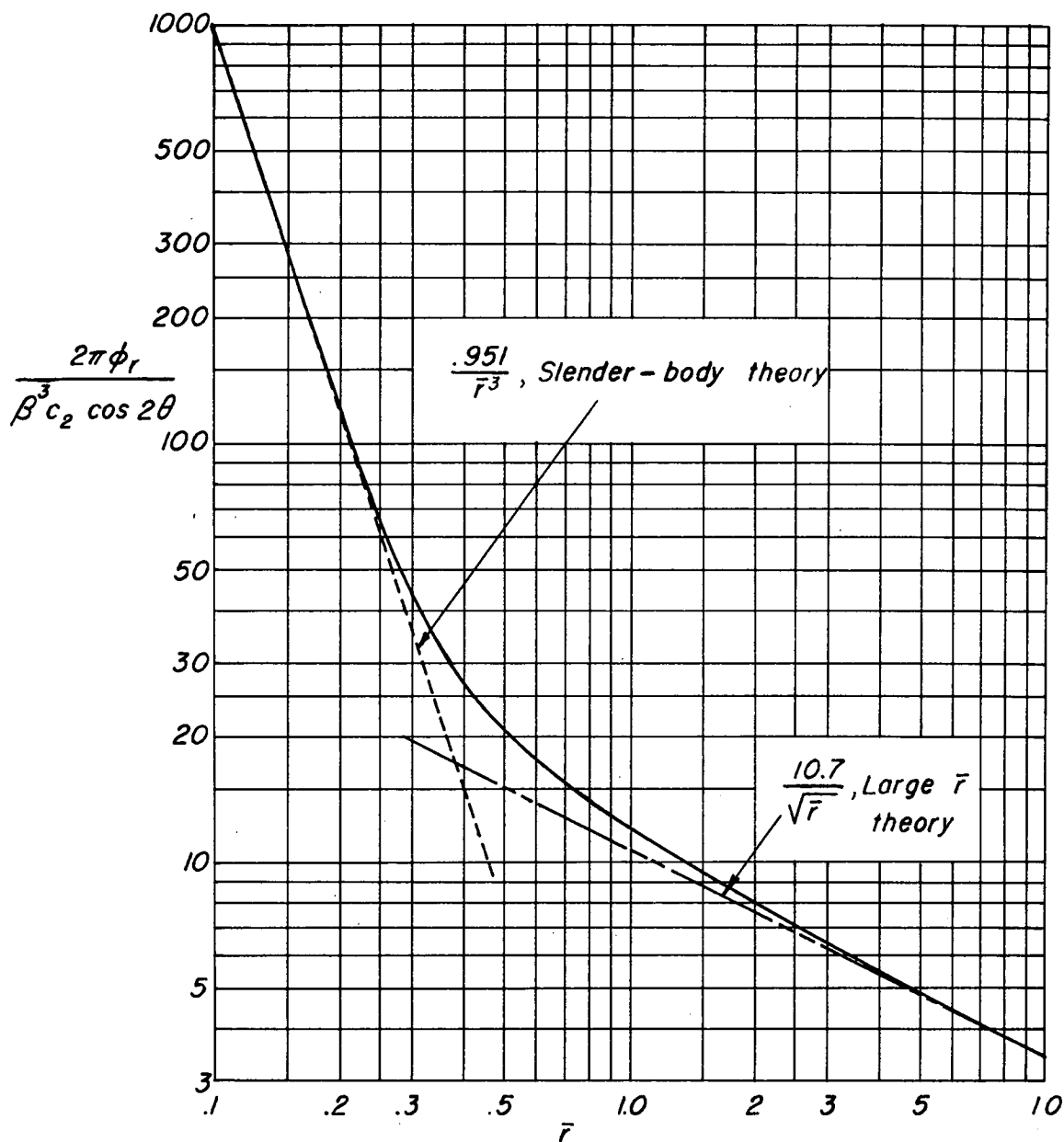
(b)  $\phi_{2r}$ 

Figure 3.- Continued.



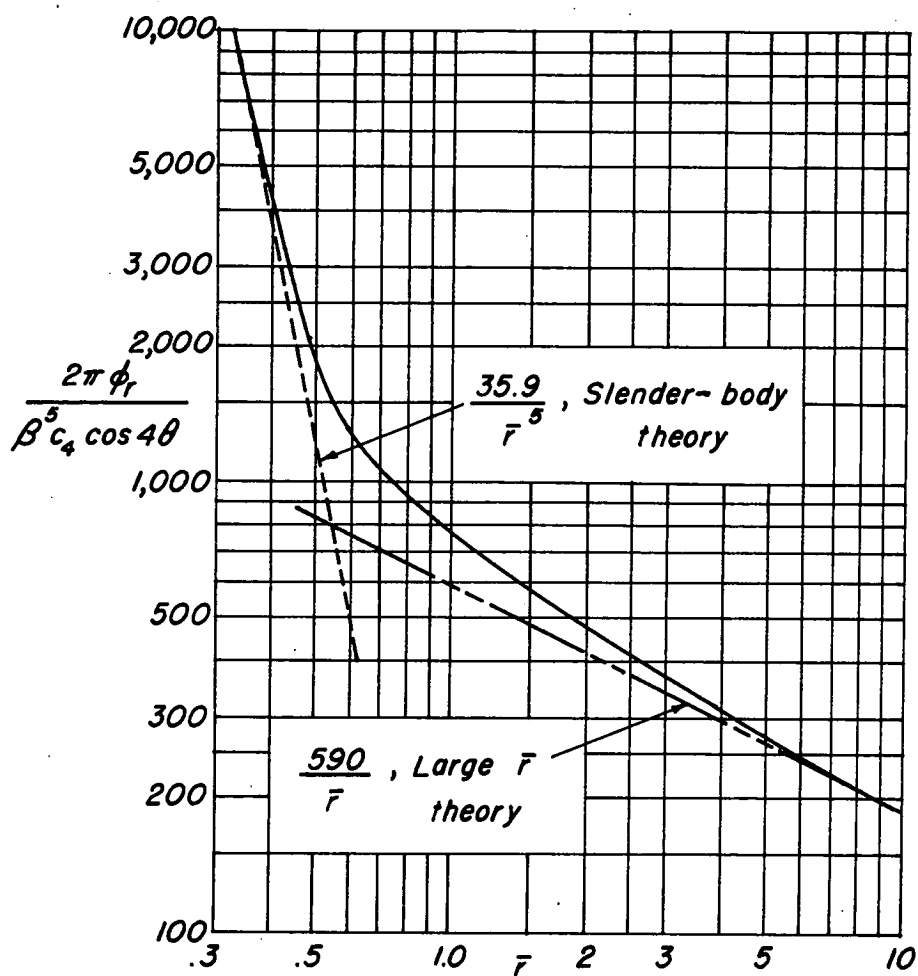
(c)  $\phi_{4r}$ 

Figure 3.- Continued.

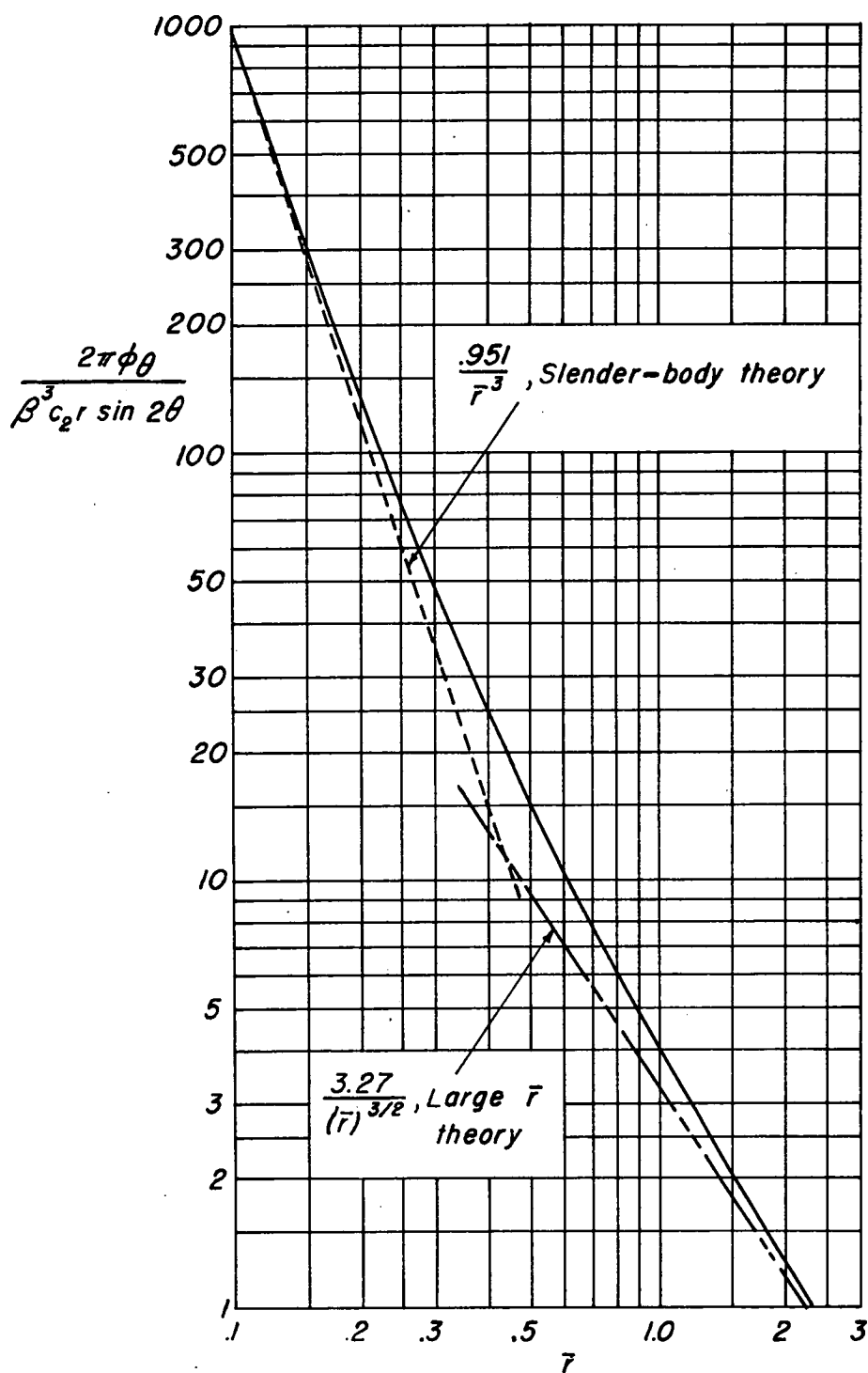
(d)  $\phi_{2\theta}$ 

Figure 3.- Continued.

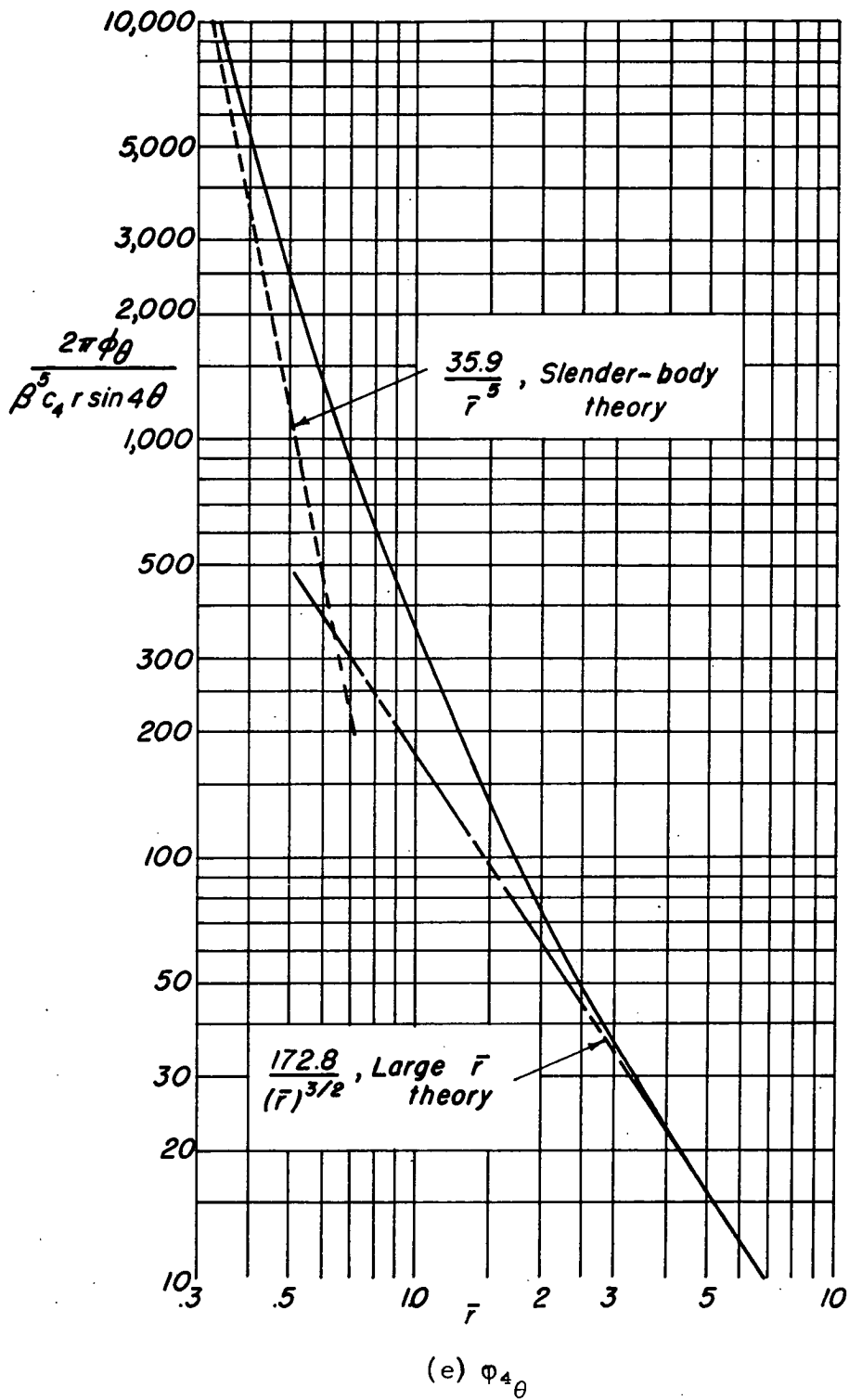
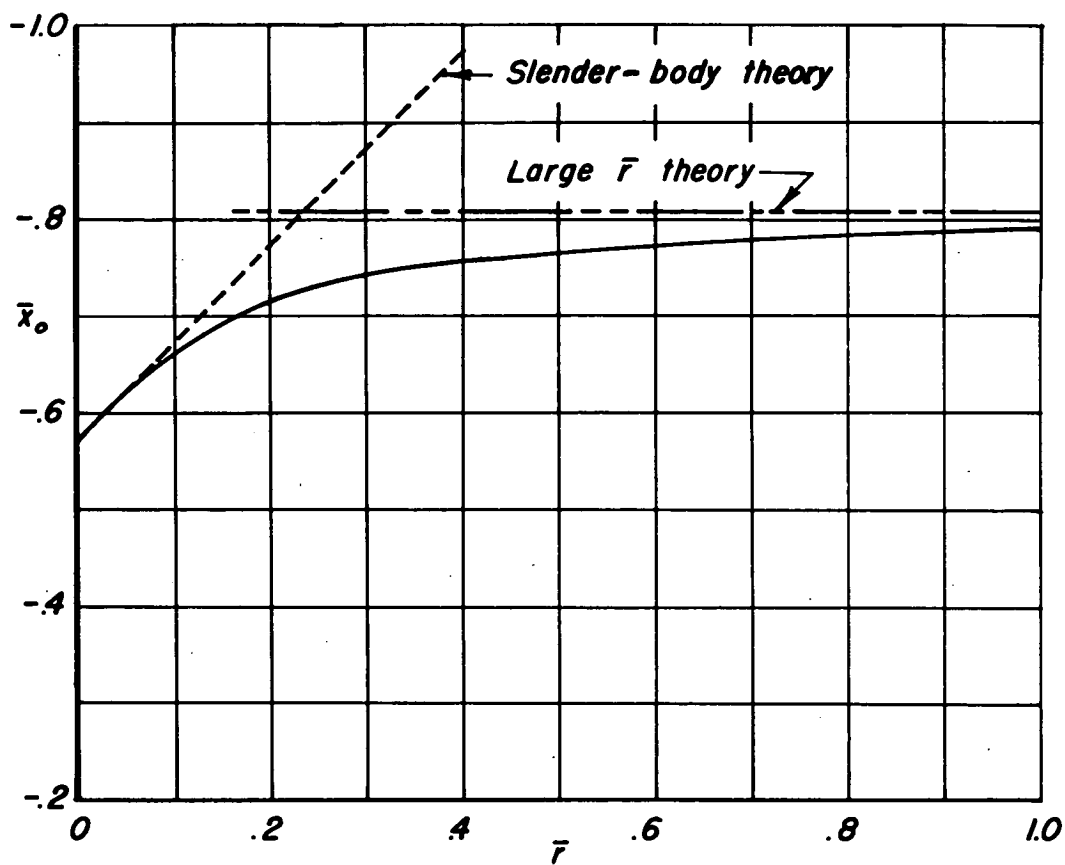
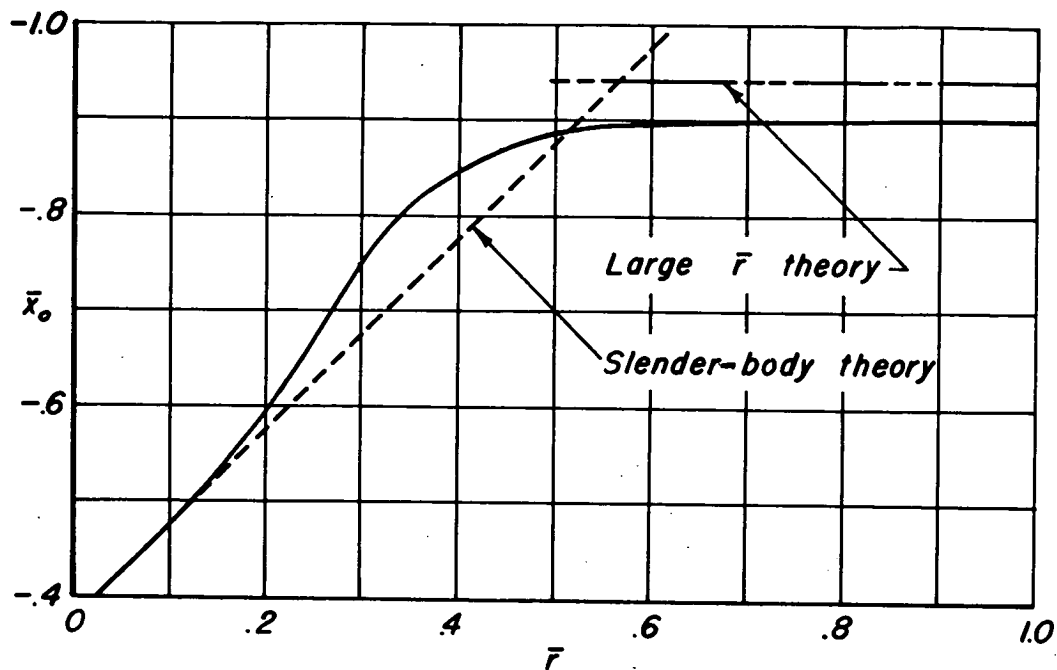


Figure 3.- Concluded.

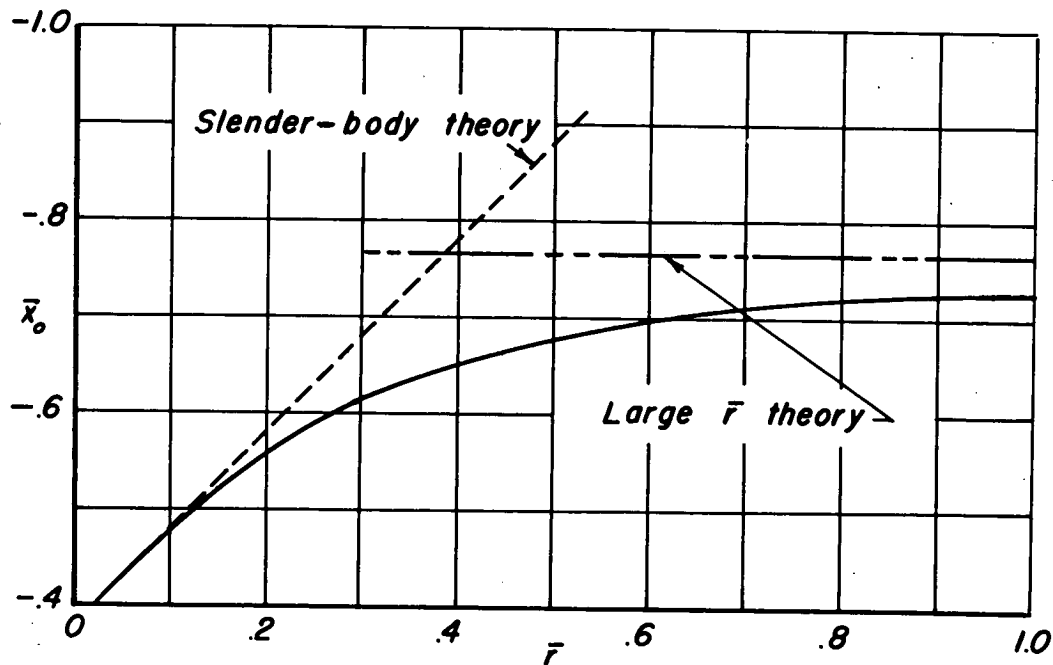


(a) Radial velocities induced by sources.

Figure 4.- Position of first crest of waves created by multipole distributions shown in figure 1.

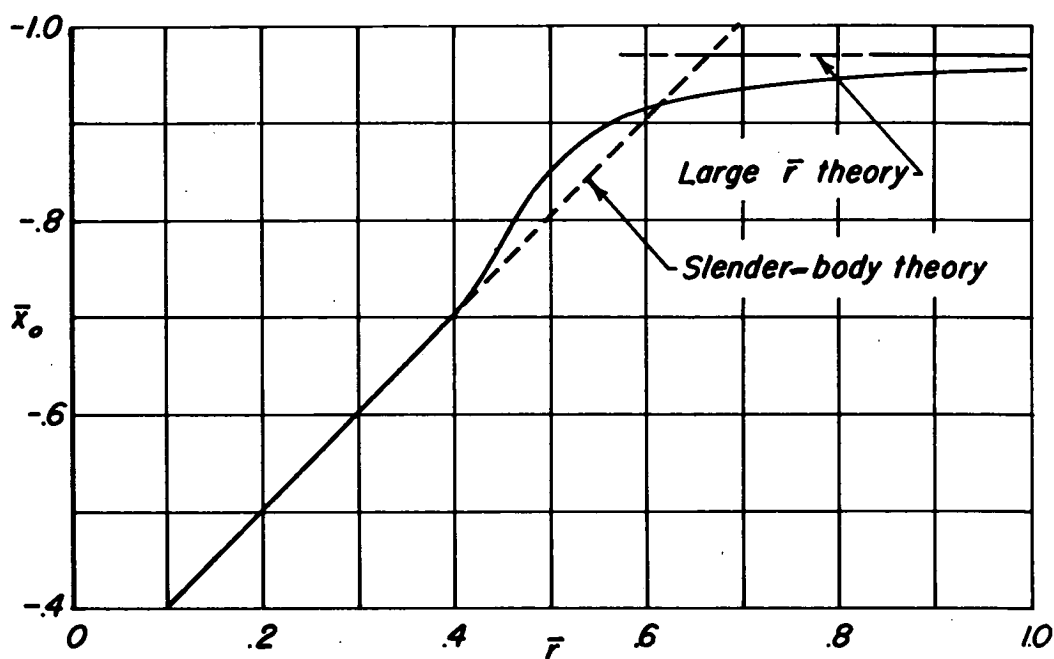


(b) Radial velocities induced by second-order multipoles.

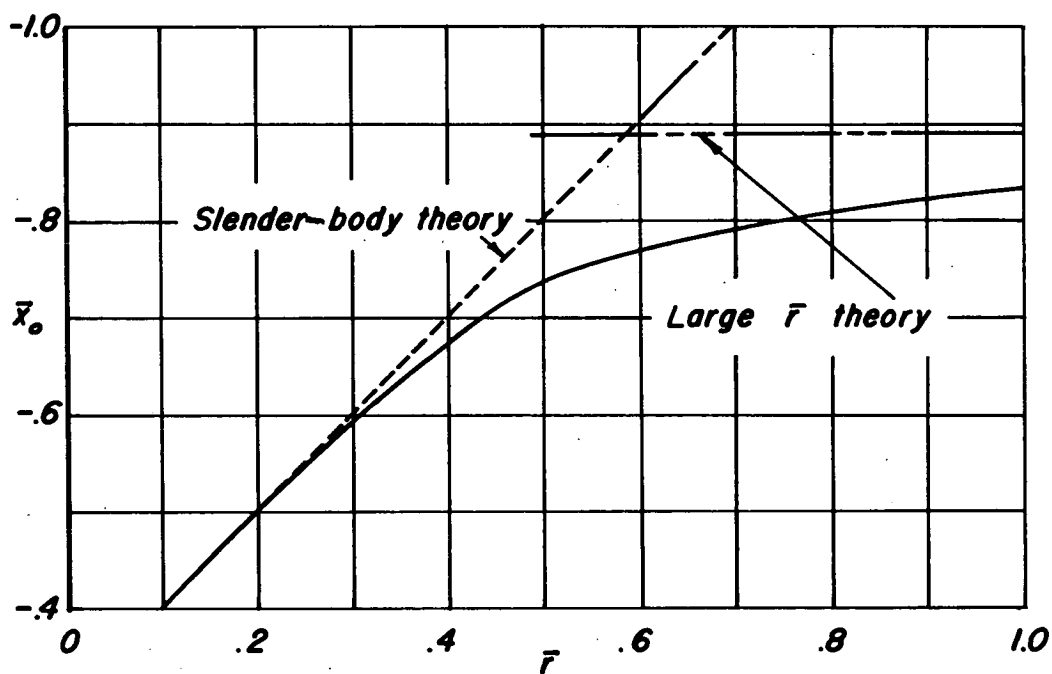


(c) Tangential velocities induced by second-order multipoles.

Figure 4.- Continued.

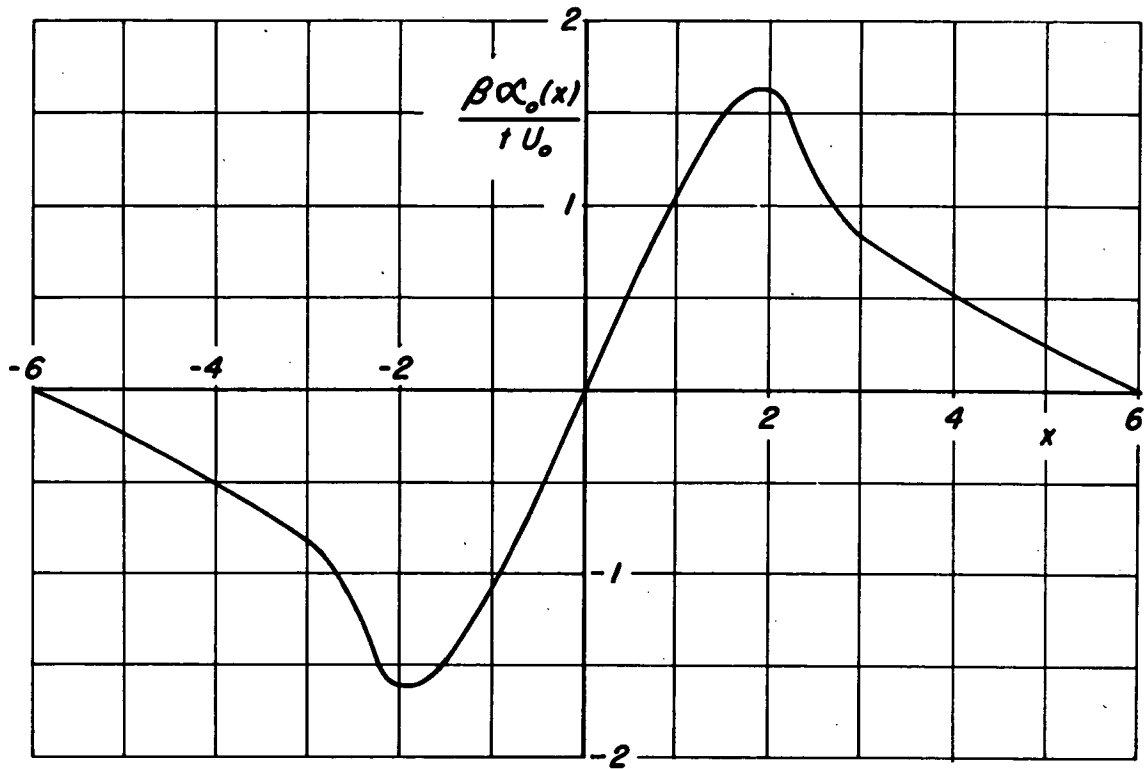


(d) Radial velocities induced by fourth-order multipoles.



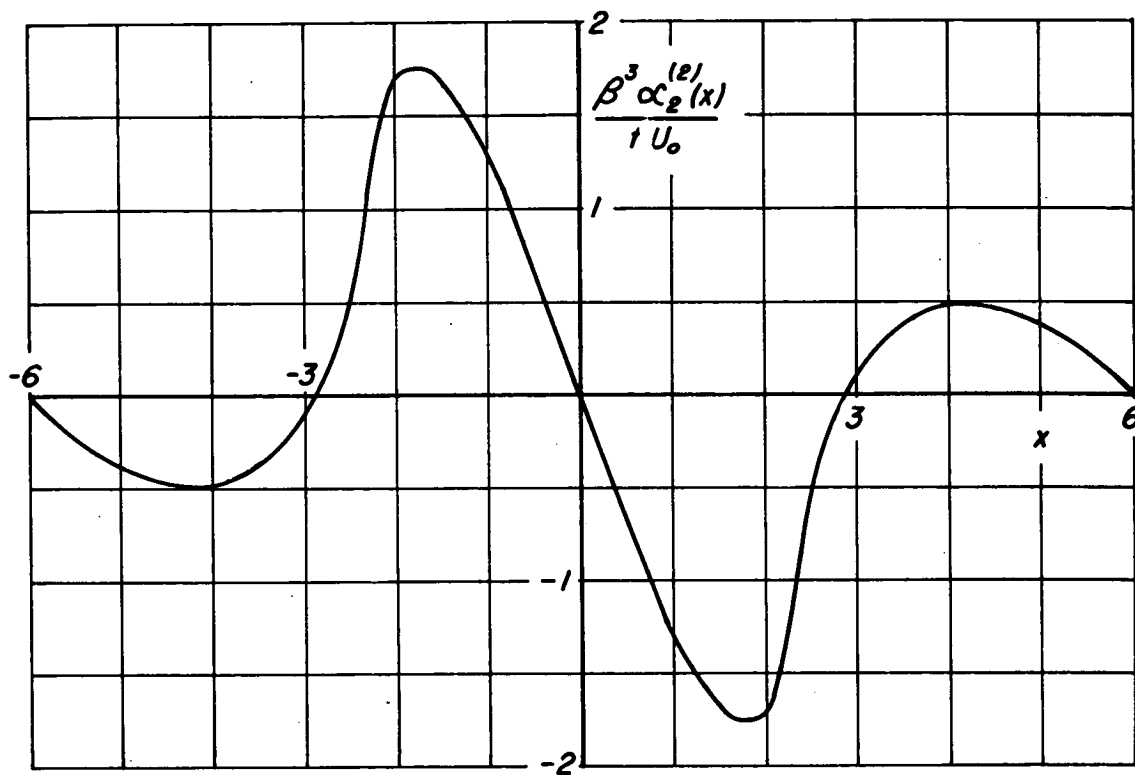
(e) Tangential velocities induced by fourth-order multipoles.

Figure 4.- Concluded.



(a)  $n = 0$

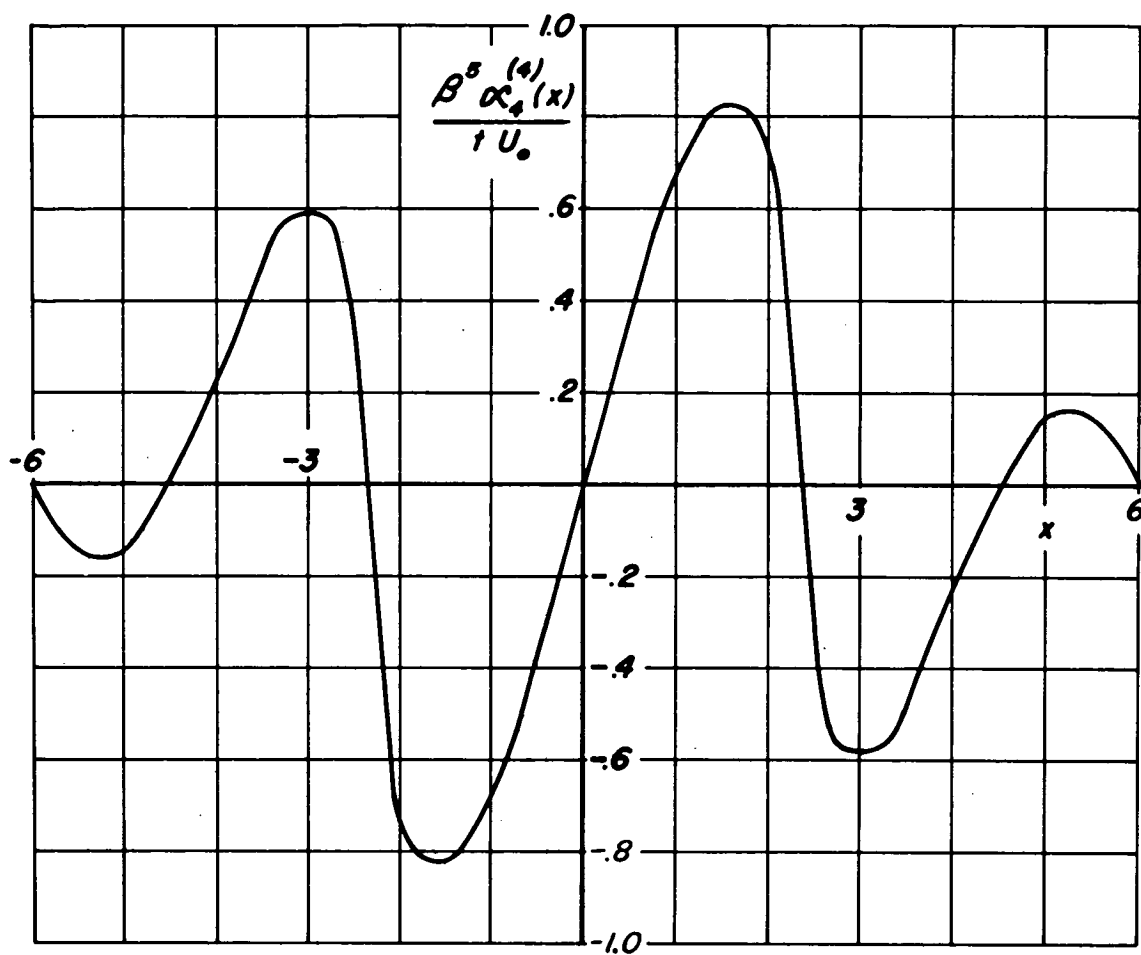
Figure 5.- Variation of  $n$ th derivative of  $n$ th-order cancellation multi-poles for elliptic wing.



(b)  $n = 2$

Figure 5.- Continued.





(c)  $n = 4$

Figure 5.- Concluded.

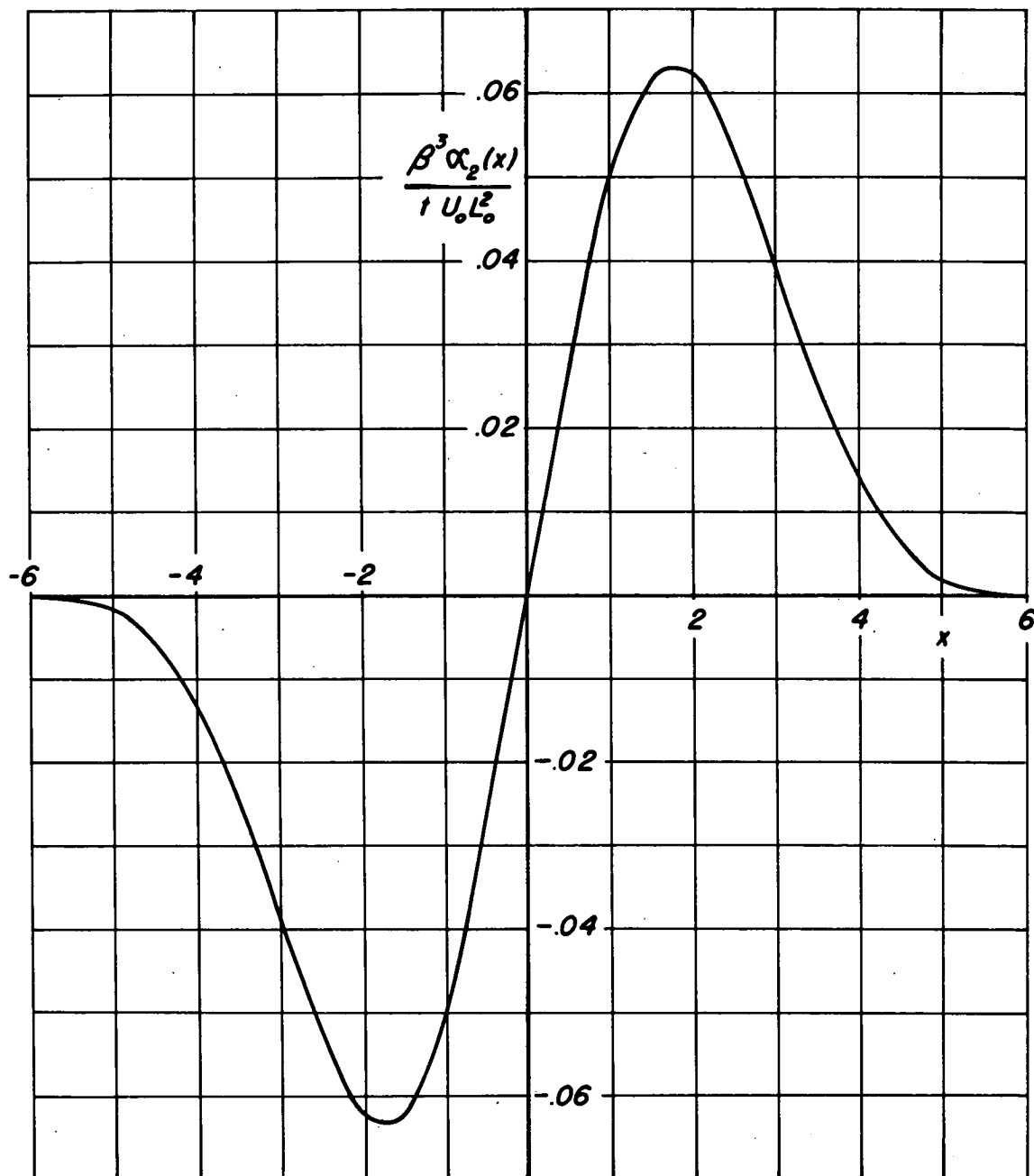
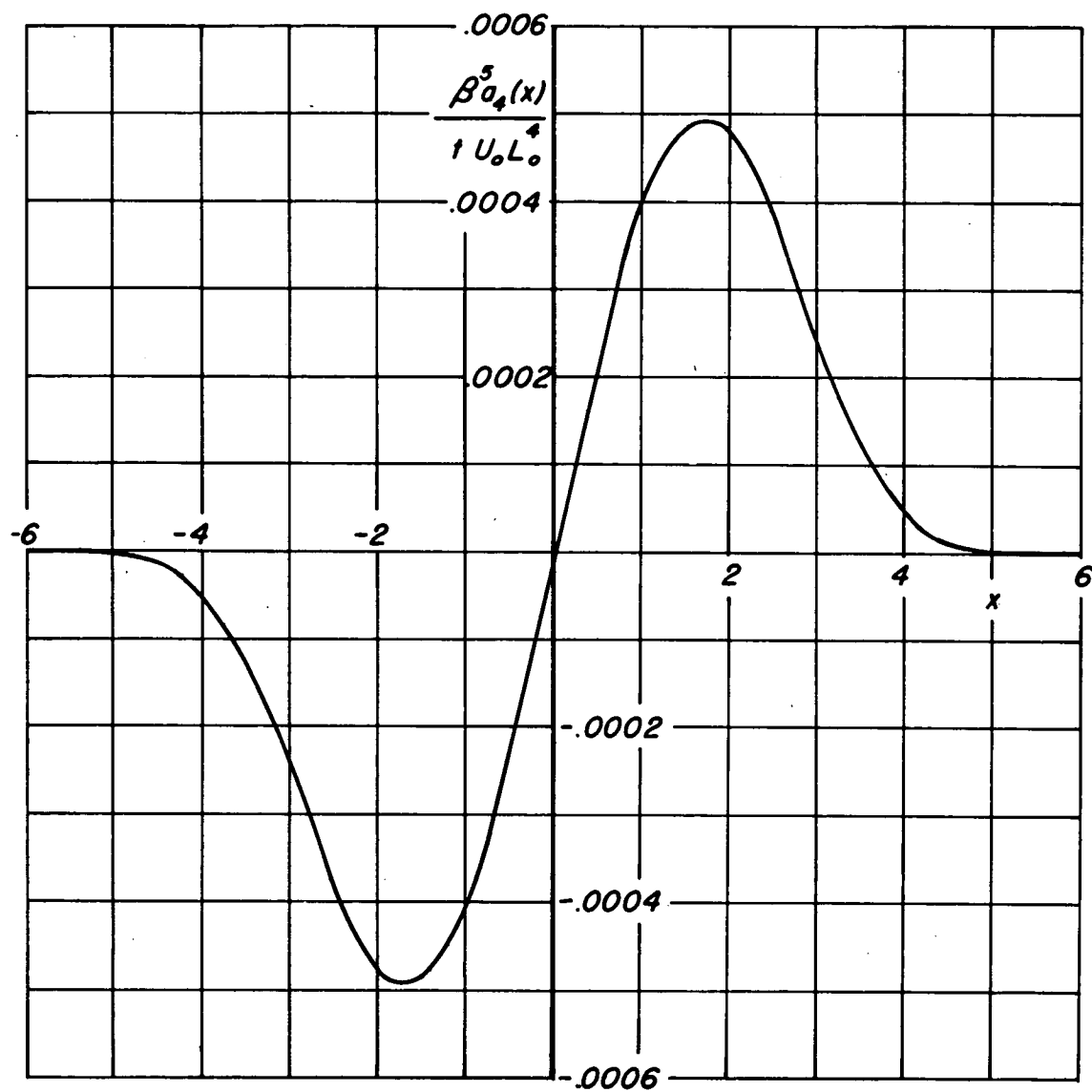
(a)  $n = 2$ 

Figure 6.- Variation of  $n$ th-order cancellation multipoles for elliptic wing.



(b)  $n = 4$

Figure 6.- Concluded.

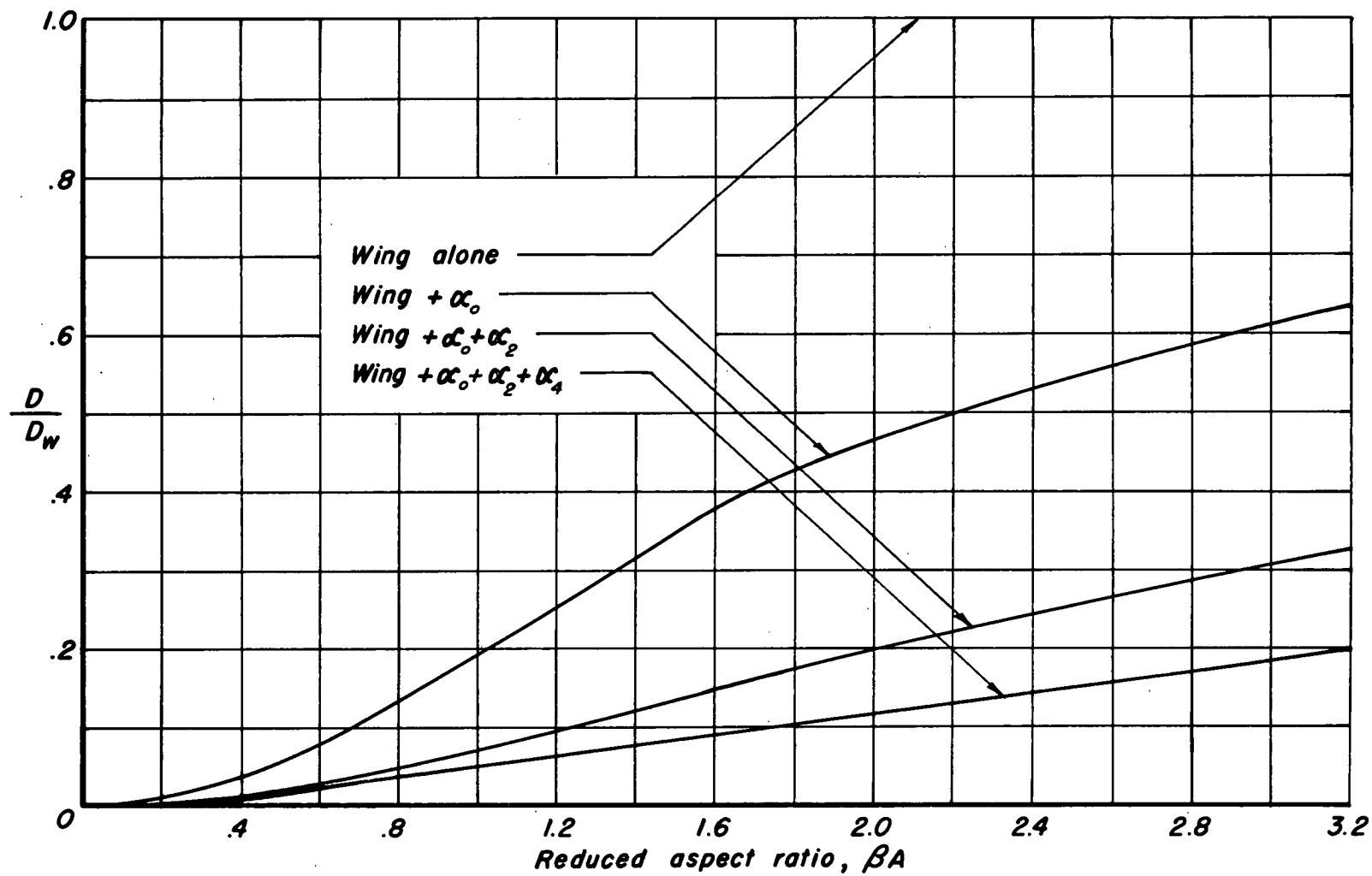
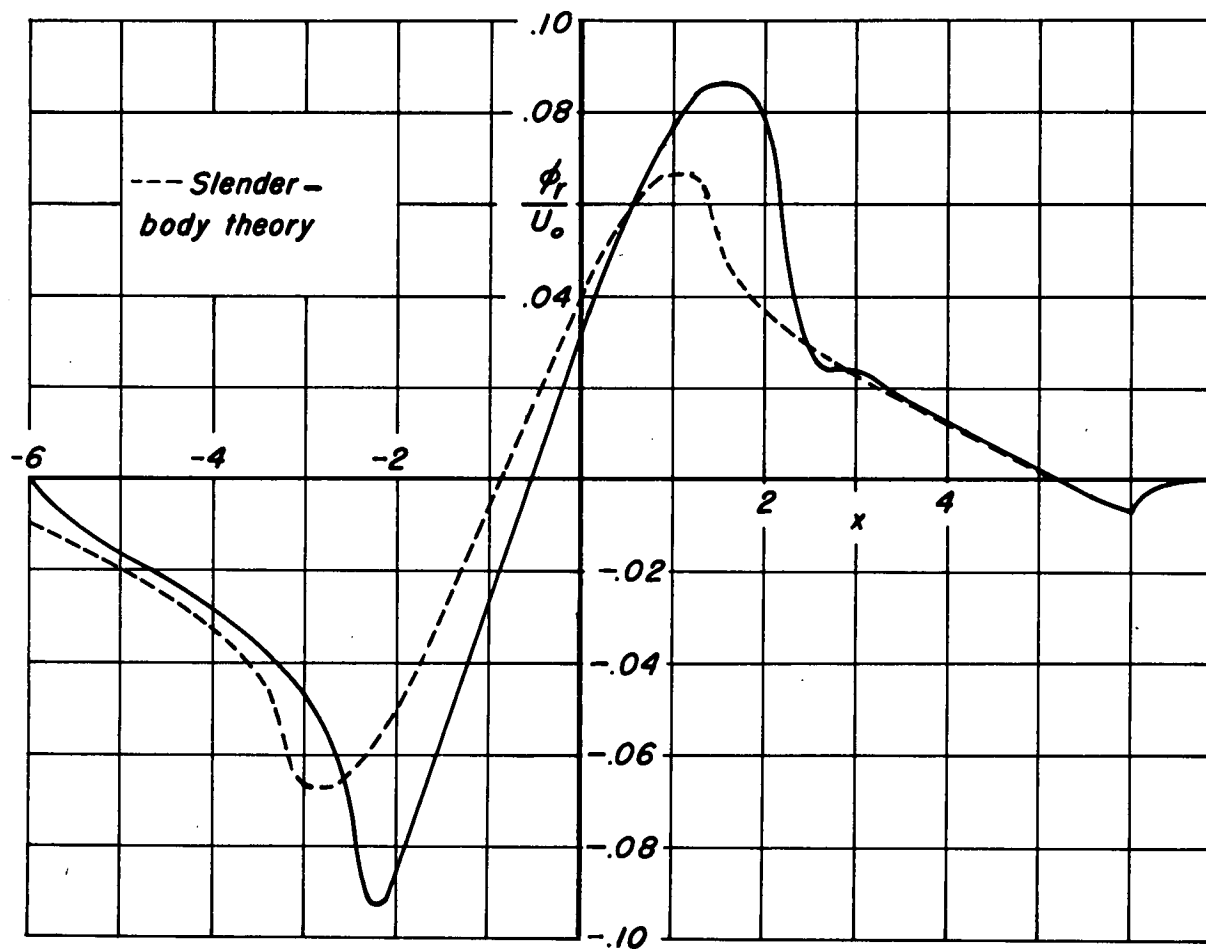
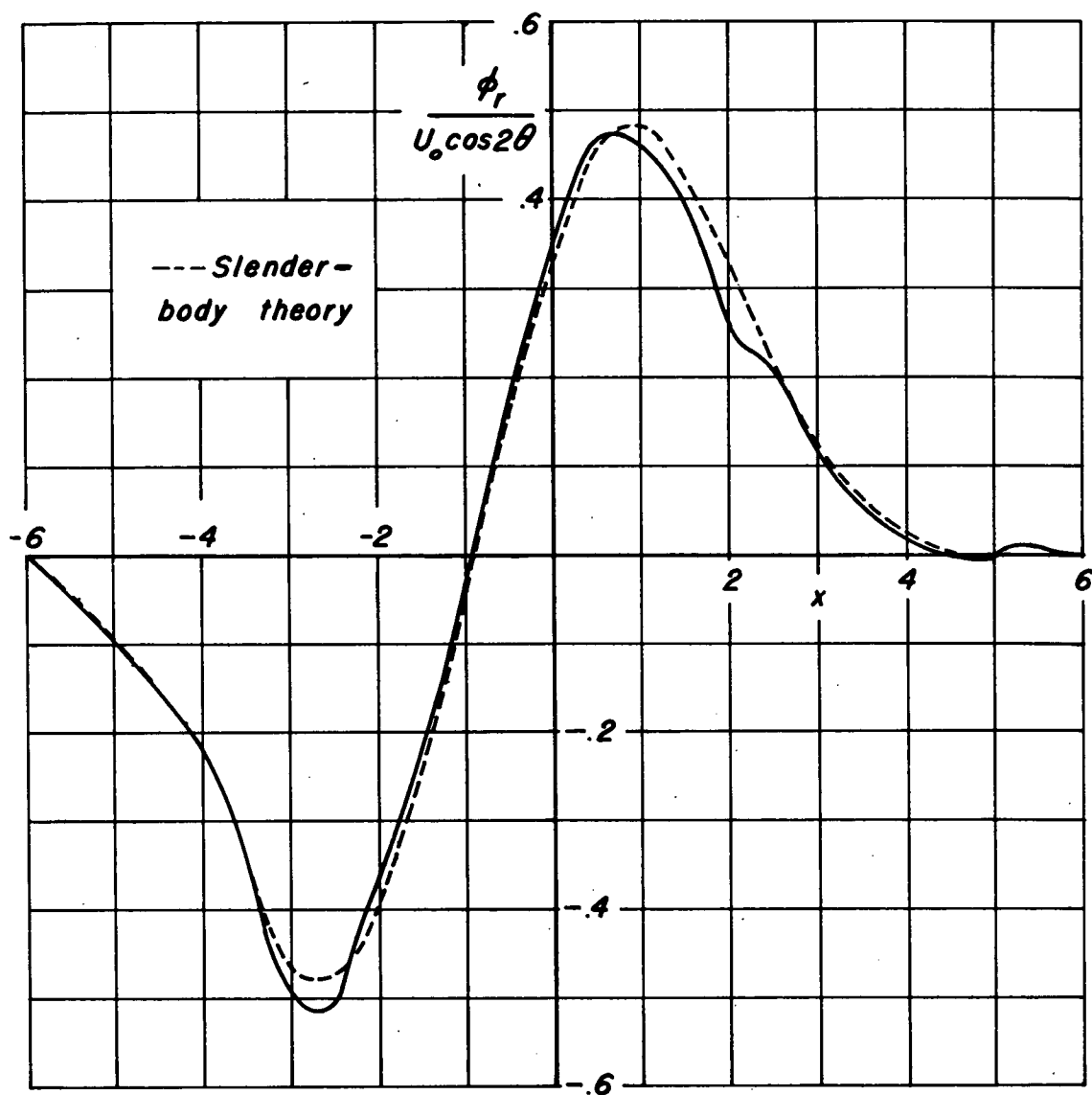


Figure 7.- Portions of elliptic-wing wave drag created by various equivalent multipole distributions.



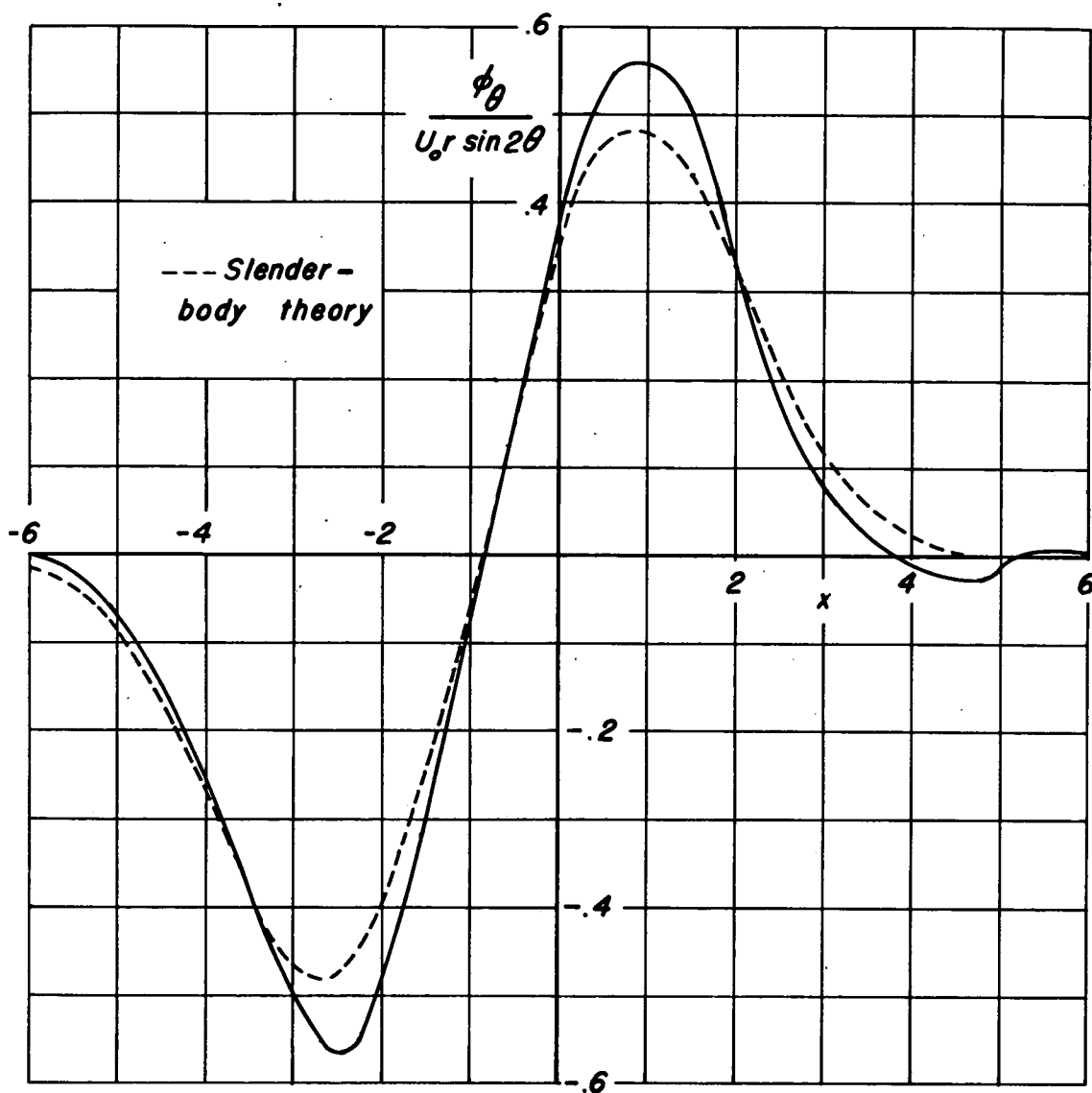
(a) Radial velocities induced by sources.

Figure 8.- Velocities induced by the elliptic-wing cancellation multipoles at the control surface where  $\beta R/L_0 = 0.148$ .



(b) Radial velocities induced by second-order multipoles.

Figure 8.- Continued.



(c) Tangential velocities induced by second-order multipoles.

Figure 8.- Concluded.

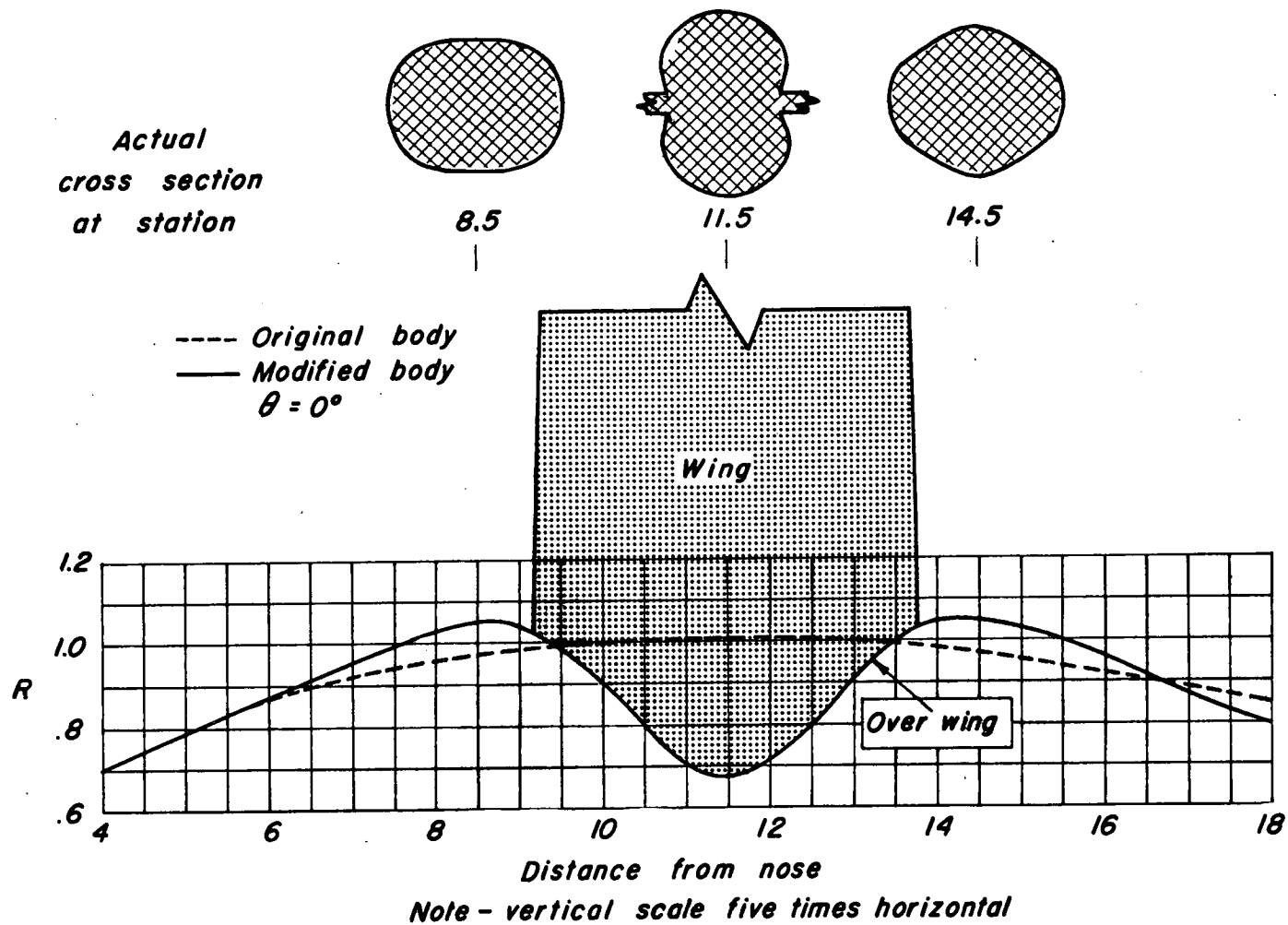


Figure 9.- Body shape having favorable interference wave drag at  $M = 1.41$  when combined with elliptic wing.



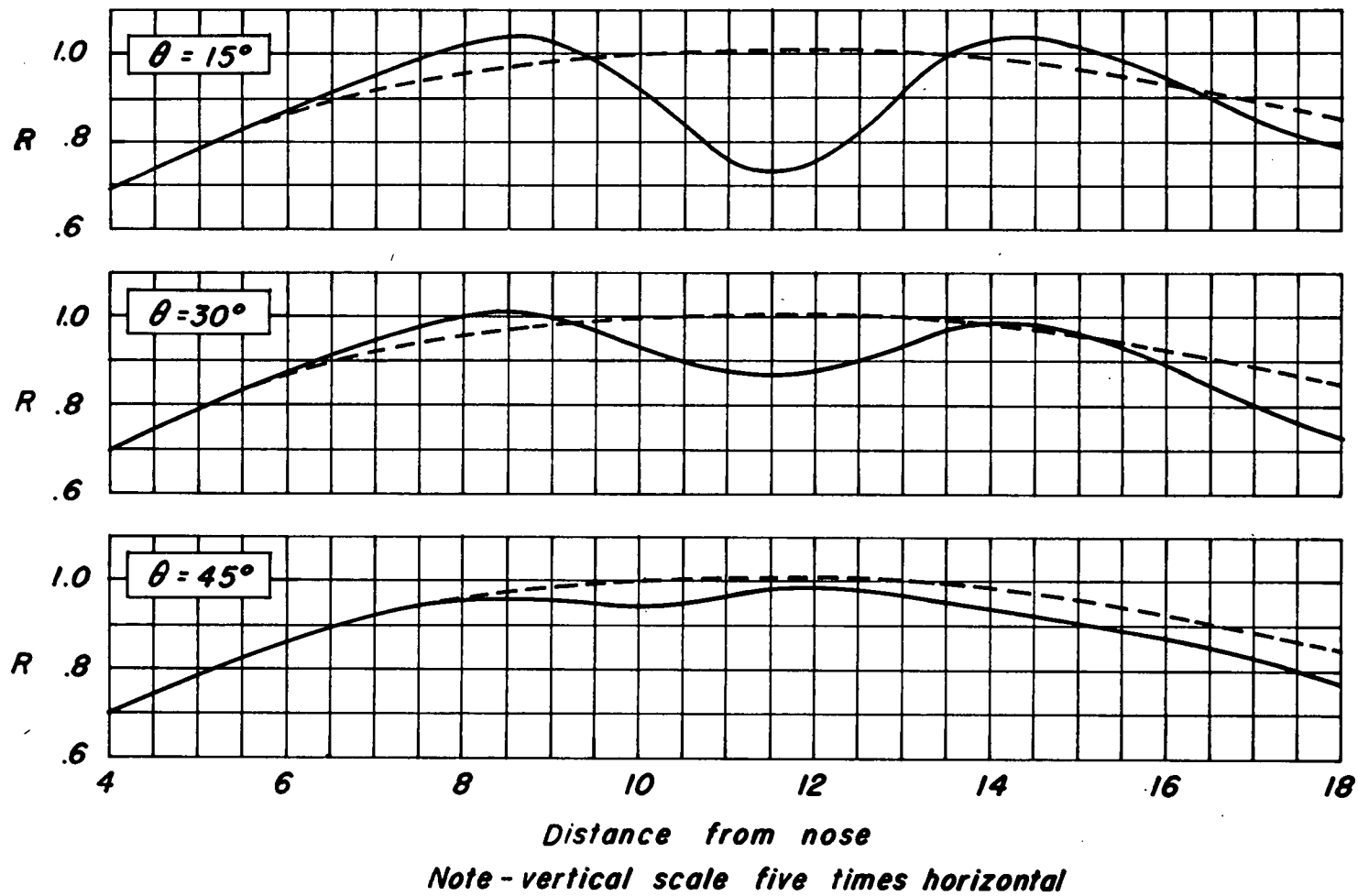


Figure 9.- Continued.

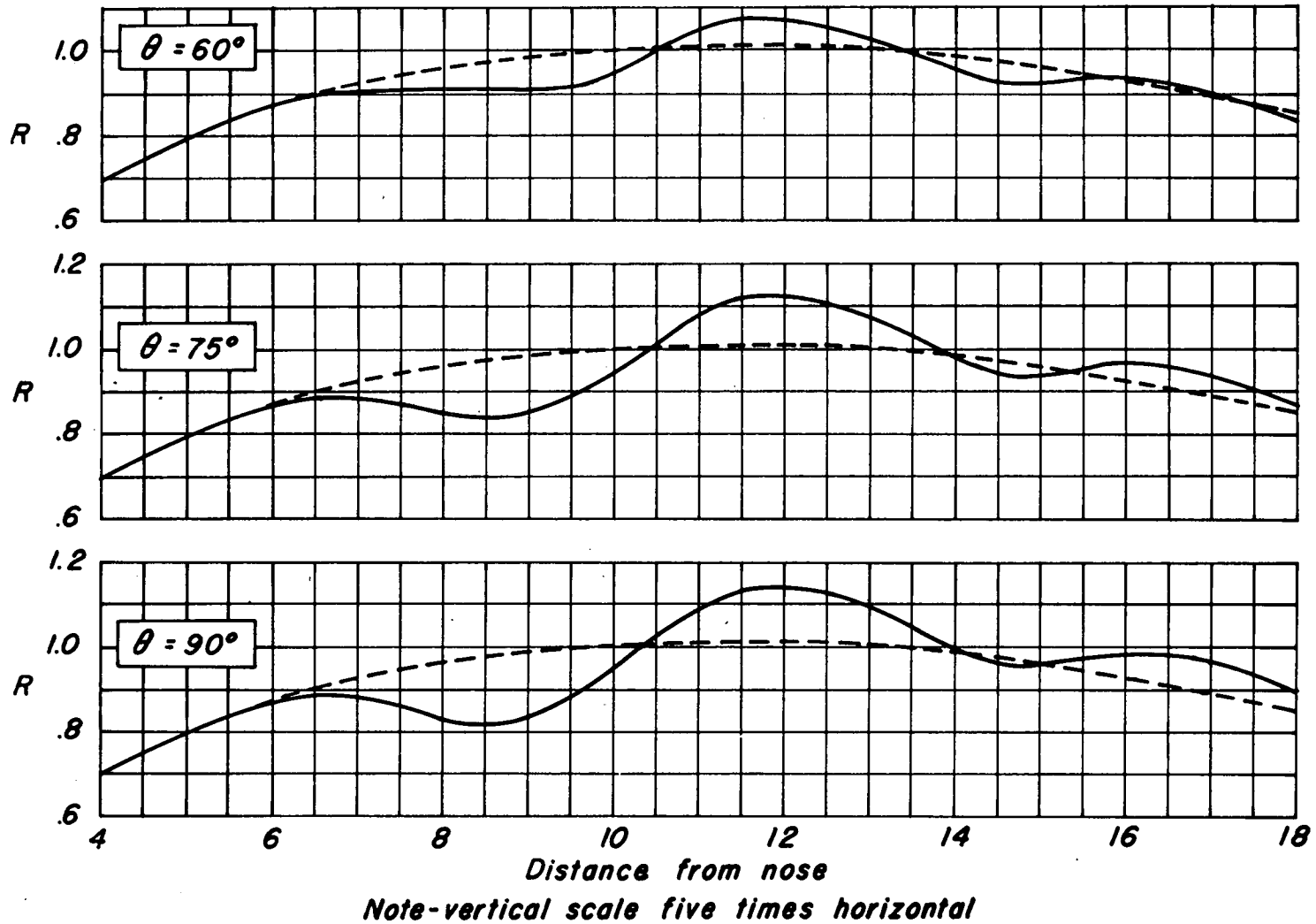


Figure 9.- Concluded.

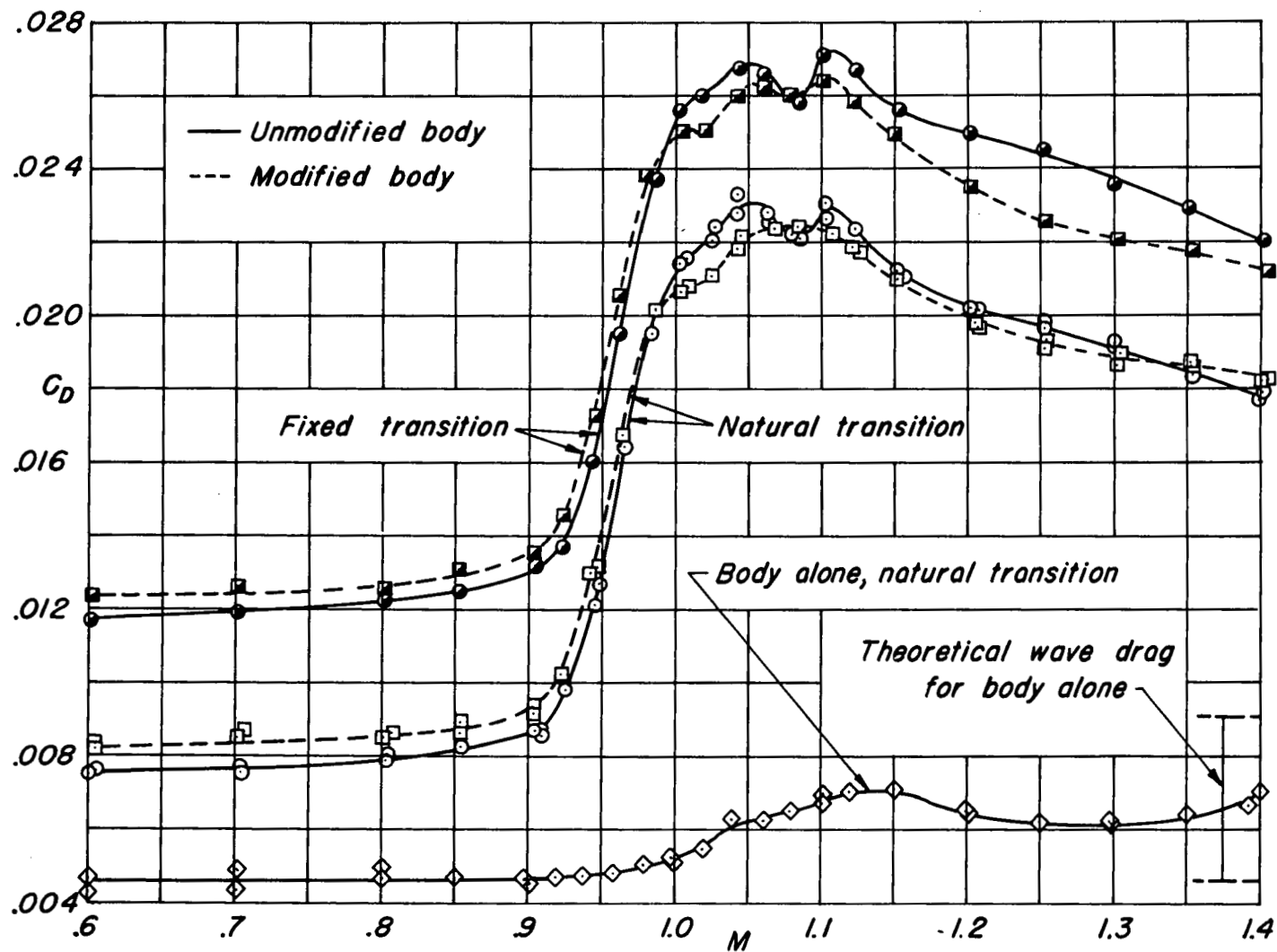


Figure 10.- Experimental values for drag coefficient.

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